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No. [REDACTED]

14 November 1967

TO:

[REDACTED]
C. Murphy
A. Johnson

THRU:

FROM:

SUBJECT: MISSION 1040-1 and 1040-2 FINAL REPORT

Enclosed is the Final Performance Evaluation Report for
Mission 1040-1 and 1040-2.

[REDACTED]

Manager
Advanced Projects

Declassified and Released by the N R O

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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1040-1 and 1040-2

FTV 1636 J-35

5 October 1967

Approved: [REDACTED]

[REDACTED] Manager
Advanced Projects

Approved: [REDACTED] for

[REDACTED] Mgr.
Program

FOREWORD

This report details the performance of the payload system during the operational phase of the Program [redacted] flight Test Vehicle 1636.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level-of-Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1040-1 and 1040-2 which was launched on 30 March 1967.

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INTRODUCTION

This report presents the final performance evaluation of Missions 1040-1 and 1040-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-35 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPFF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors' plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/AIM resolution are produced by AFSPFF. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary reports published by [REDACTED]

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

SECTION 1

SYSTEM PERFORMANCE

A. MISSION OBJECTIVES

The payload section of Mission 1040, placed into orbit by Flight Test Vehicle #1636 and LV-2A booster #501, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-35 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was two, 5 day photographic periods with no deactivate period. The vehicle was flown nose forward.

B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 1854 Z (1054 PST) on 30 March 1967. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1040-1 consisted of a 5 day operation and was completed by air recovery on 4 April 1967. Mission 1040-2 was completed with an air recovery on 8 April 1967 following a 4 day photographic operation.

The comparison of the planned and actual orbit parameters is tabulated as follows:

ORBITAL PARAMETERS

<u>Parameter</u>	<u>REV-1 Predicted</u>	<u>REV-42 Actuals</u>	<u>REV-11C Actuals</u>
Period (Min.)	90.30	90.265	90.091
Perigee (N.M.)	99.85	99.668	100.603
Apogee (N.M.)	214.77	214.130	210.450
Inclination (Deg.)	85.00	85.054	85.054
Perigee Latitude (Deg. N.)	20.37	28.271	45.391
Eccentricity	0.01597	0.01591	0.01529

C. PANORAMIC CAMERAS

The image quality was rated better than Mission 1038 and comparable to Mission 1039. This was a nose forward flight.

D. STELLAR-INDEX CAMERAS

Both units produced good photography for vehicle orientation data reduction. The Stellar images were point type.

E. OTHER SUB-SYSTEMS

The clock, instrumentation, command, thermal control pressure make-up and recovery subsystems performed satisfactorily.

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SCHEMATIC INBOARD PROFILE - CORONA J SYSTEM

J-35
MISSION 1040

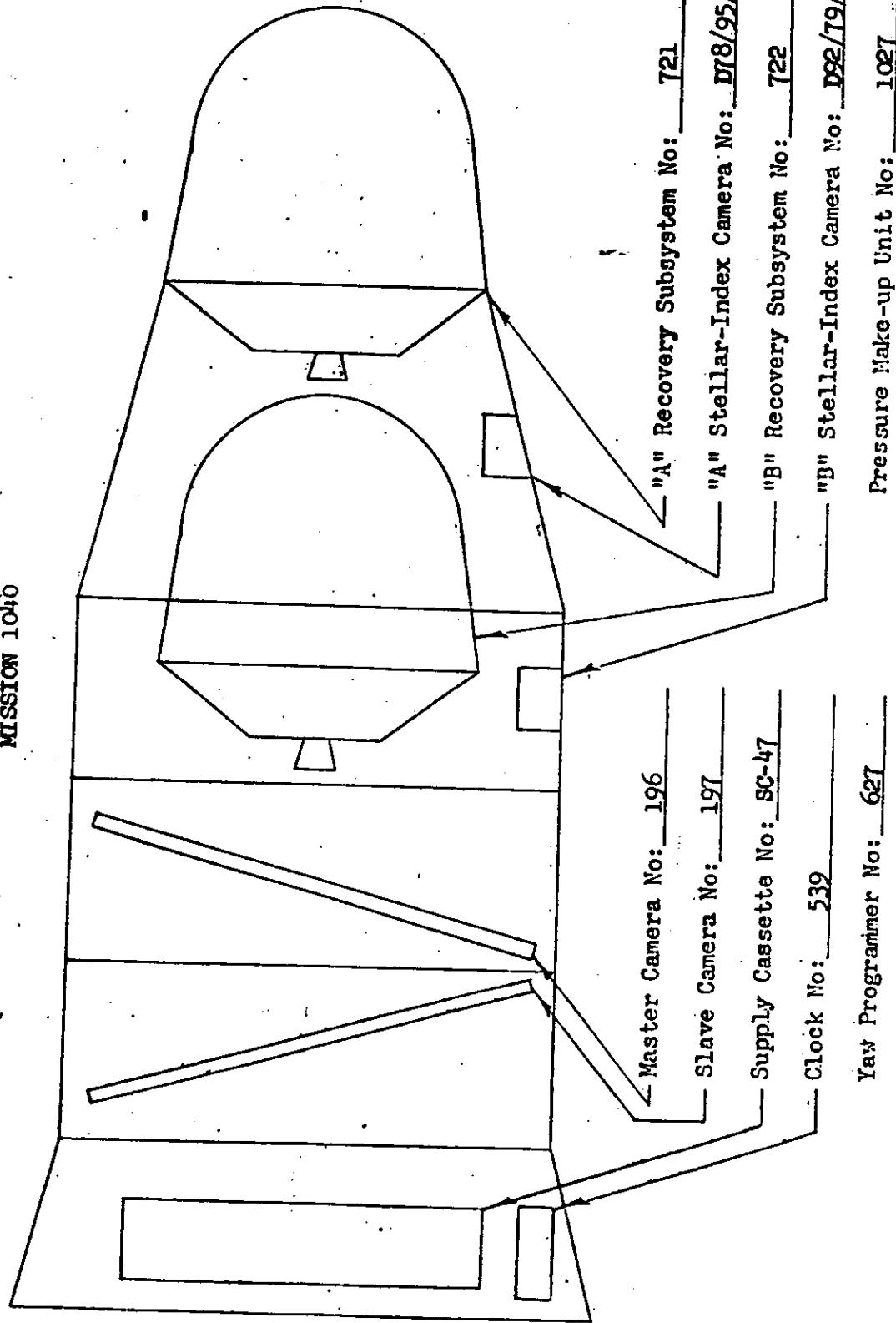


FIGURE 1-1

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SECTION 2

PRE-FLIGHT SYSTEMS TESTS

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-35 payload system was subjected to an environmental HIVOS chamber test from 30 March through 6 April 1966. A total of 5542 cycles was operated in the master instrument and 5579 cycles in the slave. The internal camera pressures experienced during this test were 0.7 to 80 microns.

The pan instruments operated satisfactorily except for the random occurrence of light or absent horizon fiducials, camera serial number and binary index imagery. This condition was checked and it was determined to be caused by voltage irregularities in the HIVOS cabling.

The only Corona observed was random occurrences of low density start-up Corona.

Payload scratching was at a minimum. Slight scan head scratches were confined to the start of scan.

The cut and wrap function was normal.

The operations of S/I D-78 and D-92 were entirely acceptable for the 425 frames cycled in each unit.

C [REDACTED]

B. RESOLUTION TEST

Resolution and theodolite tests were performed on 18 April 1966. Results of the thru-focus resolution tests of pan instruments 196 and 197 show the following characteristics:

Master Pan Instrument No. 196

Maximum high contrast resolution 169 lines/mm at -0.001 focal position.

Maximum low contrast resolution 110 lines/mm at +0.001 focal position.

Slave Instrument No. 197

Maximum high contrast resolution 187 lines/mm at +0.001 focal position.

Maximum low contrast resolution 116 lines/mm at +0.001 focal position.

Both instruments met the system requirements specification.

C. LIGHT LEAK TEST

The system was rated acceptable for flight and placed in storage. On removal from storage the space structure was disassembled and a new recovery barrel was integrated to the system. The second light leak test indicated an excessive leak from the master camera drum seals. The seals were adjusted and checked out for flight acceptability.

D. FLIGHT READINESS

The Flight Readiness test of Panoramic Instrument #196 and 197 was completed without incident on 20 March 1967. Examination of the processed 3404 type film exhibits from Instrument #196 and 197 revealed acceptable camera performance including tracking, normal rail scratches, horizon camera performance including tracking, normal rail scratches, horizon fiducials and shutter function, time track, serial number, binary index marks, binary word, shrinkage markers, and uniformity of fogged format.

Processed film exhibits from the Post Storage Baseline test from Stellar/Index cameras D-78 and D-92 demonstrated acceptable performance. Reseau, fiducial, and correlation lamp imagery, produced on film type 3401 by both stellar cameras, were rated good. Reseau and correlation lamp imagery produced on film type 3400 by both index cameras was acceptable.

Flight film spools were placed in the supply cassette without incident on 21 March 1967.

The J-35 system pre-flight acceptance run was initiated on 22 March 1967. Film transport was terminated when the field flattener rollers on Master camera #196 appeared to exhibit abnormal operation. The field flattener rollers were changed using those from J-40 system. Subsequent film operations on the morning of 23 March 1967 revealed normal J-35 system performance.

The J-35 system was accepted for flight.

Customer review and final J-35 system buy off was concluded on the afternoon of 23 March 1967.

SECTION 3

FLIGHT OPERATIONS

A. SUMMARY

All launch, ascent, and injection events occurred as programmed. The orbit achieved was within the 3-sigma dispersions.

Both panoramic cameras operated satisfactorily throughout the flight. Average cycle rates for both cameras deviated from the pre-flight calibrated values by less than 2.0 per cent.

Both the -1 and -2 Stellar/Index cameras, the clock system, and the instrumentation and command systems operated satisfactorily throughout the flight.

The on-orbit internal temperature environment was comparable to the pre-flight predictions.

The on-orbit sine function generator performed normally for the duration of the mission.

Kik-Zorro 38 (early A to B switchover) was performed on Rev 72 by the [REDACTED] Tracking Station and all transfer functions were normal.

Both recovery systems operated normally throughout the flight.

This vehicle was used as a test agena for in-flight testing of the new UNCLE Command System. Numerous tests were performed with the UNCLE system at all tracking stations. Preliminary evaluation of the UNCLE Command System, as derived from real-time Augie data is included in Paragraph H. Complete analysis of the UNCLE Command System is continuing.

The analog command system (S-PAND) failed to respond to commands on Rev 43. The cause of this failure was attributed to a failure of the type XI decoder. Command capability returned briefly on Rev 54, 55, and 56. The command system remained inoperative until Rev 113. The command system then functioned properly throughout the remainder of the mission. Payload system commanding was accomplished utilizing the VHF command system from Rev 43 through the remainder of the flight except for the isolated revs in which the analog command system was functioning.

This payload system was flown with the new gold-epoxy recovery barrel in place of the normal vacuum deposited gold finish on the recovery barrel. The remainder of the J-35 payload system conformed to the standard J-1 configuration.

B. PANORAMIC CAMERA PERFORMANCE

Both panoramic cameras operated normally throughout the mission. Cycle period data for the engineering passes monitored are tabulated in Table 3-1. Camera system dynamic operation, 99/101 clutch operation, start-up, shut-down, and transport functions were normal for all passes monitored. The cut and wrap operation and transfer to the -2 system occurred as programmed utilizing the Kik-Zorro 38 command (early A to B switchover).

The panoramic film was exhausted on Rev 136 Frame No. 61 on the Master (Aft Looking) and Rev 143 Frame No. 13 on the Slave (FWD Looking).

Panoramic Film Consumption (Frames)

	<u>Actual</u>	
	<u>Master</u>	<u>Slave</u>
Sample Off-Spooling	19	19
Pre-Launch	150	148
-1 Mission	2780	2734
-2 Mission	3113	3161
Total	6062	6062

FMC Match

The V/h ramp to orbit match was acceptable throughout the flight. The following settings 6, 8, and 10 were utilized to obtain the optimum FMC match during the flight:

	<u>RTC Commands</u>	<u>Remarks</u>
RTC Positions	6 8 10	Launch thru Rev 4
	6 5 6	Rev 4 thru the end of the mission
	6 5 7	

C. STELLAR/INDEX CAMERA PERFORMANCE

Both the -1 and -2 Stellar/Index cameras operated satisfactorily on all monitored engineering passes.

D. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

The instrumentation and command systems operated properly throughout the flight except for an intermittent vehicle command system failure on the S-Band Link which resulted in the loss of the primary payload command system. Subsequent to this failure, all payload commands were issued by the secondary command system (VHF Link) except for a few revs in which the S-Band command system was operative.

E. CLOCK SYSTEM PERFORMANCE

Clock system operation was normal for the duration of the flight. Satisfactory time correlation between the flight clock and [REDACTED] Tracking Station time was obtained. Table 3-2 contains the correlation data.

F. PRESSURE MAKE-UP SYSTEM PERFORMANCE

Pressure make-up system performance was normal throughout the flight. Average gas consumption was approximately 8.7 psi/min for the 234 minutes of total operate time. The system had a surplus of 360 PSIA at the end of the mission.

G. THERMAL ENVIRONMENT

Temperature data for the [REDACTED] acquisitions are included in Table 3-3. The average instrument temperatures ranged from a high of 80°F on the Master and 77°F on the Slave to a low of 68°F on the Master and 65°F on the Slave.

The thermal control paint pattern on the payload system and on the gold-epoxy R-Barrel were modified for this flight. This modification produced temperature predictions of 75°F ± 5°F on the Master and 70°F ± 5°F on the Slave.

H. UNCLE COMMAND SYSTEM FLIGHT TEST

FLIGHT OBSERVATIONS (Based on AUGIE data and real-time microwave records from 13 [redacted] passes)

1. UNCLE System will accept "clear" and "special" execute commands at 20 and 1000 Bits/Second.

The [redacted] microwave data indicates however that periodic command failures will occur during a repetitive sequence, the incidence of failures being significantly higher at low elevations (weak signal strengths).

2. In no observed case did a "false" command execute.

Testing included "long" and "short" commands, parity errors, simultaneous bits, false address as well as a false KIK UNCLE 40 (secure execute) command.

3. Antenna point error is not critical.

The command antenna drive was stopped in a number of cases while commanding in a repetitive mode. Commands continued to be accepted for up to two minutes in these cases.

4. UNCLE somewhat susceptible to "turn on" and random bits at low signal strength.

Under certain conditions the UNCLE receiver appears to accept (or generate) a significant number of data bits. These bits are accepted by the decoder and load the shift register. No spurious decoder command outputs were observed but a probability study is recommended.

5. Effective command horizon requires further investigation.

The effective, reliable UNCLE commanding horizon appears somewhat limited (UNCLE commanding being negated by noise, etc., during periods of relatively high elevation). This command horizon should be established by further analysis of data from passes where repetitive commanding was performed near acquisition and fade.

6. 84 task accomplishments by Satellite Control Facility (in spite of "unscheduled" requirement to use ZEKE system extensively) will provide ample data for analysis.

J-35 FLIGHT

[REDACTED] INST. 196 ----- INST. 197 -----

REV. OP RAMP TUR SYSTEM ACTUAL UNIT SYSTEM ACTUAL UNIT SYSTEM 196/1
 MODE : R A SECS CALIB. DEV. DEV. DEV. DIFF.

008	A	6	5	80	3.887	3.604	1.75F	2.02F	3.832	1.70F	1.43F	0.60
016	A	6	5	1705	2.248	2.242	0.30S	0.25F	2.273	0.59S	1.18S	1.38
047	A	6	5	1793	2.221	2.250	1.77S	1.30S	2.250	0.75S	1.30S	0.0
079	B	6	5	1781	2.224	2.225	0.61S	0.05S	2.250	0.63S	1.18S	1.12
111	B	6	5	1999	2.215	2.225	0.70S	0.45S	2.243	0.34S	1.27S	0.81
127	B	6	5	2054	2.222	2.235	1.68S	0.57S	2.250	0.69S	1.24S	0.67

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2
F=FAST AND S=SLOW

TABLE 3-1

TOP SHEET

CLOCK CORRELATION SUMMARY.

ORDER FIT ONE

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.234034810 05	0.2648036560 06	0.2340343620 05	-0.0052	8	
0.685067780 05	0.3099069650 06	0.6850678860 05	-0.0106	16	
0.237174830 05	0.3515170620 06	0.2371747940 05	0.0036	24	
0.687287300 05	0.3965289170 06	0.6872872770 05	0.0023	32	
0.239957610 05	0.4381959520 06	0.2399575560 05	0.0044	40	
0.63092980 05	0.4778094990 06	0.630929770 05	0.0003	47	
0.242340920 05	0.5248342940 06	0.2423408570 05	0.0063	56	
0.638284780 05	0.2755777600 05	0.6382847390 05	0.0041	63	
0.244788860 05	0.7460819400 05	0.2447888490 05	0.0011	72	
0.640137930 05	0.1141431060 06	0.6401379100 05	0.0020	79	
0.246003030 05	0.1611356230 06	0.2460030110 05	0.0019	88	
0.641149100 05	0.2006442360 06	0.6411490820 05	0.0018	95	
0.247245470 05	0.2476538810 06	0.2472454630 05	0.0007	104	
0.642217210 05	0.2871510660 06	0.6422172540 05	-0.0044	111	
0.248058290 05	0.3341351810 06	0.2480583350 05	-0.0045	120	
0.642793380 05	0.3736087000 06	0.6427934660 05	-0.0086	127	
0.194847350 05	0.4152140990 06	0.1948473940 05	-0.0044	135	
0.642973530 05	0.4600272100 06	0.6429784380 05	0.0092	143	

A0=-0.24140013050 06 A1= 0.9999998516690 00

SIGMA=0.00494 NO. POINTS= 18

RATIO OF CLOCK TIME TO SYS TIME= 0.1000000148130 01

ORDER FIT TWO

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.234034810 05	0.2648036560 06	0.2340348290 05	-0.0019	8	
0.685067780 05	0.3099069650 06	0.6850678640 05	-0.0084	16	
0.237174830 05	0.3515170620 06	0.2371747230 05	0.0047	24	
0.687287300 05	0.3965289170 06	0.6872872750 05	0.0025	32	
0.239957610 05	0.4381959520 06	0.2399575710 05	0.0039	40	
0.63092980 05	0.4778094990 06	0.6309298870 05	-0.0007	47	
0.242340920 05	0.5248342940 06	0.2423408730 05	0.0047	56	
0.638284780 05	0.2755777600 05	0.6382847570 05	0.0023	63	
0.244788860 05	0.7460819400 05	0.2447888690 05	-0.0009	72	
0.640137930 05	0.1141431060 06	0.6401379300 05	-0.0040	79	
0.246003030 05	0.1611356230 06	0.2460030290 05	0.0001	88	
0.641149100 05	0.2006442360 06	0.6411490760 05	0.0002	95	
0.247245470 05	0.2476538810 06	0.2472454730 05	-0.0003	104	
0.642217210 05	0.2871510660 06	0.6422172590 05	-0.0049	111	
0.248058290 05	0.3341351810 06	0.2480583310 05	-0.0041	120	
0.642793380 05	0.3736087000 06	0.6427934550 05	-0.0075	127	
0.194847350 05	0.4152140990 06	0.1948473730 05	-0.0023	135	
0.642973530 05	0.4600272100 06	0.6429784050 05	0.0125	143	

A0=-0.24140014440 06 A1= 0.9999999020060 00

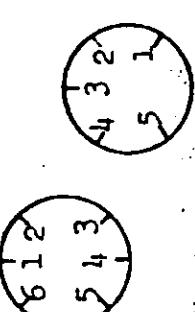
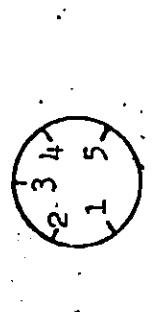
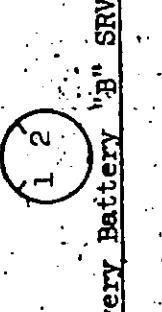
A2=-0.39709291206480-13

TABLE 3-2

TABLE 3-3
J-35 TEMPERATURE SUMMARY

Master Camera		Sensors Acquired												Slave Camera		Supply Room			
Sensor		Avg	16	24	32	40	47	56	63	72	79	88	92	106	111	120	Avg	Supply	Room
3	72	63	65	63	68	73	70	74	68	74	75	78	73	77	74	76	67	63	59
4	80	69	73	68	72	76	78	73	78	72	77	79	74	70	74	72	67	62	66
5	81	72	72	75	78	74	75	79	77	77	78	74	75	74	75	76	69	62	68
6	88	75	75	78	74	78	75	78	74	75	77	74	76	75	77	75	65	60	64
7	80	73	73	78	74	79	74	79	74	75	76	75	76	74	77	75	64	59	62
8	83	73	80	73	81	82	74	81	75	75	75	75	75	75	75	75	69	64	66
9	84	74	82	82	84	78	68	74	68	75	67	75	68	71	69	74	64	61	65
11	78	68	74	68	77	68	75	75	71	75	71	76	72	75	71	69	63	61	65
12	80	68	77	68	77	75	75	75	71	75	71	76	72	75	71	68	63	61	65
13	79	71	71	73	71	75	71	75	71	75	71	76	72	75	71	69	63	61	65
Avg	80	74	78	74	76	71	71	77	71	76	71	75	73	73	73	70	69	63	66
Slave Camera																			
3	76	67	70	67	75	72	80	75	69	76	69	75	70	73	76	72	66	62	65
4	80	71	76	72	76	77	68	72	69	75	70	74	70	75	77	72	69	64	67
5	76	67	70	70	73	73	69	74	71	75	70	75	73	73	76	73	69	64	67
6	75	67	70	68	72	72	78	73	78	72	75	73	78	73	77	72	69	64	67
7	77	69	71	75	72	72	68	72	69	74	71	75	73	73	77	72	69	64	67
8	79	71	75	75	72	78	74	75	72	78	73	75	74	73	77	72	69	64	67
9	76	67	72	68	65	65	65	67	64	65	65	65	67	65	65	67	63	61	64
11	68	62	68	62	68	65	65	65	67	65	65	65	67	65	65	67	63	61	64
12	78	68	74	69	74	71	69	71	71	74	71	74	70	70	75	71	68	64	67
13	74	67	71	67	71	68	69	70	69	71	67	71	68	70	73	70	68	64	67
Avg	77	65	74	66	73	70	69	73	69	71	67	71	68	70	73	70	68	64	67

TABLE 3-3
J-35 TEMPERATURE SUMMARY

<u>SENSOR</u>	<u>ORBITS ACQUIRED</u>											
	A		B		C		D		E		F	
	1	2	1	2	1	2	1	2	1	2	1	2
Fair ("A") Barrel #1 ("B")	8	16	24	32	40	47	56	63	72	88	95	104
1 	29	98	23	68	29	74	22	71	27	18	27	30
2	15	22	20	9	12	9	9	9	57	39	48	39
3	-2	02	-2	-2	2	2	-2	2	5	5	50	109
4	39	45	27	42	39	45	36	45	33	65	83	102
5	50	75	32	12	47	81	44	81	44	49	79	46
6	37	107	27	89	37	92	37	95	37	56	59	38
Barrel #2												
1 	43	46	28	46	39	49	46	52	43	55	33	55
2	42	67	27	58	39	61	48	64	42	67	42	36
3	70	109	37	82	67	88	70	85	64	79	82	109
4	64	55	36	46	64	49	64	46	58	52	37	46
5	59	52	33	56	56	56	56	56	49	52	31	37
Conic Adapter												
1	42	57	30	57	45	63	45	63	45	69	38	75
Clock												
1	68	62	36	64	72	66	68	64	58	60	60	58
2	63	59	53	59	63	61	65	59	53	53	57	53
Thrust Cone "A" to "B" SRV												
1	42	32	36	31	34	31	34	37	30	55	52	56
2	61	49	43	48	53	48	53	48	52	69	71	69
R. Barrel												
1 	57	101	32	85	57	88	51	88	54	94	57	94
2	50	47	31	31	44	31	44	31	38	31	35	31
Recovery Battery "B" SRV												
1	64	58	57	57	56	57	57	57	57	80	76	82
Master Cassette "A" SRV												
2	68	63	64	66	67	67	66	65	65	64	64	64

C [REDACTED]
SECTION 4

MISSION 1040-1 RECOVERY SYSTEM

SRV #721 was received at A/P on 24 November 1965. The receiving weight was 149.95 pounds. After modifications and incorporation of outstanding E.O.'s, the SRV was delivered to Systems Test for incorporation into the J-35 system.

The capsule was shipped to VAFB on 26 March 1967.

The -1 recovery capsule was successfully recovered by air catch Rev 81 at 1517 PST on 4 April 1967. All re-entry events appeared normal and occurred within tolerance. The capsule impact point was approximately 8 N.M. south of the predicted impact point.

	<u>Latitude</u>	<u>Longitude</u>
Predicted	25° 45.2' N	156° 37.4' W
Actual	25° 36.8' N	156° 36.6' W

The re-entry sequence of events is contained in Table 4-1.

MISSION 1040-1
RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.71	77.0 ± 1.0
*Transfer	1.98	2.0 ± 0.25
Electrical Disconnect	0.86	0.900 ± 0.430 0.400
Separation	--	--
**Spin	3.40	3.4 ± 0.30
Retro	7.49	7.55 ± 0.45
Despin	10.67	10.75 ± 0.59
T/C Separation	1.51	1.5 ± 0.15
***"G" Switch Open	493.37	493.4
Parachute Cover Off	33.39	34.0 ± 1.5
Drogue Chute Deployed	0.68	0.63 ± 0.08
Main Chute Bag Separate	10.82	10.0 ± 3.0 - 2.2
Main Chute Deployed	0.52	0.52 ± 0.13
Main Chute Disreef	4.88	4.5 ± 0.80

* From Separation
 ** From Electrical Disconnect
 *** From Retro

TABLE 4-1

~~TOP SECRET~~

C [REDACTED]

SECTION 5

MISSION 1040-2 RECOVERY SYSTEM

SRV #722 was received at A/P on 24 November 1965. The receiving weight was 152.00 pounds. After modifications and incorporation of outstanding E.O.'s the unit was delivered to Systems Test for mating to the J-35 system.

The capsule was shipped to VAFB on 26 March 1967.

The -2 recovery capsule was successfully recovered by air-catch on Rev 145 at 1524 PST on 8 April 1967. All re-entry events appeared normal and occurred within tolerance. The capsule impact point was slightly south of the predicted impact point.

	<u>Latitude</u>	<u>Longitude</u>
Predicted	26° 02.6' N	164° 48.4' W
Actual	25° 58.4' N	164° 47.4' W

The re-entry sequence of events is contained in Table 5-1.

MISSION 1040-2
RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.83	77.0 ± 1.0
*Transfer	2.0	2.0 ± 0.25
Electrical Disconnect	0.88	0.900 ± 0.430
Separation	--	0.400
**Spin	3.40	3.4 ± 0.30
Retro	7.55	7.55 ± 0.45
Despin	10.60	10.75 ± 0.59
T/C Separation	1.50	1.5 ± 0.15
***"G" Switch Open	511.80	514.1
Parachute Cover Off	33.47	34.0 ± 1.5
Drogue Chute Deployed	0.65	0.63 ± 0.08
Main Chute Bag Separate	10.19	10.0 ± 3.0
Main Chute Deployed	0.54	0.52 ± 0.13
Main Chute Disreef	4.63	4.5 ± 0.80

* From Separation
 ** From Electrical Disconnect
 *** From Retro

TABLE 5-1

SECTION 6

J-35 PANORAMIC CAMERAS

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Master (AFT)</u> <u>Serial Number</u>	<u>Slave (FWD)</u> <u>Serial Number</u>
Main Camera	196	197
Main Camera Lens	1952435	1972435
Supply Horizon Camera	299-G6H	293-G6H
Supply Horizon Camera Lens	E12851	E12901
Take-up Horizon Camera	298-G5H	294-G5H
Take-up Horizon Camera Lens	E12847	E12884
Supply Cassette	SC-47	SC-47

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5	24" f/3.5
Slit Width	0.175"	0.225"
Filter Type	Wratten 21	Wratten 234
Film Type (Eastman)	3404	3404

Supply Horizon Cameras:

	<u>Starboard</u>	<u>Port</u>
Lens	55 mm f/6.3	55 mm f/6.3
Aperture Setting	f/6.3	f/8.0
Exposure Time	1/100 second	1/100 second
Filter Type	Wratten 25	Wratten 25

Take-up Horizon Cameras:

	<u>Port</u>	<u>Starboard</u>
Lens	55 mm f/6.3	55 mm f/6.3
Aperture Setting	f/8.0	f/6.3
Exposure Time	1/100 second	1/100 second
Filter Type	Wratten 25	Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION (Master Camera)

The Master camera produced 2734 frames (7650 Feet) of photography during Mission 1040-1 and 3211 frames (8347 Feet) during Mission 1040-2. Image quality was rated better than Mission 1038 and comparable to Mission 1039. The MIP was 85.

Image quality produced by the Master camera was rated slightly lower in overall sharpness than the Slave camera for Mission 1040-1 and 1040-2. The comparison was made by visual evaluation using original negative and duplicate positive films magnified by 20 to 50 times. The overall image quality of Mission 1040-1 was judged to be comparable to Mission 1040-2.

Auxiliary data recording such as H.O. fiducials, timing track, binary word, serial number, index marks, S/I slur pulse, and blanked pulse were operational throughout Mission 1040-1 and 1040-2. An intermittent minus density streak up to one quarter inch wide was present on master camera photography throughout Mission 1040-1. The streak appears to follow the field flattener. Minus density marking is attributed to foreign particles on the field flattener and camera filter. Improvements in cleanliness procedures have been implemented which are expected to result in fewer minus density marks in flight payload.

Small areas of smeared imagery (in the scan direction) appeared at the take-up end of the Master formats intermittently throughout Mission 1040-1 and 1040-2. Smeared areas are approximately one quarter of an inch wide and extend across the width of the format. Some of the smeared imagery occurs in minus density bands that are also approximately one quarter of an inch wide and extend across the width of the format. Banding is characteristic of an interlocking system. Ground tests at the Advanced Projects facility have been extended to include format fogging operations at camera cycle rates expected in flight as a means of detecting and correcting banding caused by marginal lens/detent interlock chatter.

Minor light leak fog is present on the fifth and next to last frame of most passes. The fog density is commensurate with the camera off periods.

D. POST FLIGHT PERFORMANCE EVALUATION (Slave Camera)

The Slave camera produced 2780 frames (7780 Feet of photography) during Mission 1040-1 and 3115 frames (8286 Feet) of photography during Mission 1040-2. Visual comparison of original negative and duplicate positive from Mission 1040-1 and 1040-2 indicate that Slave camera photography is slightly sharper than the Master camera photography.

Auxiliary data recording such as H.O. fiducials, timing track, binary word, serial number, index marks, blanked pulse, and start of pass mark were operational throughout Missions 1040-1 and 1040-2.

Heavy plus density light struck areas were observed in frames 69, 70, and 72 pass D-53 of the Slave camera Mission 1040-1. Fogging was caused by a high intensity light discharge from the satellite recovery vehicle during the post flight film retrieval operation. After a considerable diagnostic effort was completed it was concluded that the source of the momentary light flash was caused by an electrical discharge of some sort in the vicinity of the capsule. The exact cause is unknown. No further action is contemplated.

Several minus density streaks were present on the Slave camera original negative film from Missions 1040-1 and 1040-2. The Slave minus density streaks were approximately one sixteenth to one eighth of an inch wide. The minus density streaks followed the movement of the field flattener. The minus density streaks are attributed to emulsion dust and/or foreign particles on the surface of the field flatteners. As in the master camera this condition was not present at the start of Mission 1040-1.

Minus density bands approximately one fourth inch wide across the format were present at the take-up end of many frames. Occurrence was random. One frame of photography contained seven minus density bands. Imagery in some of the minus density bands was soft but not smeared. Corrective action consists of disassembling and checking all lens/stove detent mechanisms and correcting to flight configuration prior to launch.

In addition, ground testing at Advanced Projects will be extended to diagnose banding when it occurs at camera cycle rates expected in flight.

A small plus density mark one sixty-fourth of an inch in diameter was present throughout Mission 1040-1 and 1040-2 Slave camera photography. The subject mark reoccurred at regular intervals of six and one-fourth inches. The plus density mark is believed to be caused by a small high spot on the frame metering roller rubber surface.

Minor light leak fog is present on the first and third from the last frame of photography on some passes. No corrective action is indicated.

SECTION 7

MISSION 1040. STELLAR-INDEX CAMERAS

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>-1 Mission Serial Number</u>	<u>-2 Mission Serial Number</u>
Camera	D-78	D-92
Index Reseau	95	79
Stellar Reseau	96	110

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8	85 mm f/1.8
Exposure Time	1 second	2 seconds
Filter Type	None	None
Film Type (Eastman)	3401	3401

Index Camera:

Lens	38 mm f/4.5	38 mm f/4.5
Exposure Time	1/500 second	1/500 second
Filter Type	Wratten 21	Wratten 21
Film Type (Eastman)	3400	3400

C. POST FLIGHT EVALUATION (Mission 1040-1)

The Stellar/Index film recovered consisted of 439 frames of photography from each film path of S/I D-78/95/96. Minus density streaks, so often present in -1 Mission photography in previous flights, was not present in Mission 1040-1 Stellar photography.

Stars appear as point imagery in all S/I D-78 frames. Point imagery is attributed to an exposure time of one second. There are approximately 20 Stellar images in each frame of photography. Stellar baffle flare into Stellar photography was very low as evidenced by the fact that 30 per cent of the reseau grid was not detectable on every frame. Minor edge fog is present along both film edges but does not affect the active format area. The Stellar fiducials and correlation lamp imagery were acceptable throughout the photography.

The Index camera operated well throughout the mission producing 439 frames of photography. Newton rings are visible over areas of low contrast but do not interfere with the usability of the photography. Several very small minus density spots approximately 1/100 inch in diameter are present in the active format area throughout the mission. Foreign particles on the reseau grid are suspect since the minus density pattern remains the same on each format. Clean room procedures have been reviewed and improved to minimize foreign particles in the payload prior to launch. One plus density spot one sixty-fourth inch in diameter is present in each frame of Index photography near the film edge outside the active format area. The plus density spot is believed to correspond to a hole in the mirrored surface of the reseau plate. No corrective action is indicated. The correlation lamp imagery was acceptable throughout the mission.

D. POST FLIGHT EVALUATION (Mission 1040-2)

Stellar/Index camera D 93/79418 operated throughout Mission 1040-2. The Stellar and Index cameras each produced 498 frames of photography. Approximately 20 Stellar images are present in each frame of Stellar photography. Stellar images generally appear as point images. Sufficient baffle flare light was present to properly expose the reseau grid onto each Stellar format. Minor edge fog is present along both edges of the Stellar film. Two plus density streaks occurred outside the active Stellar format area along the camera serial number edge. The plus density streaks start in the pre-flight film and continue throughout the mission. Associated with the streaks is emulsion cracking. As the mission progressed, the cracking disappeared and the density of the streak diminished. No known cause could be found that explained the plus density streaks and emulsion cracking found in the Stellar film. Stellar fiducial and frame correlation lamp imagery were acceptable throughout the mission.

Several small hair like minus density marks are present on every frame of Index camera photography. The effect on terrain imagery is not significant. Index camera correlation lamp imagery is acceptable throughout the mission.

SECTION 8

PANORAMIC CAMERA EXPOSURE

The Master camera contained a 0.175 inch slit and a Wratten 21 filter. The Slave camera had a 0.225 inch slit and a Wratten 23A filter. These conditions placed the nominal exposure on the full processing curve.

The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

The nominal exposure times of the Master and Slave cameras are shown as a function of latitude for passes D-1, D-49, D-97, and D-145 in Figures 8-5 to 8-12. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]. The transition phase is a result of process machine development level changes.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>	<u>Transition</u>
1040-1	FWD	Predicted	0	79	21	
		Reported	9	21	49	21
1040-1	AFT	Predicted	0	67	33	
		Reported	12	34	36	18
1040-2	FWD	Predicted	0	66	34	
		Reported	5	22	55	18
1040-2	AFT	Predicted	1	58	41	
		Reported	2	28	55	15

TOP SECRET

C/ [REDACTED]
TOP SECRET
SOLAR ELEVATION FREQUENCY DISTRIBUTION

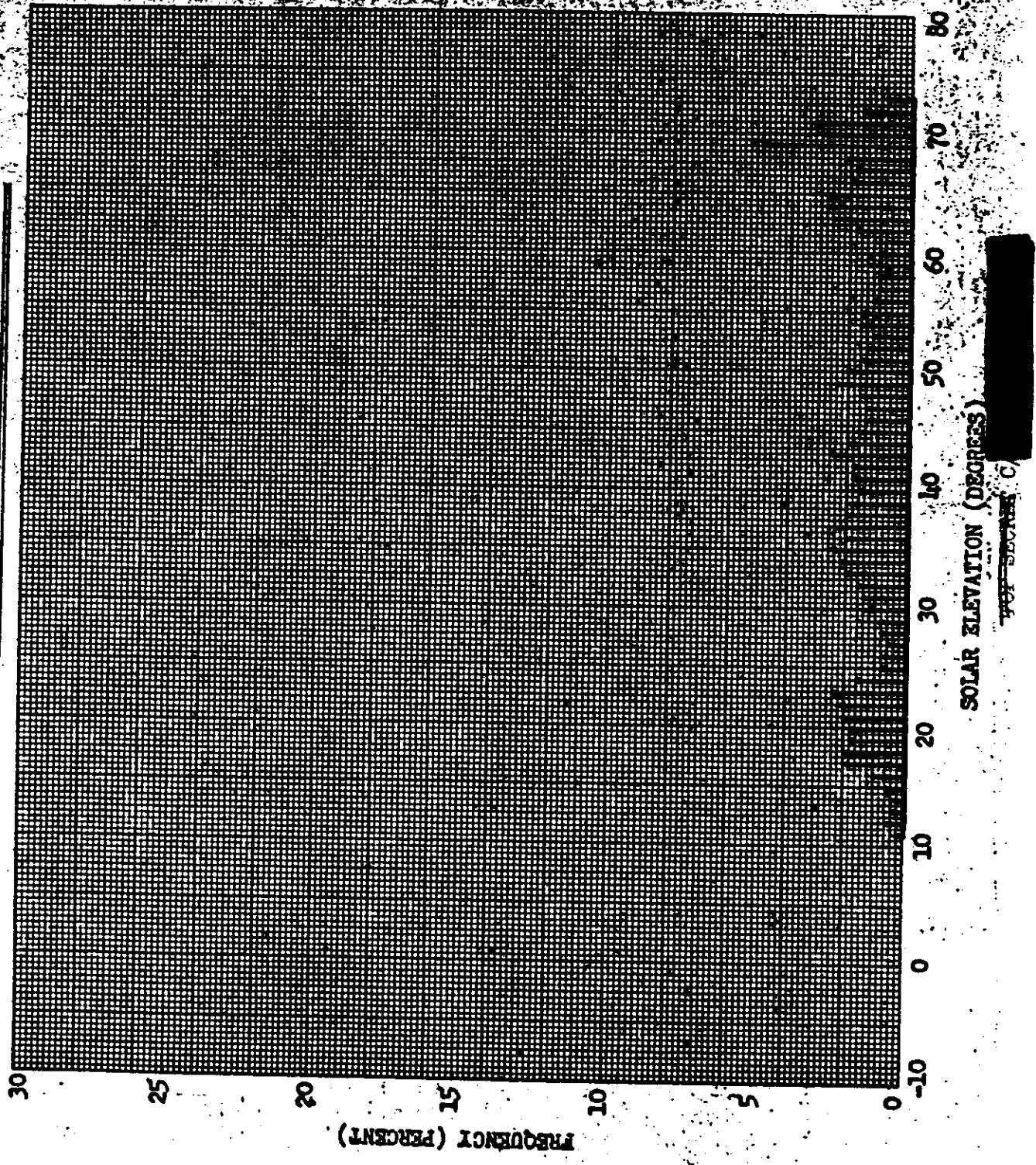
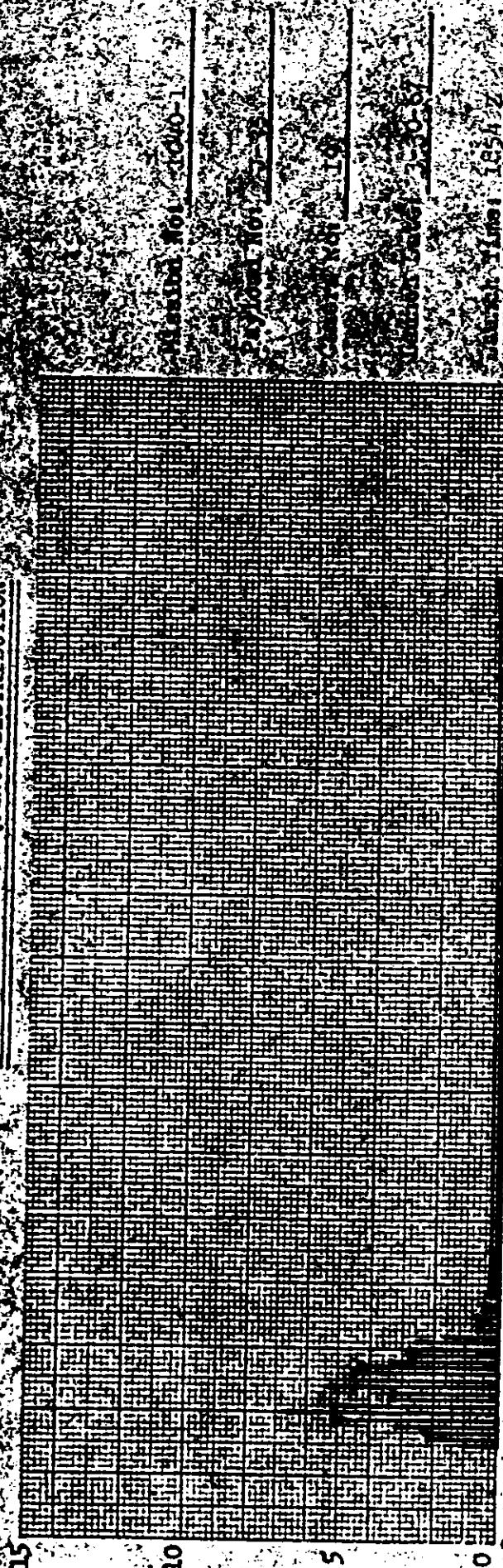


FIGURE 8-1

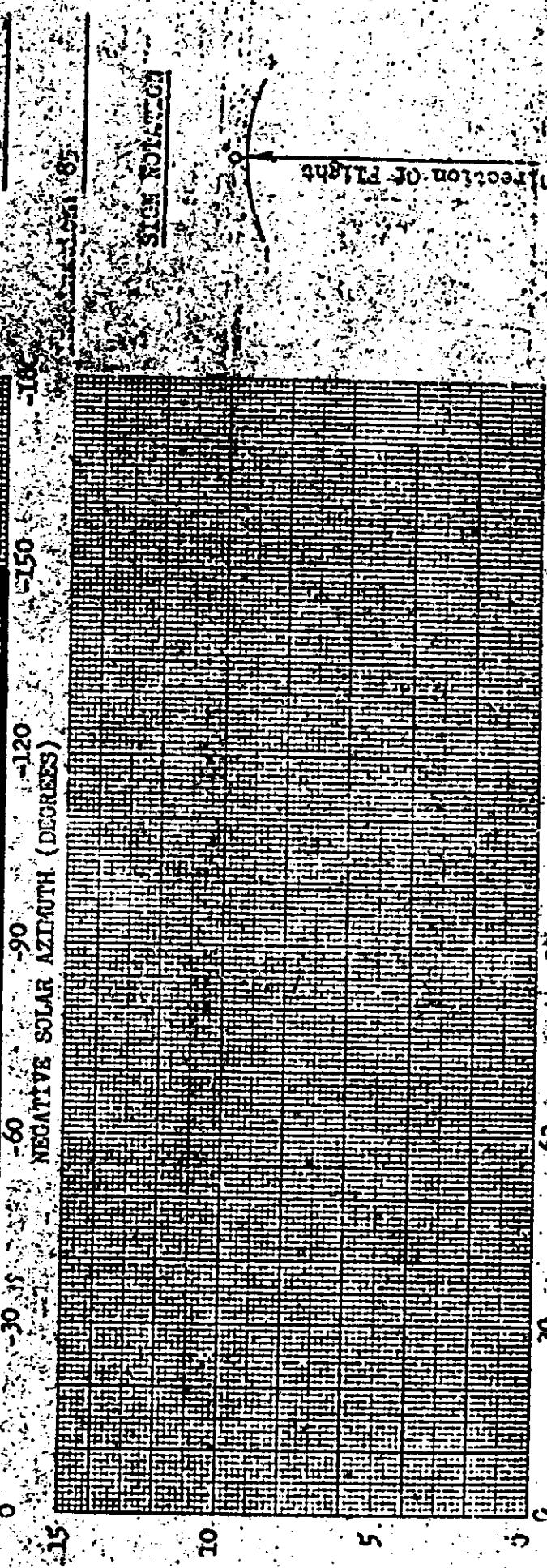
TOP SECRET

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Line 101-040-1

FREQUENCY (%)



Location of Flight

Flight 6-2

Positive Solar Azimuth (Degrees)

REF. DECODE

SOLAR ELEVATION FREQUENCY DISTRIBUTION

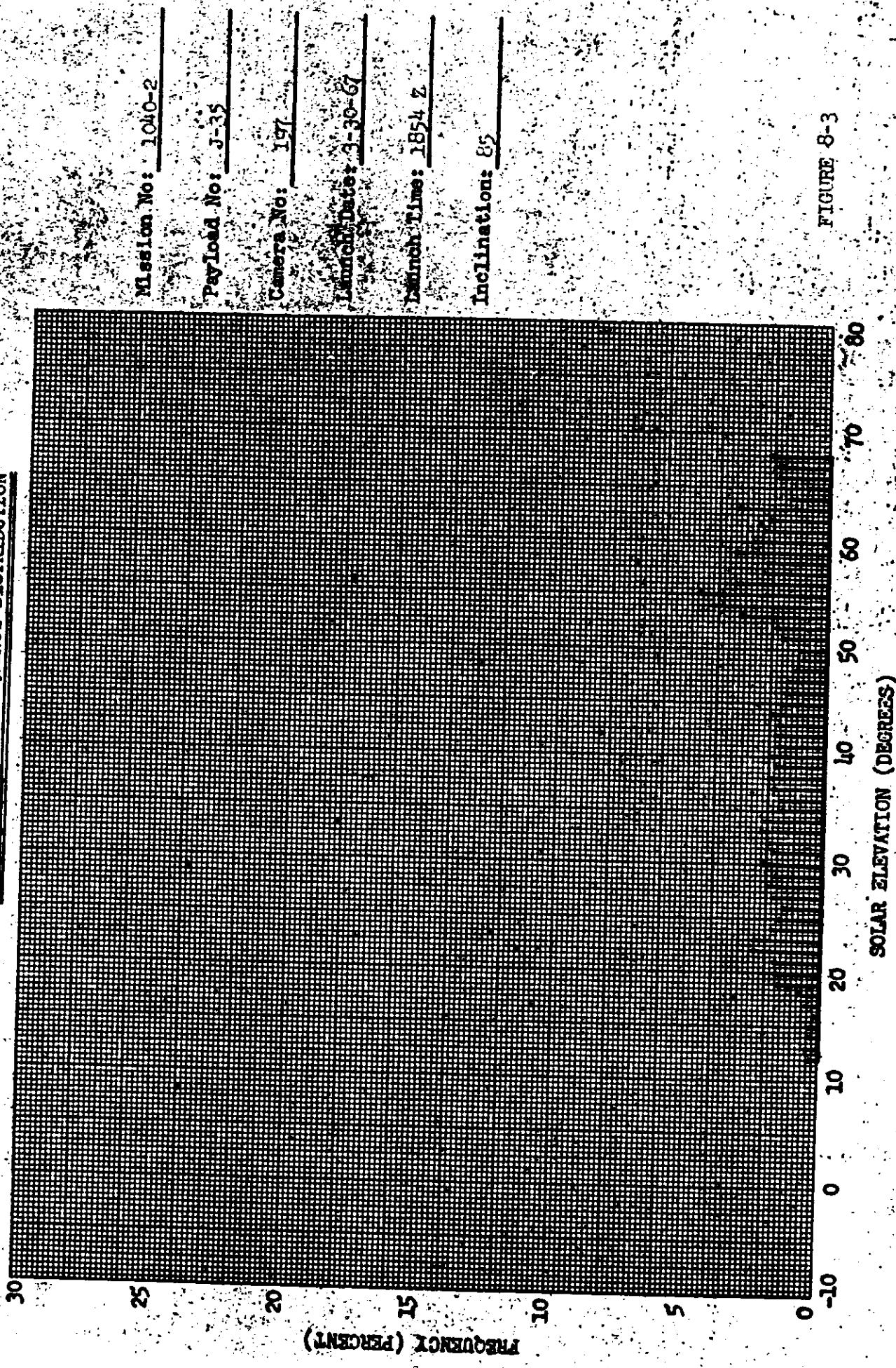


FIGURE 8-3

SOLAR AZIMUTH FREQUENCY DISTRIBUTION

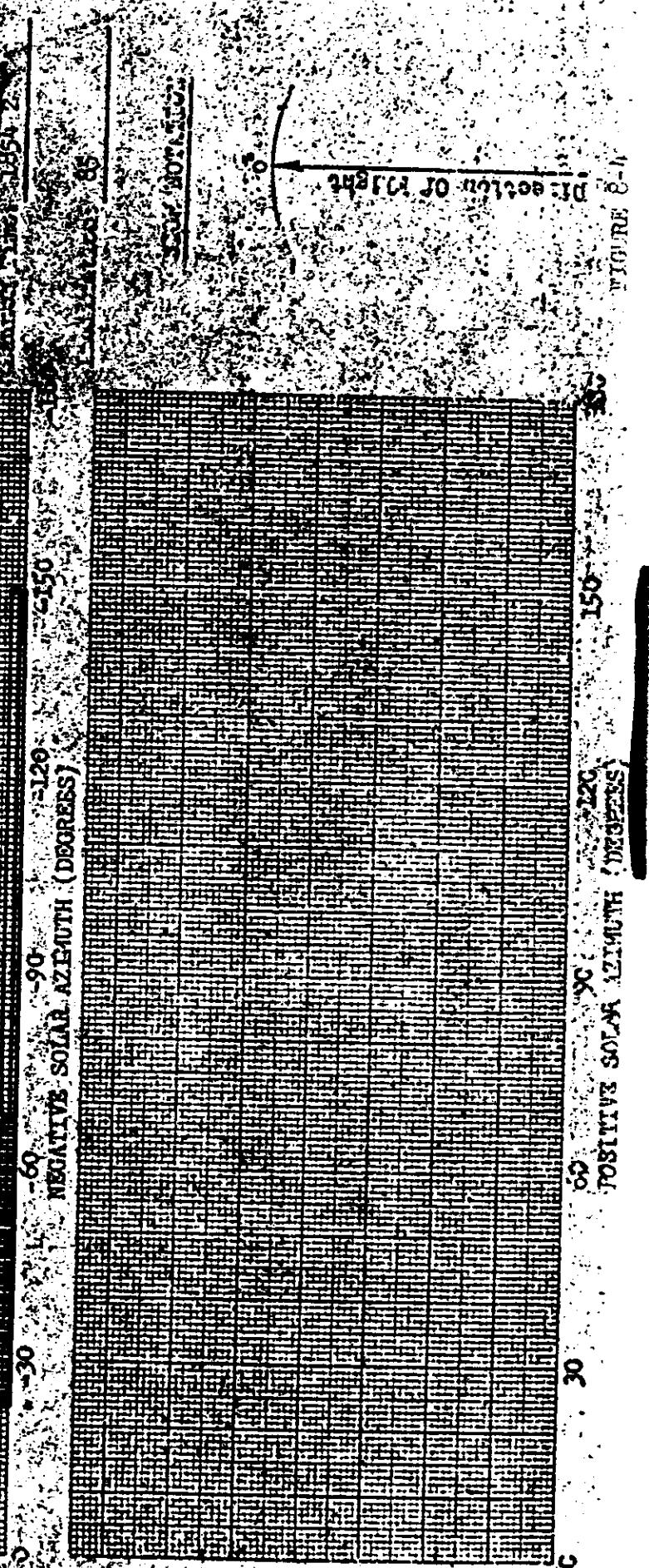
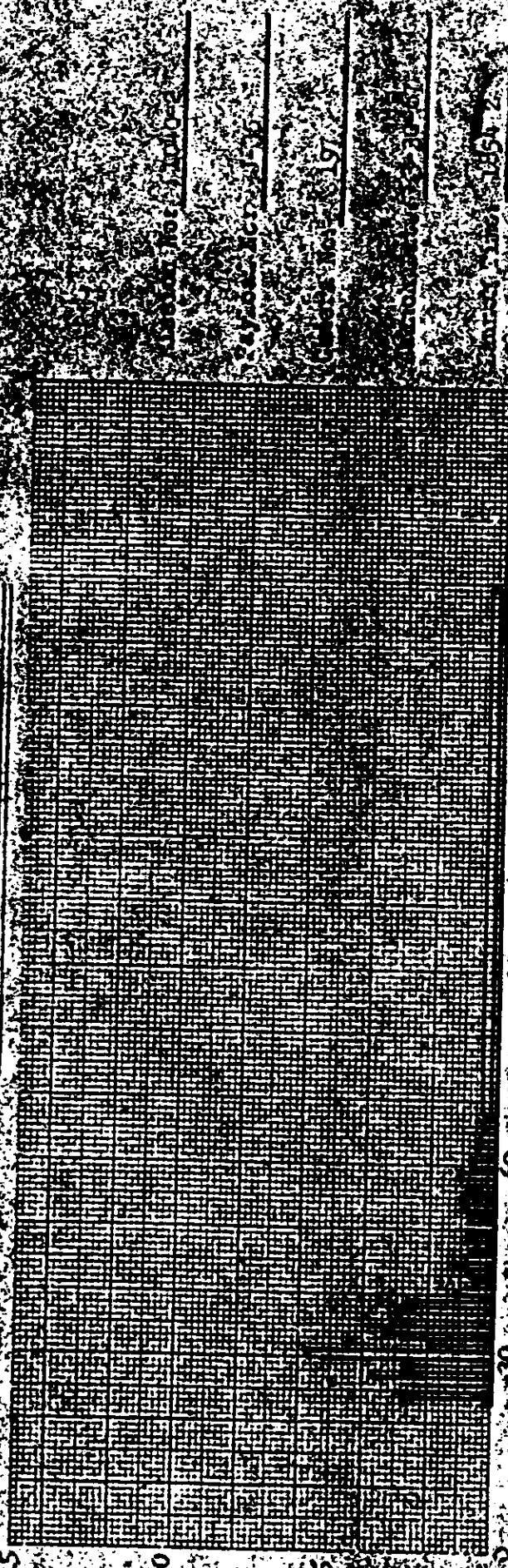


FIGURE C

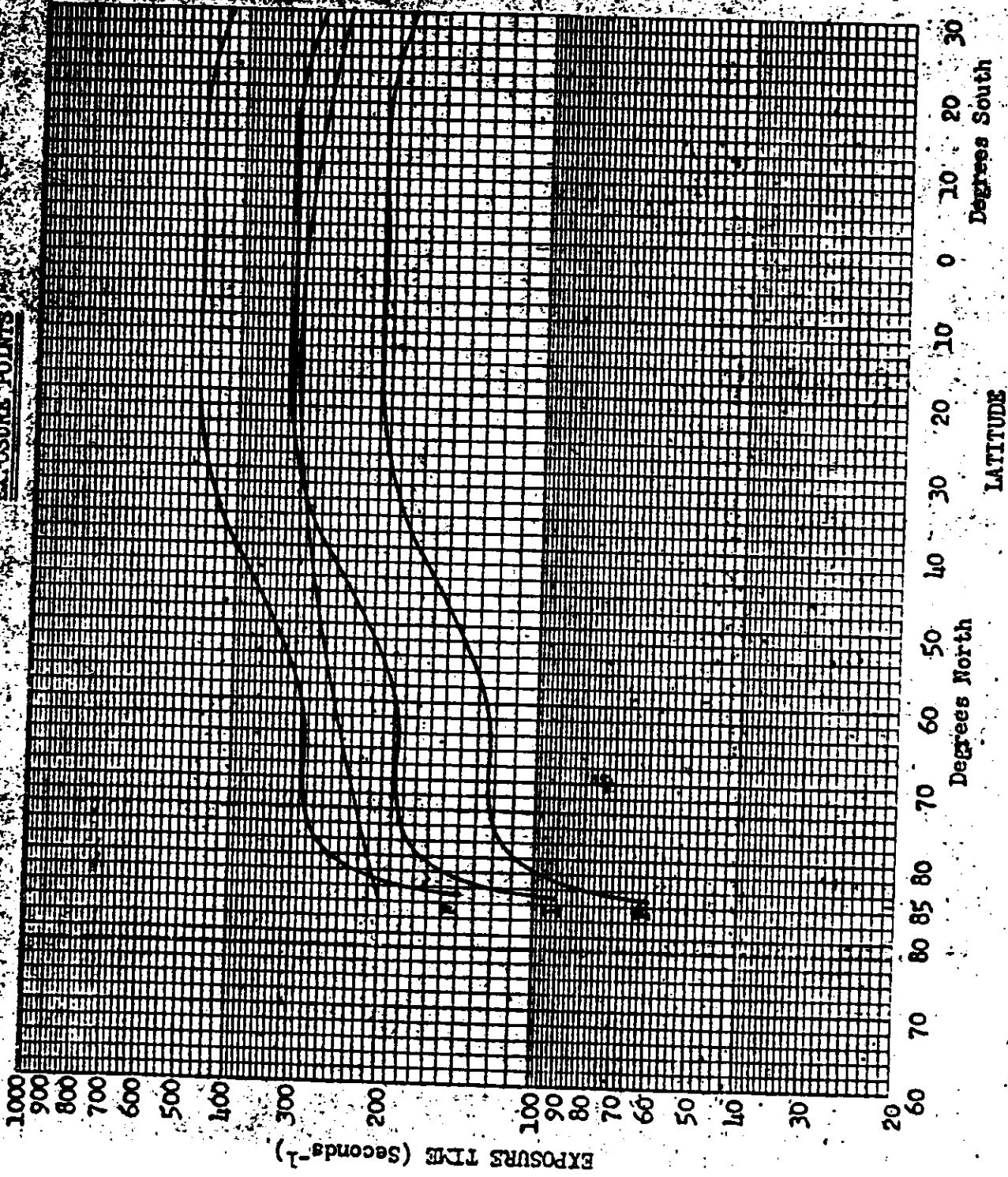
POSITIVE SOLAR AZIMUTH FREQUENCY

20

C

C

~~EXPOSURE POINTS~~



EXPOSURE POINTS

1000

900

800

700

600

500

400

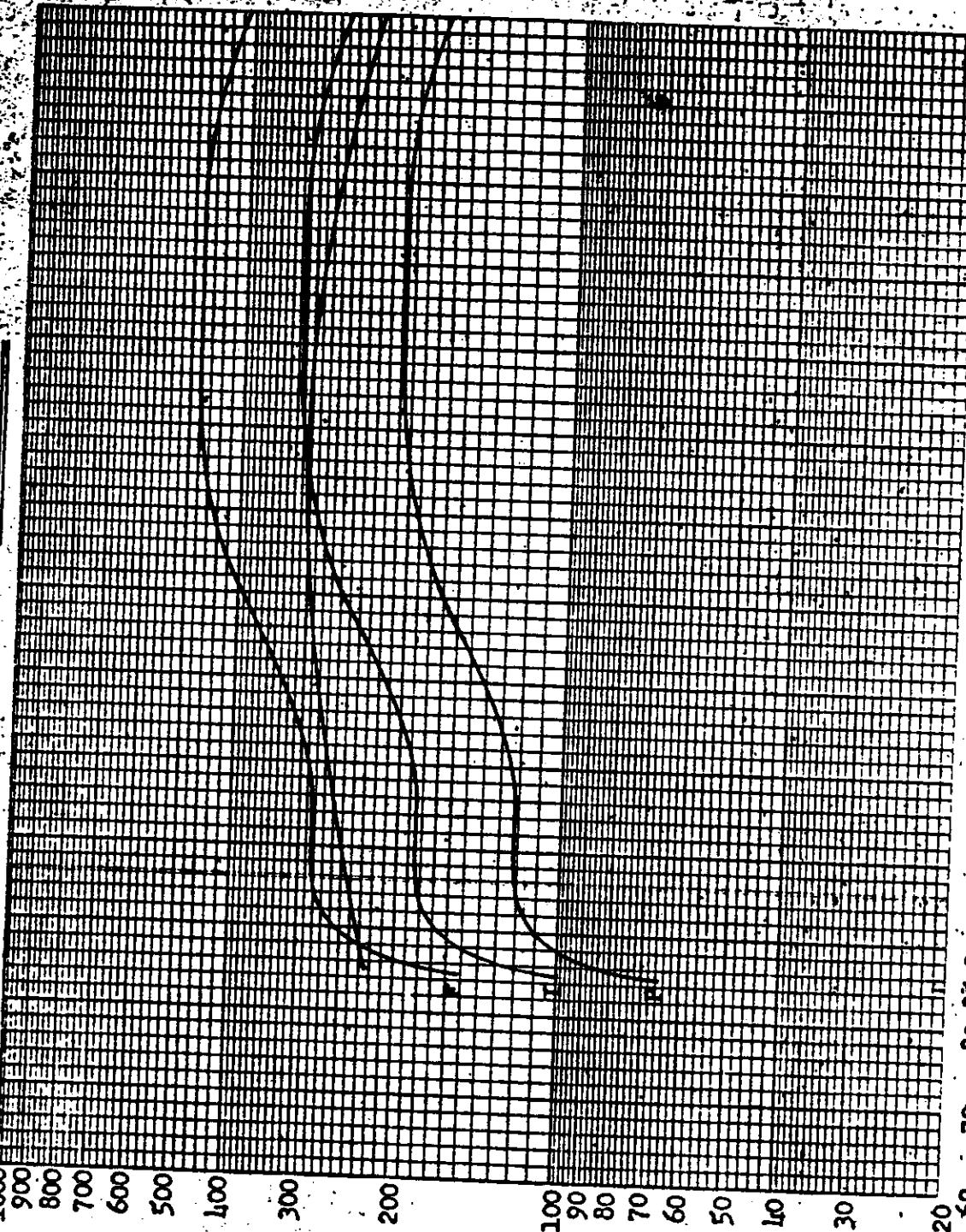
300

200

100

0

EXPOSURE TIME (Seconds⁻¹)



Mission No: 100

Payload No: J-32

Camera No: #197

Pass No: 19

Launch Date: 3/30/67

Launch Time: 1854 Z

Slit Width: .225

Filter Type: Watten 2K

SLR Type: 3101

* FORWARD LOOKING

FIGURE

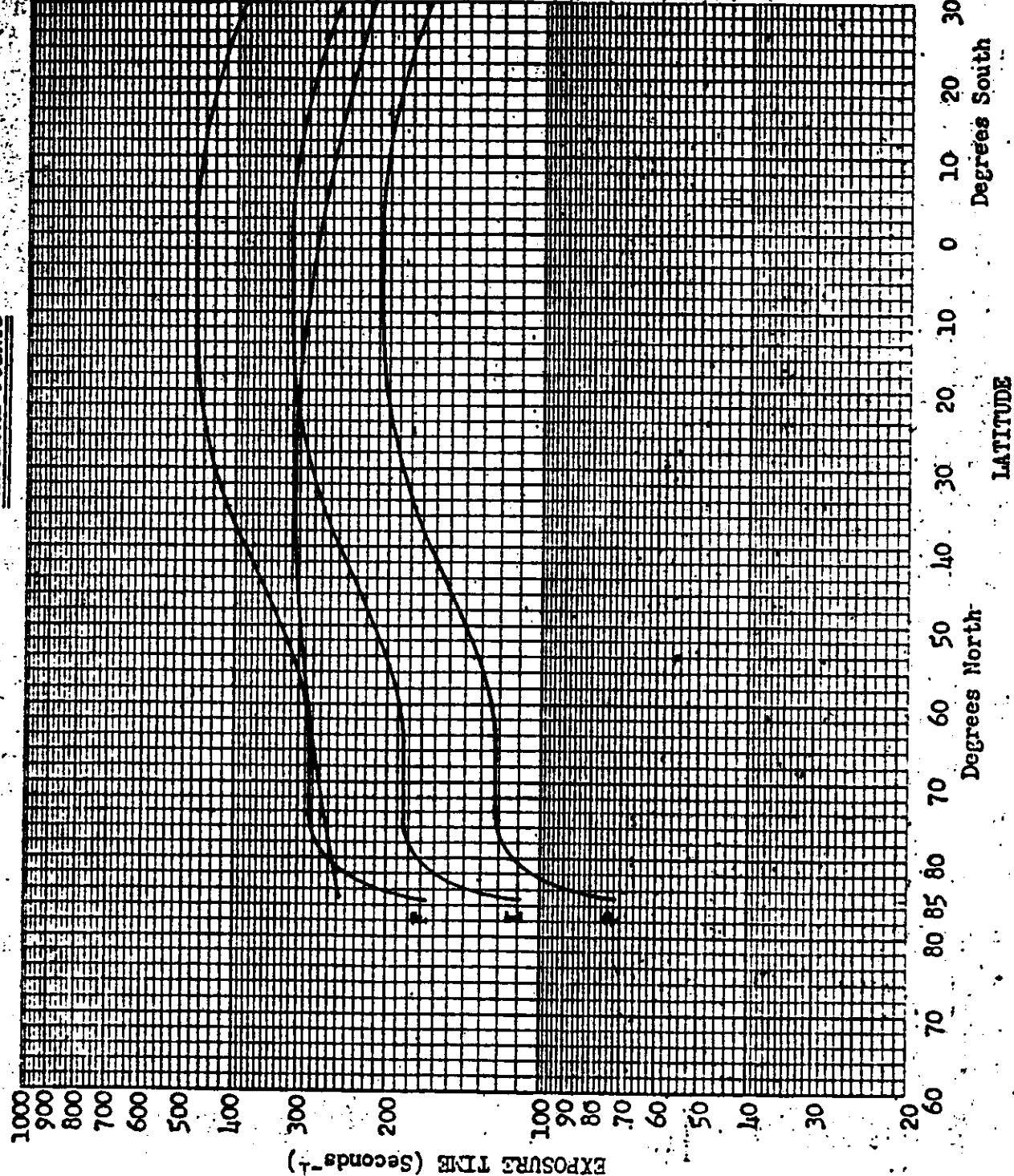
Degrees South:

Degrees North

LATITUDE

PRINTED

EXPOSURE POINTS



Mission No: 1010

Payload No: J-35

Camera No: * 197

Pass No: 97

Launch Date: 3/30/67

Launch Time: 1854 Z

Split Width: 225

Filter Type: Gritten 231

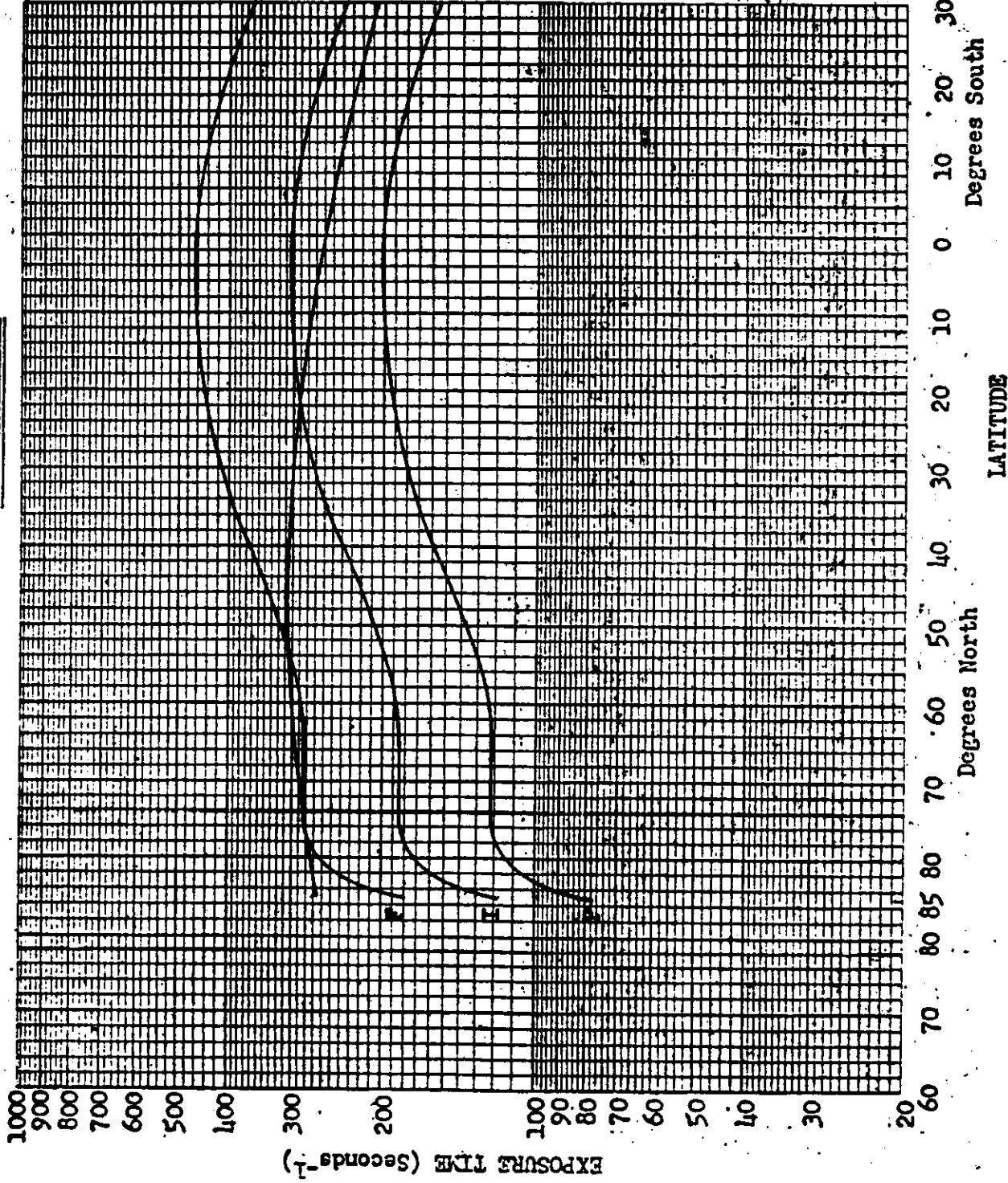
Fill Type: 3101

* FORWARD LOOKING

FIGURE 8-7

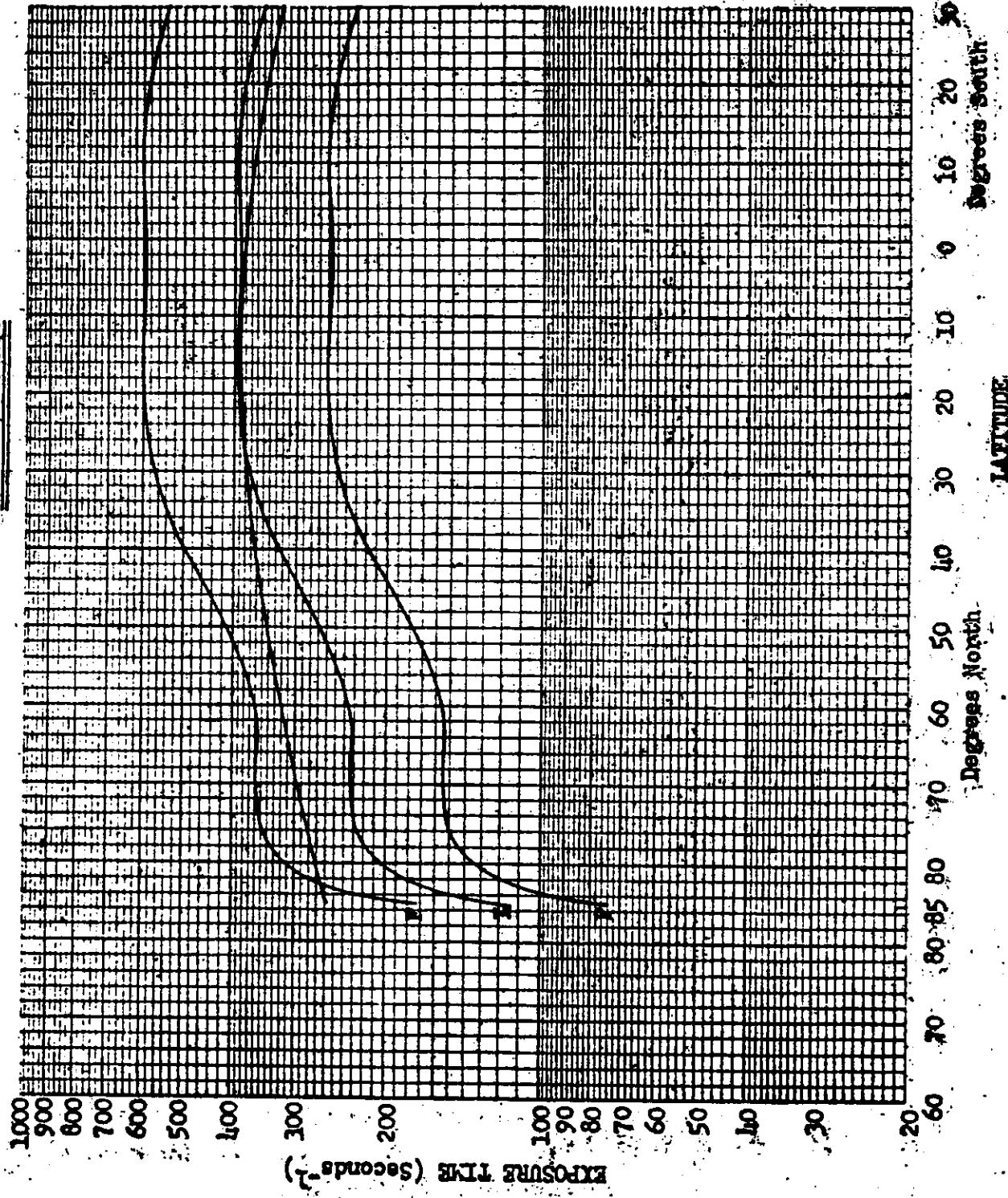
TOP SECRET

EXPOSURE POINTS



TOP SECRET

EXPOSURE POINTS



Mission No: 1040

Payload No: J-35

Camera No: * 196

Pass No: 1

Launch Date: 3/30/67

Launch Time: 1854 Z

Slit width: .175

Filter Type: Watten 21

Filter Type: 3404

* AFT LOOKING

FIGURE 8-9

TOE - SIGHTED

EXPOSURE POINTS

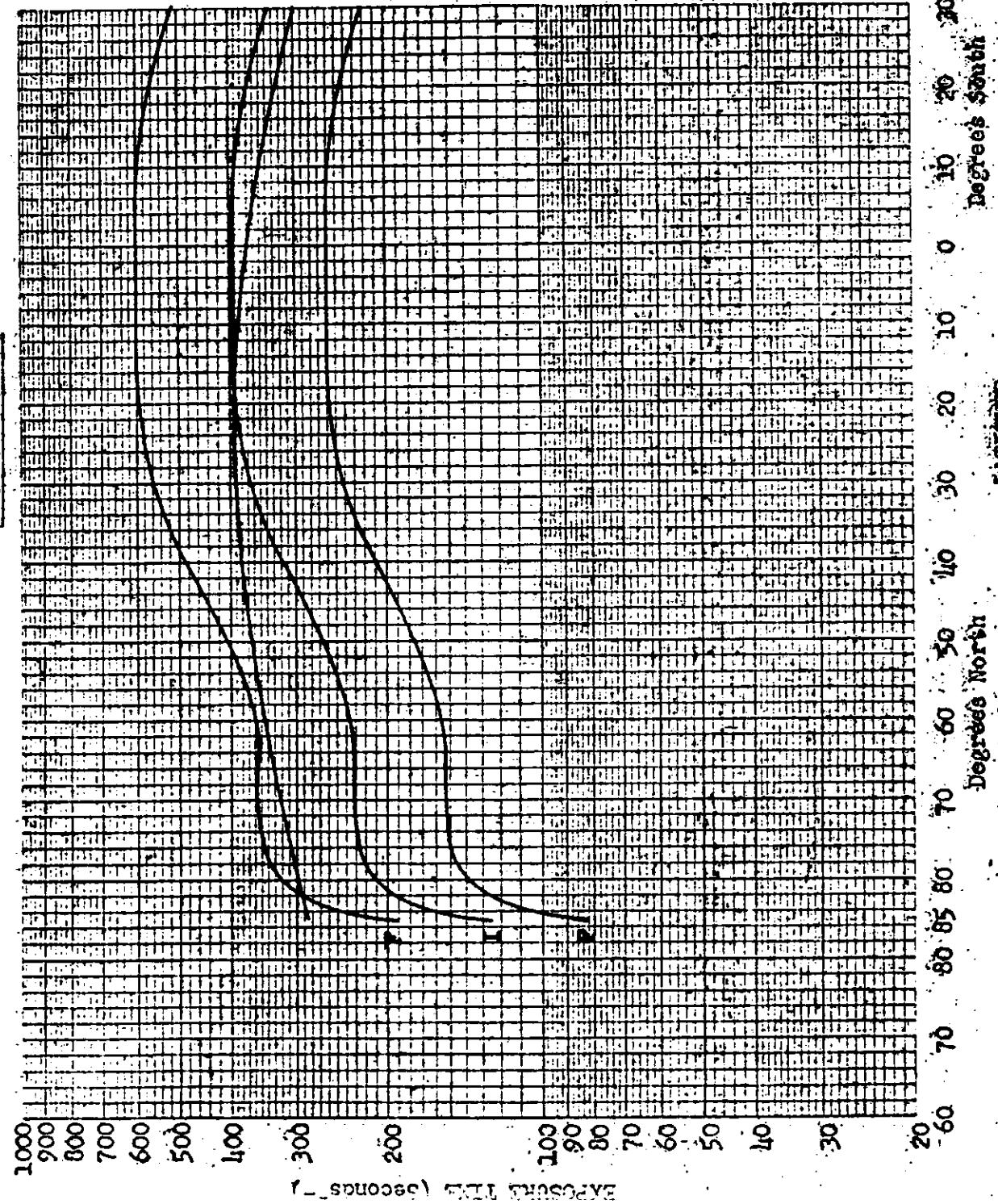
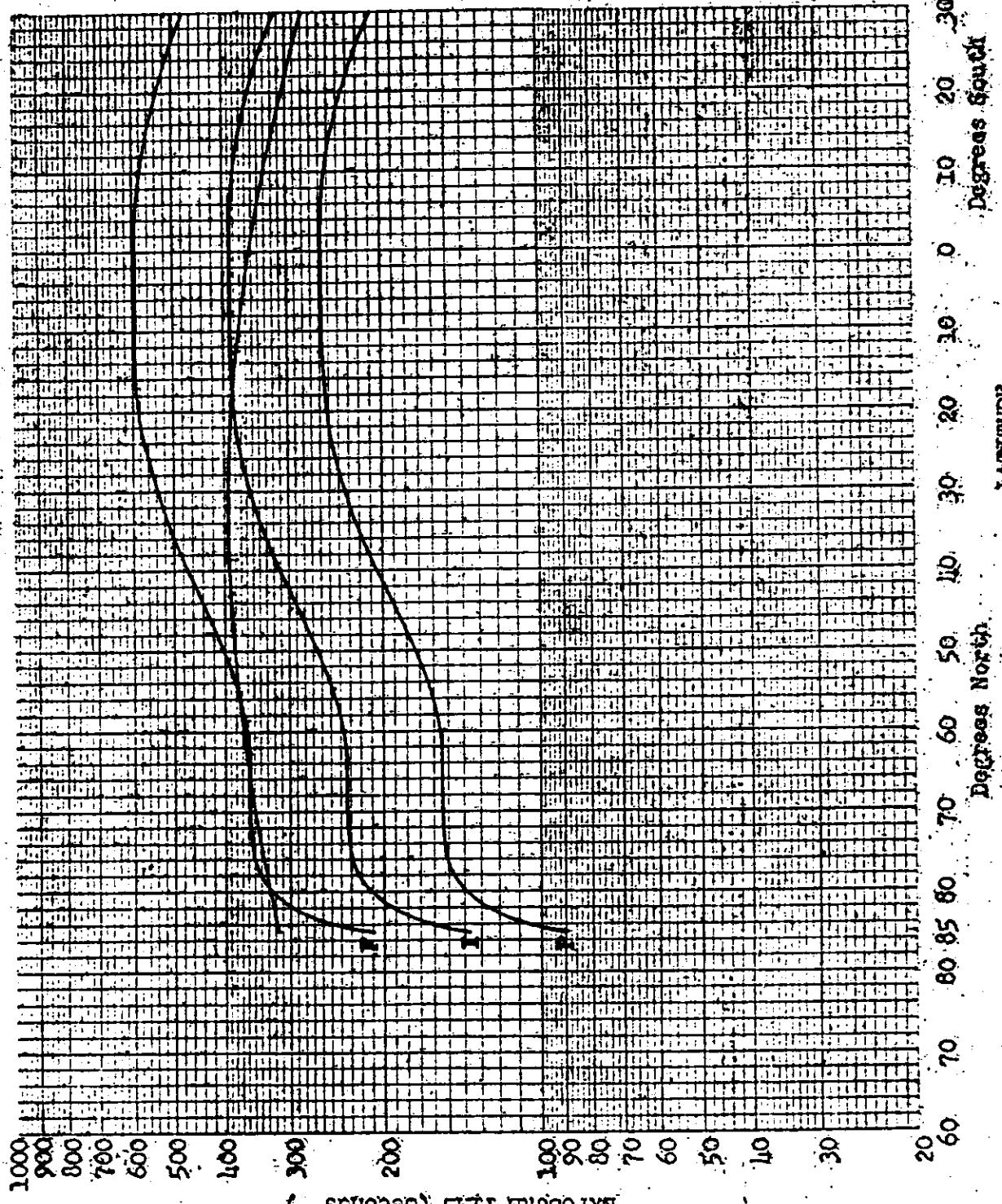


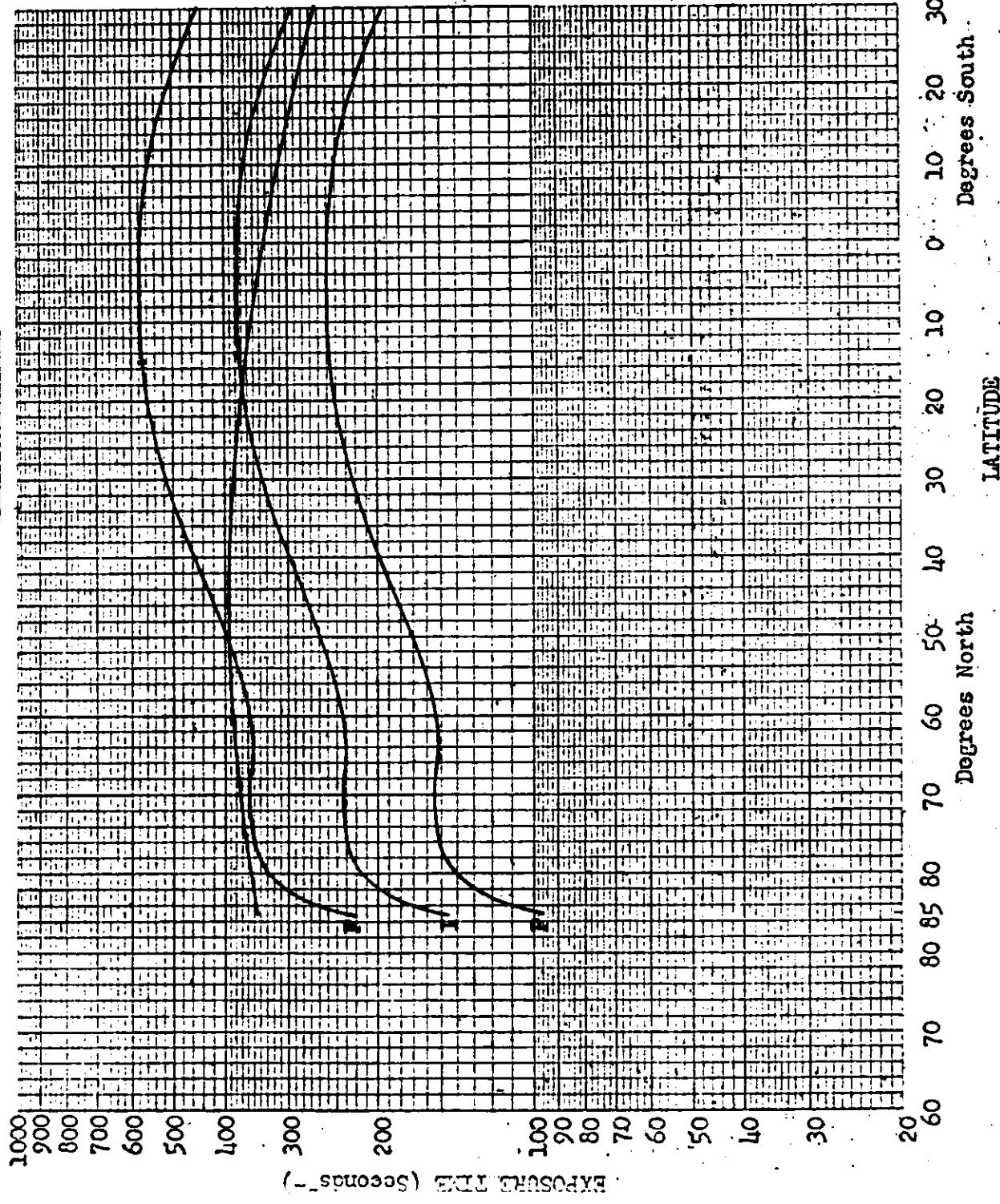
FIGURE 8-10

~~EXPOSURE POINTS~~



TOP-SECRET

EXPOSURE POINTS



SECTION 9

DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>	<u>Transition</u>
1040-1	FWD	Predicted	0	79	21	
		Reported	9	21	49	21
		Computed	2	35	63	
1040-1	AFT	Predicted	0	67	33	
		Reported	12	34	36	18
		Computed	2	53	45	
1040-2	FWD	Predicted	0	66	34	
		Reported	5	22	55	18
		Computed	3	29	68	
1040-2	AFT	Predicted	1	58	41	
		Reported	2	28	55	15
		Computed	0	32	68	

The tabulations of density frequency distributions for Missions 1040-1 and 1040-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution are computer plotted in Appendix A, Figures A-1 thru A-30.

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min criteria, (range) for proper exposure and processing is 0.10 to 0.90 density units. The area measured for D-Min is selected subjectively and is not necessarily the absolute D-Min in the photography.

A density range chart Figure 9-1 is included in this report. This type of chart for Missions 1004 to 1031 is included in the A/P final report for Mission 1031.

These charts are produced from the same density measurements previously mentioned in this section. The computer produced the mean, median and range figures for the various processing levels used. The chart includes the number of frames (samples) in which the density measurements were made. These measurements are made on approximately every tenth frame throughout the mission.

TOP SECRET C

MISSION 1040-1 INSTR - FWD
PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 3 0 PC
INTERMEDIATE 76 0 PC
FULL 1 1 PC
ALL LEVELS 216 0 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 6 0 PC
INTERMEDIATE 121 0 PC
FULL 3 3 PC
ALL LEVELS 103 1 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 6 0 PC
INTERMEDIATE 121 0 PC
FULL 3 3 PC
ALL LEVELS 230 1 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 6 0 PC
INTERMEDIATE 76 0 PC
FULL 2 2 PC
ALL LEVELS 258 1 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 6 0 PC
INTERMEDIATE 76 0 PC
FULL 2 2 PC
ALL LEVELS 258 3 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

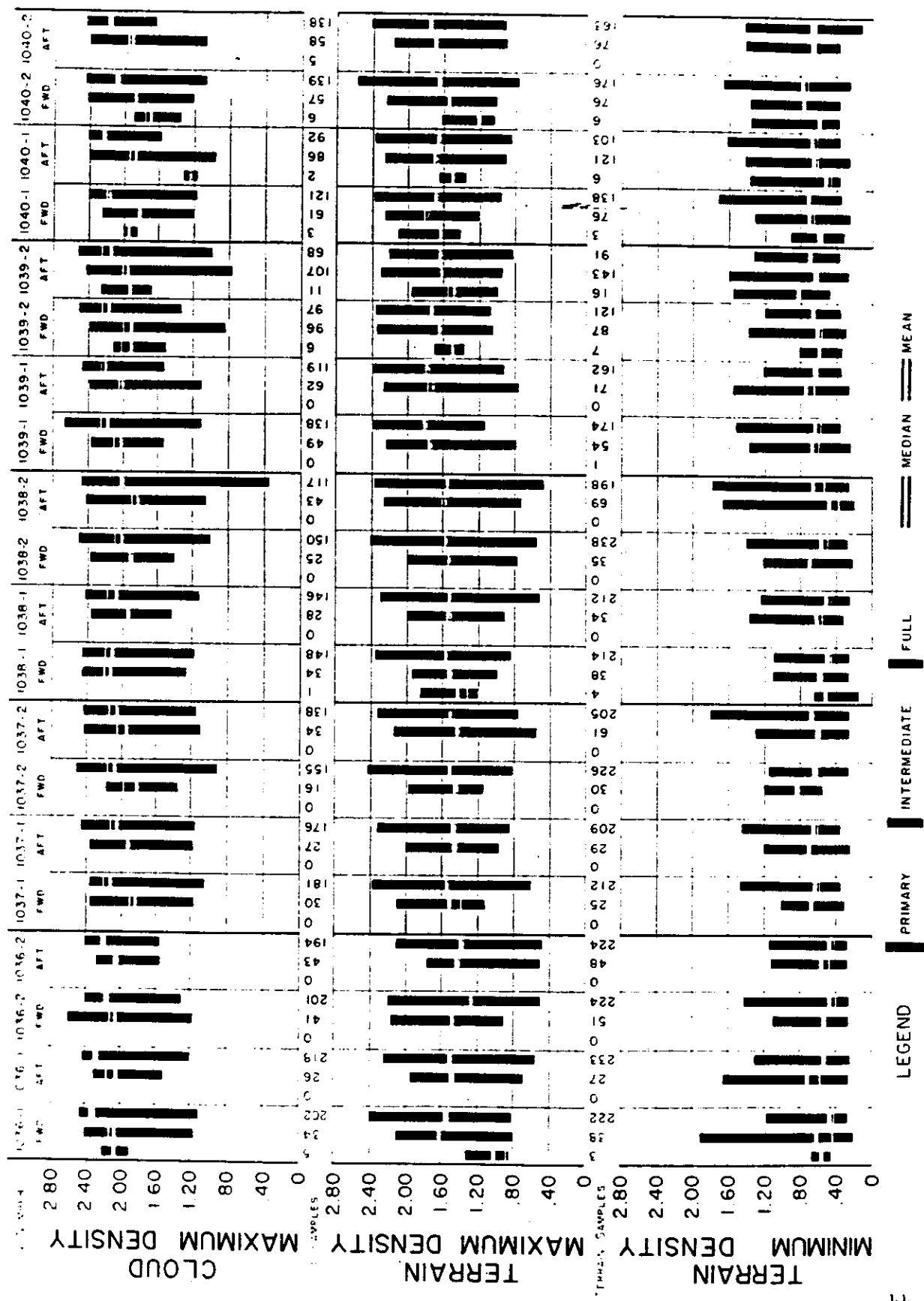
PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 0 0 PC
INTERMEDIATE 76 0 PC
FULL 3 3 PC
ALL LEVELS 239 2 PC
5/23/ PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED
PRIMARY 0.01-0.09 0.01-0.13
INTERMEDIATE 0.10-0.17 0.01-0.20
FULL 0.18 AND UP 0.01-0.39
5/23/ PROCESSING AND EXPOSURE ANALYSIS

TOP SECRET C

TABLE 9-1

J MISSION DENSITY RANGES



C [REDACTED]
SECTION 10

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1040-1 and 1040-2 received a MTF rating of 85. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF. The microdensitometer slit was 1 micron by 80 microns for the edge scan analysis.

<u>Mission</u>	<u>Camera</u>	<u>Cycles/mm</u>	<u>Average</u>	<u>Ground Resolution</u>
1040-1	FWD	94	70	17.6
1040-2	FWD	61		
1040-1	AFT	68	73	16.4
1040-2	AFT	75		

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not included in this report.

SECTION 11

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1040-1 and 1040-2 were derived from the reduction of the Stellar camera photography. This attitude date is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 11-1 through 11-6 show these distributions for Mission 1040-1 and Figures 11-7 through 11-12 for Mission 1040-2.

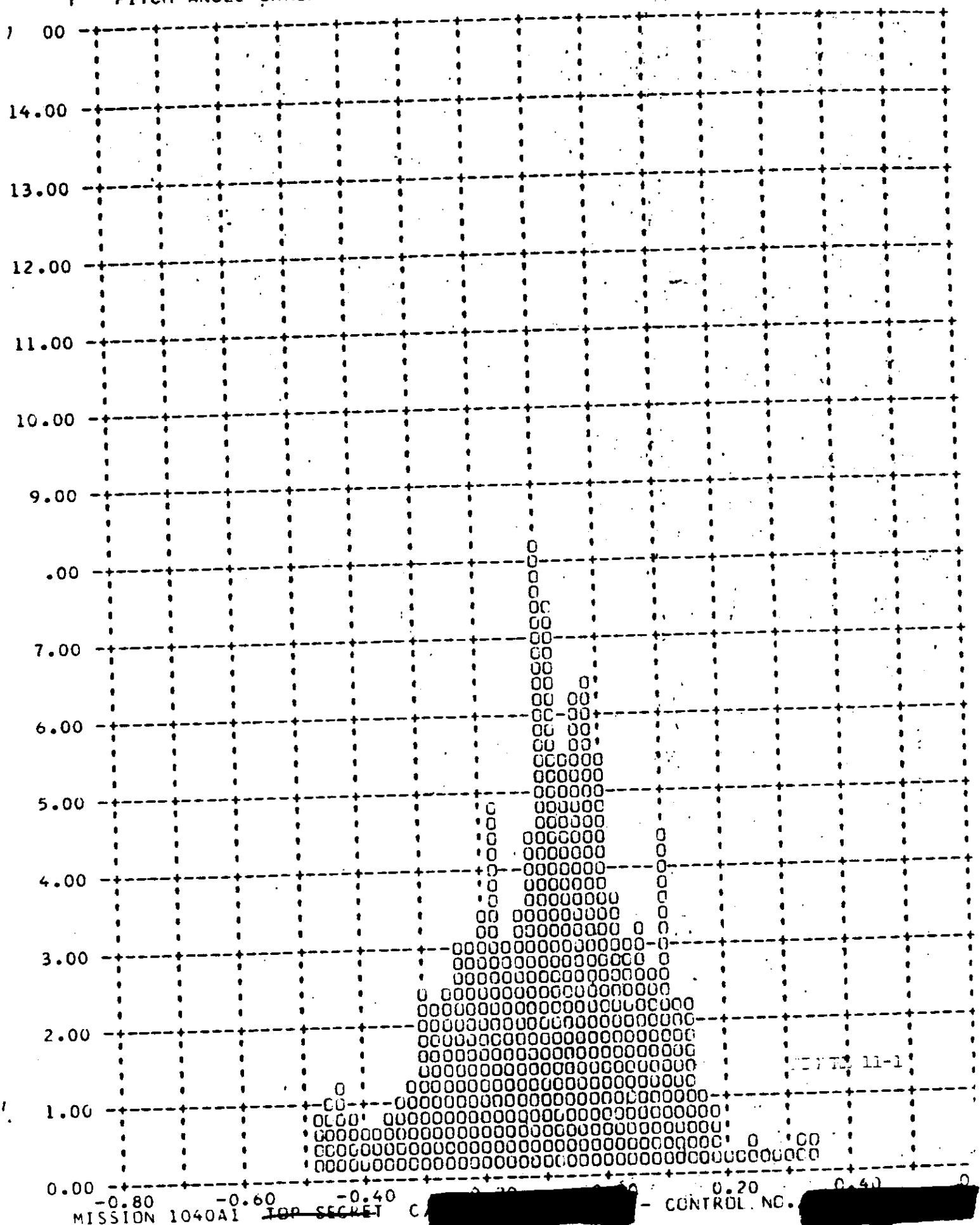
The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD camera photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

	Mission 1040-1 90%	Mission 1040-1 Range	Mission 1040-2 90%	Mission 1040-2 Range
Pitch Error ($^{\circ}$)	0.30	-0.46 to +0.34	0.29	-0.50 to +0.30
Roll Error ($^{\circ}$)	0.56	-0.66 to -0.15	0.46	-0.62 to +0.40
Yaw Error ($^{\circ}$)	2.99	-3.2 to +0.8	2.96	-3.2 to +0.60
Pitch Rate ($^{\circ}/hr.$)	22.12	-46 to +32	27.22	-60 to +38
Roll Rate ($^{\circ}/hr.$)	23.22	-38 to +98	26.47	-65 to +75
Yaw Rate ($^{\circ}/hr.$)	28.59	-84 to +32	28.74	-74 to +36

The performance of the attitude control system is comparable to the control systems used on recent missions. The panoramic photography was not degraded by the attitude control system.

FRAMES 1-5 OF 24

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1040AI TOP SECRET C

- CONTROL NO.

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

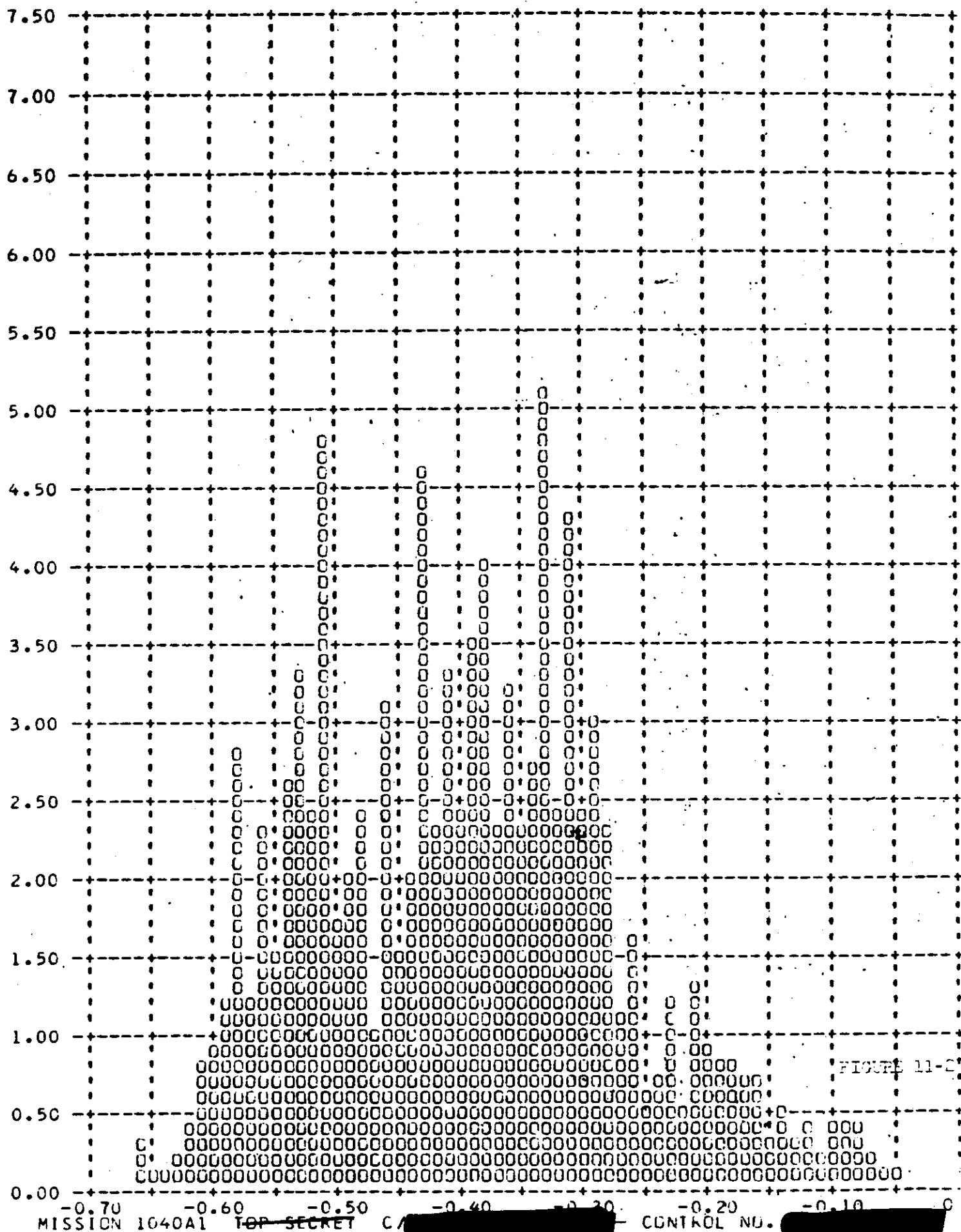


FIGURE 11-21

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

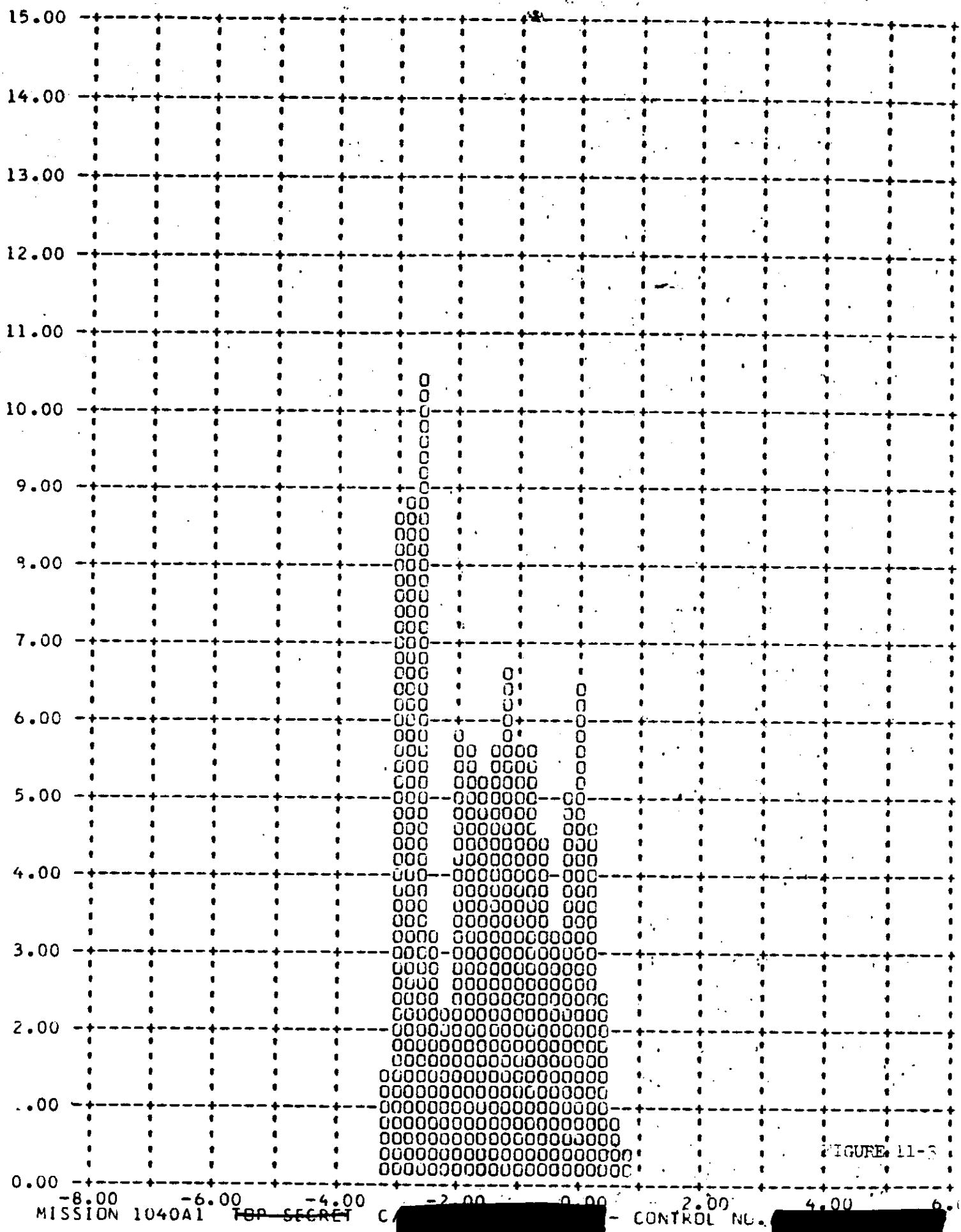
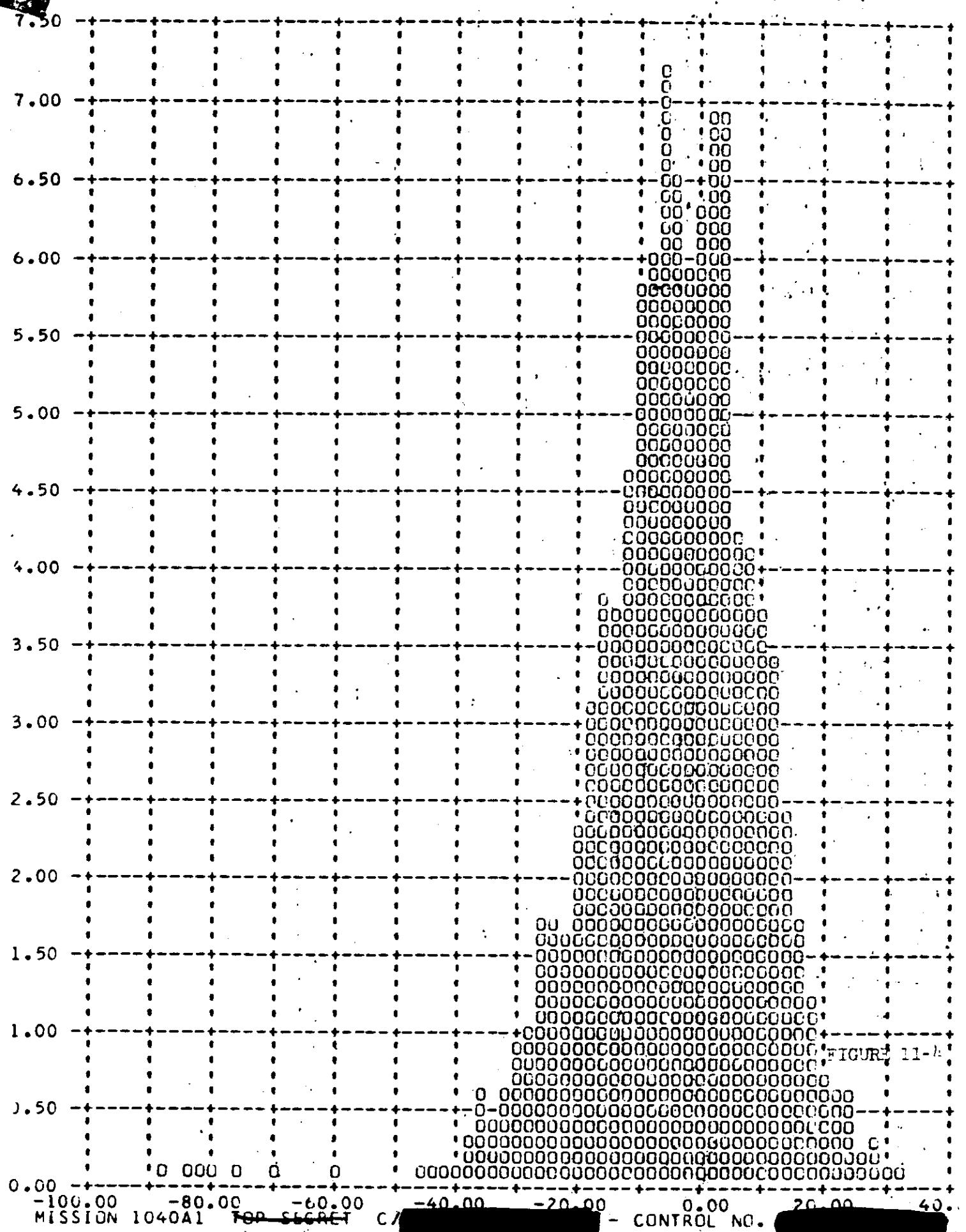


FIGURE 11-3

MISSION 1040A1 TBP SECRET C

CONTROL NO. [REDACTED]

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1040A1 TOP SECRET C/

- CONTROL NO. [REDACTED]

FIGURE 11-4

FRAMES 1-0 OF EACH OF

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

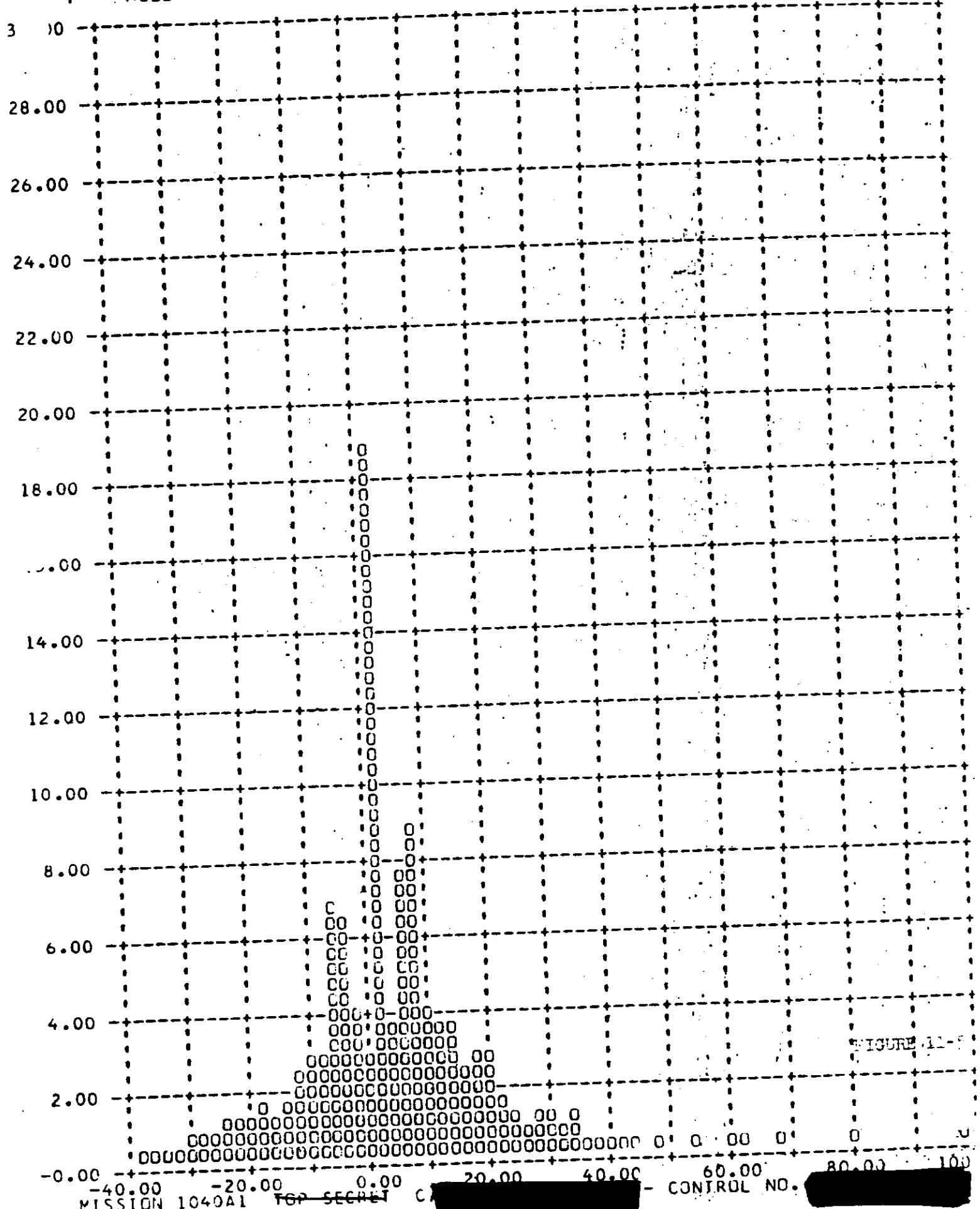


FIGURE 11-5

MISSION 1040A1

TOP SECRET

- CONTROL NO. [REDACTED] 100

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

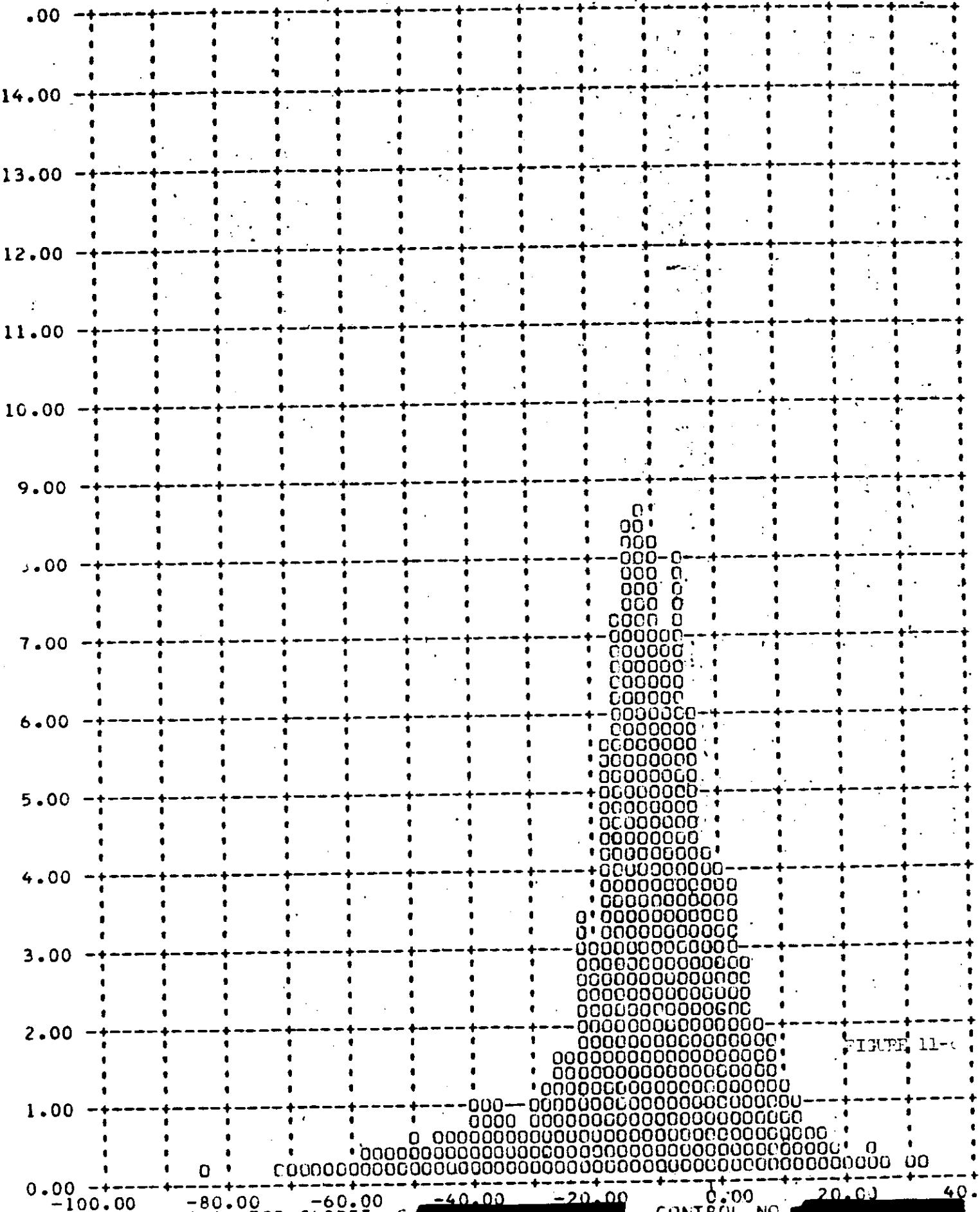
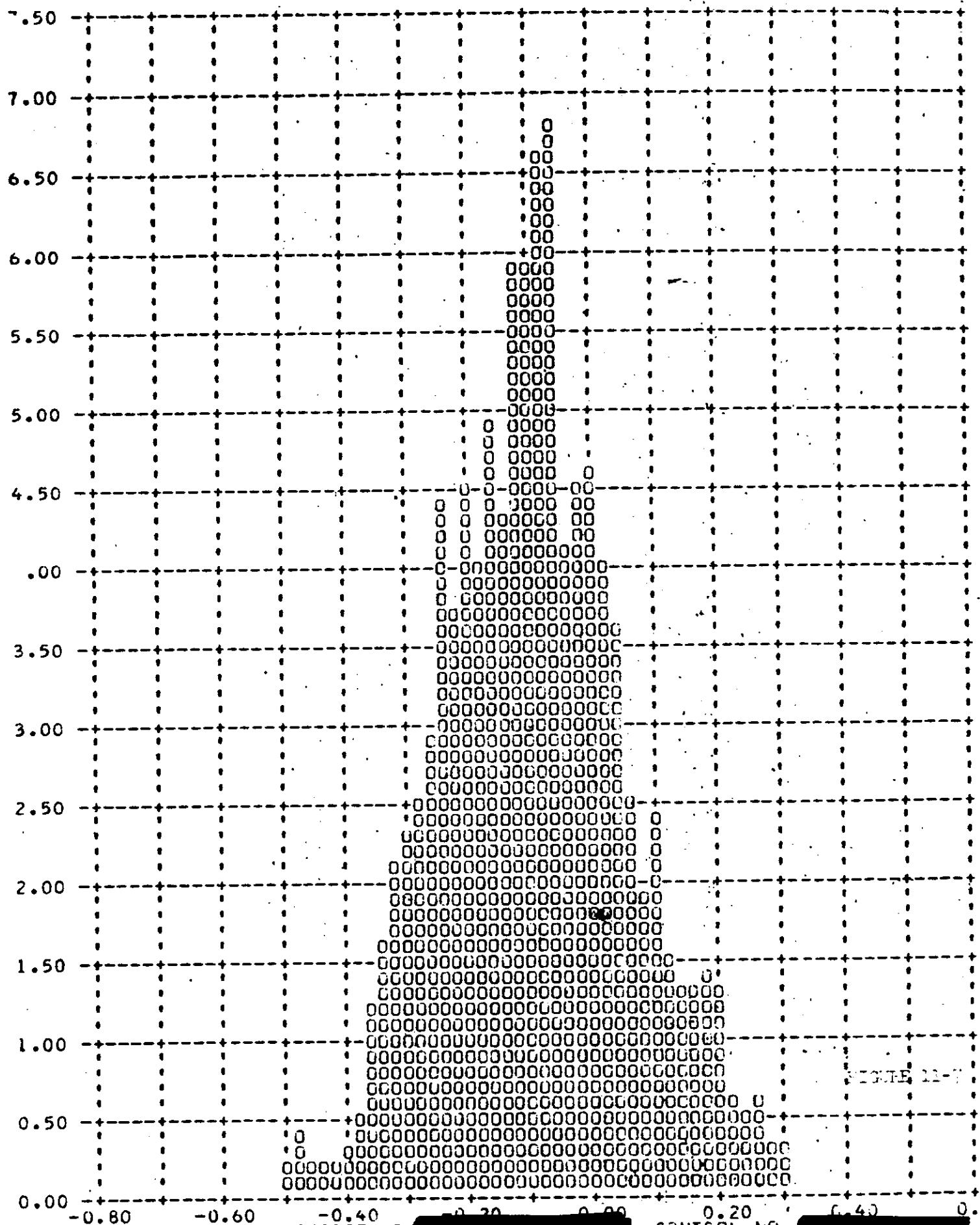


FIGURE 11-

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

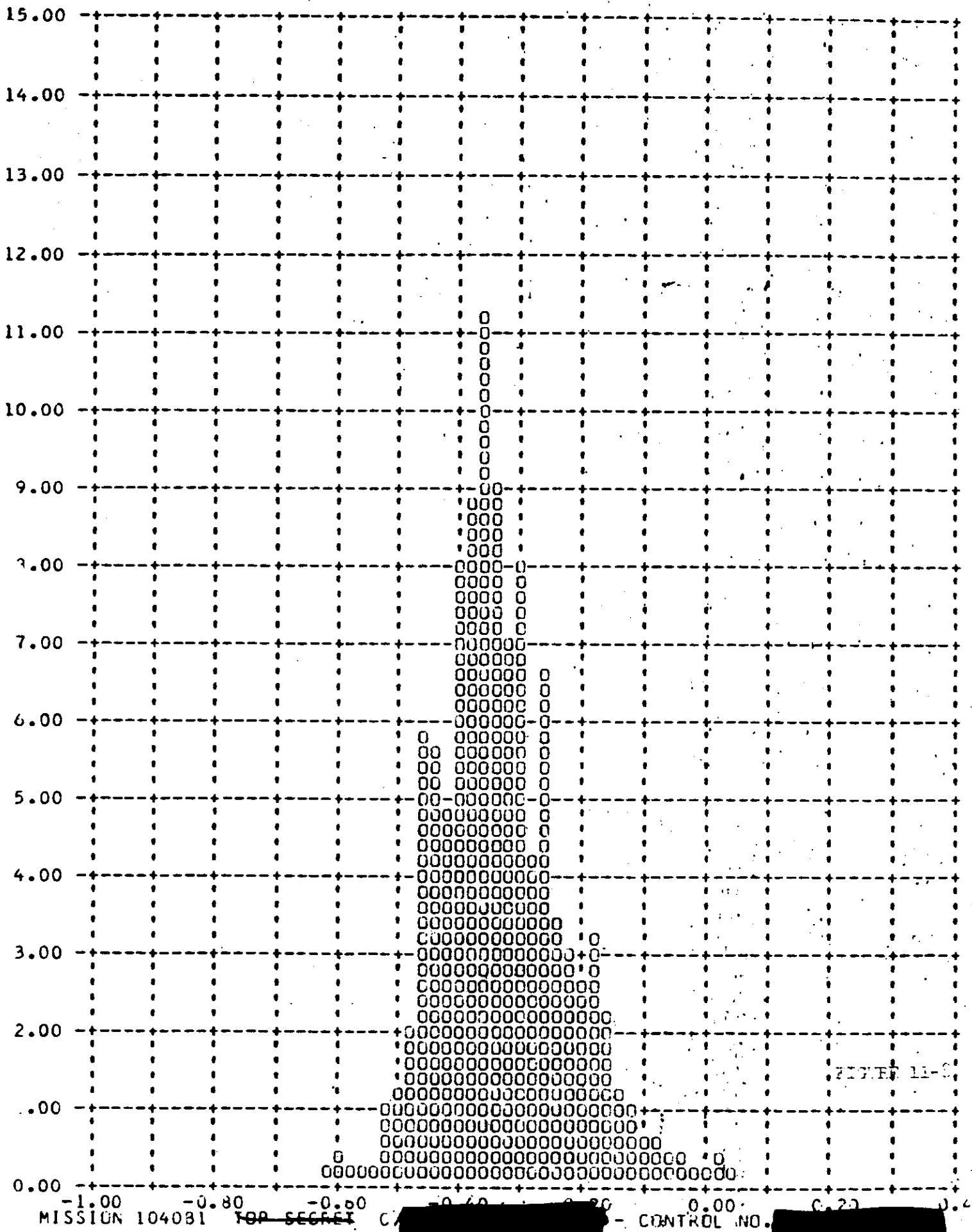


FIGURE 11-3

MISSION 104081 TOP SECRET C

CONTROL NO.

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

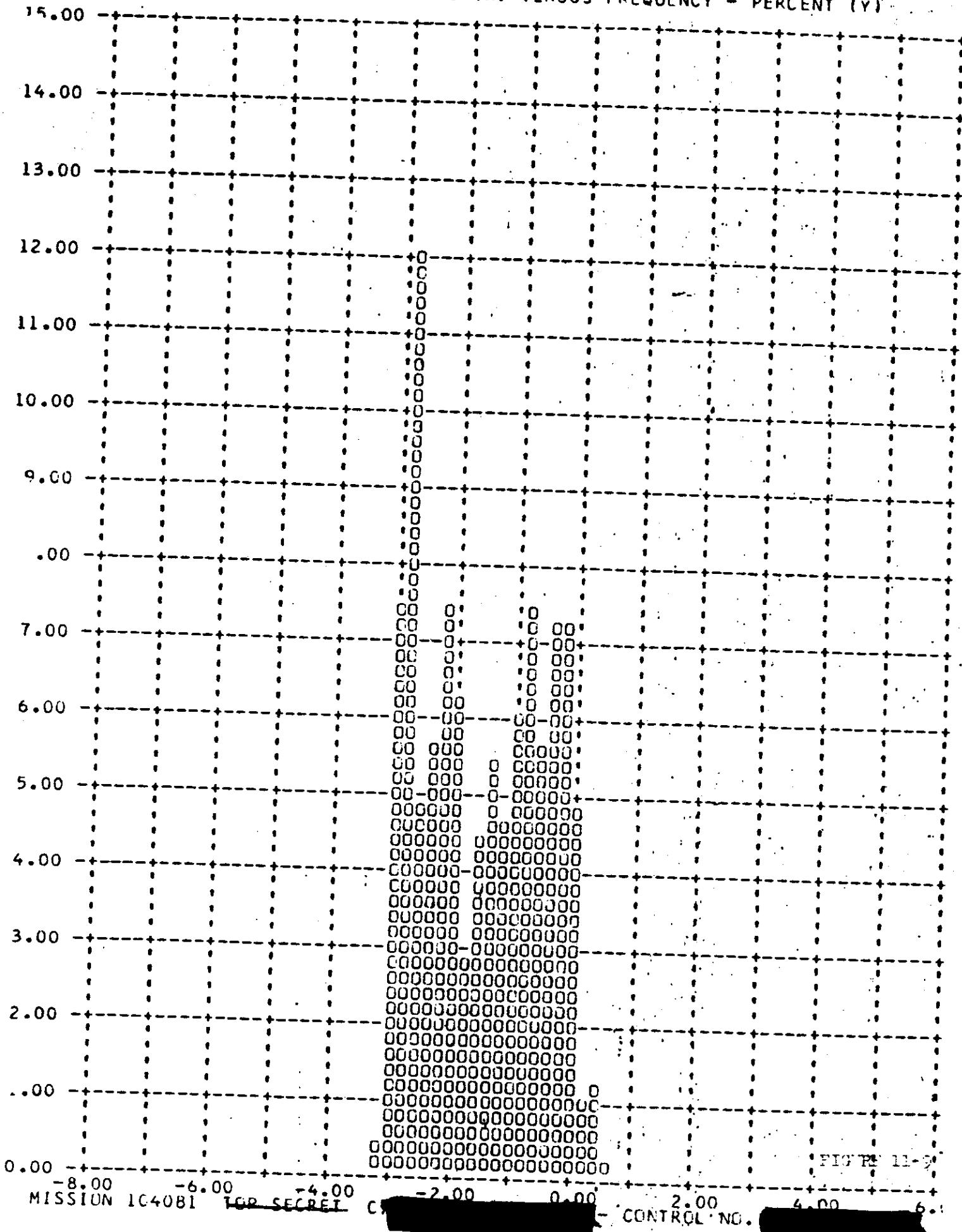


FIGURE 11-2

MISSION 1C4081

TOP SECRET

C

CONTROL NO.

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

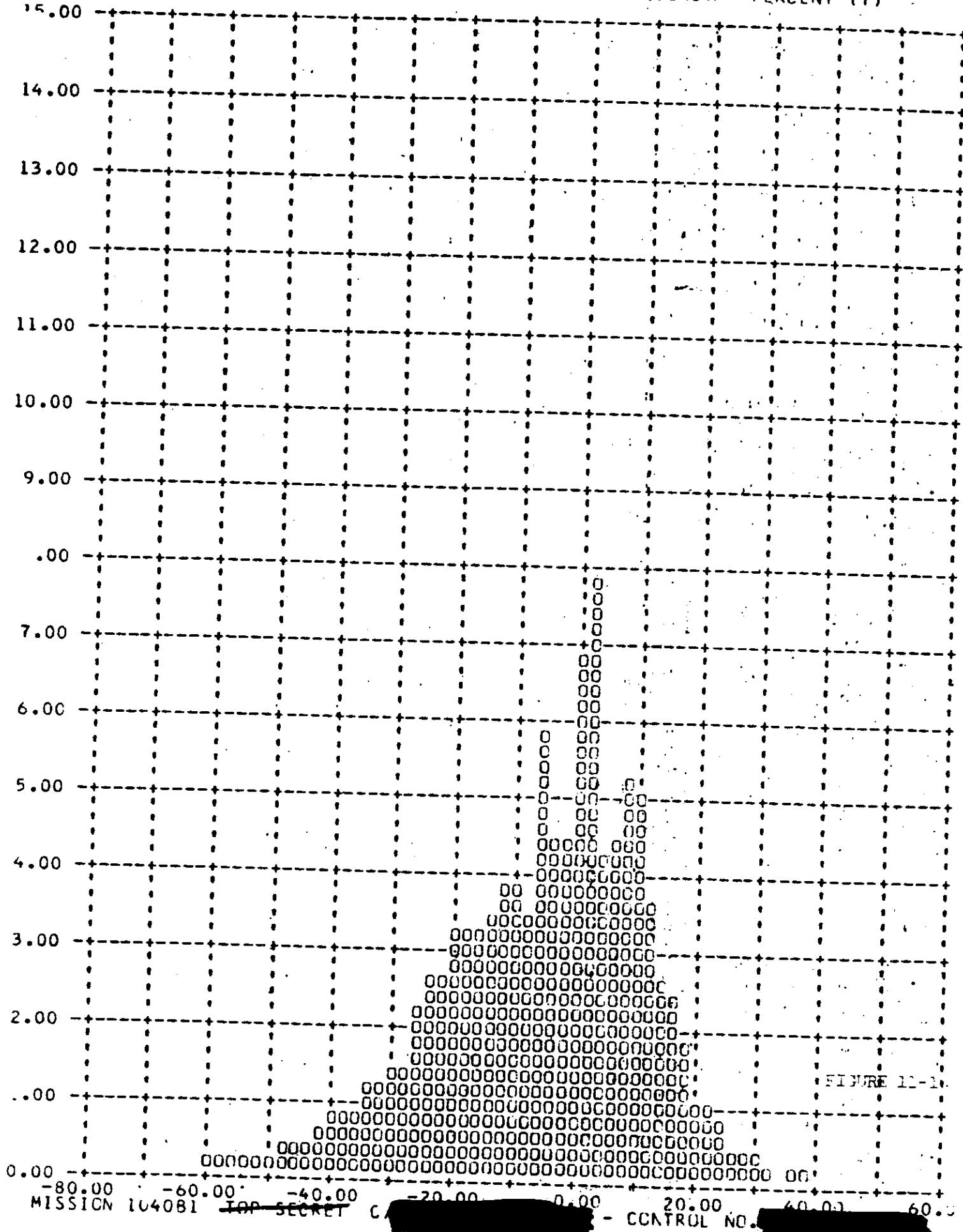


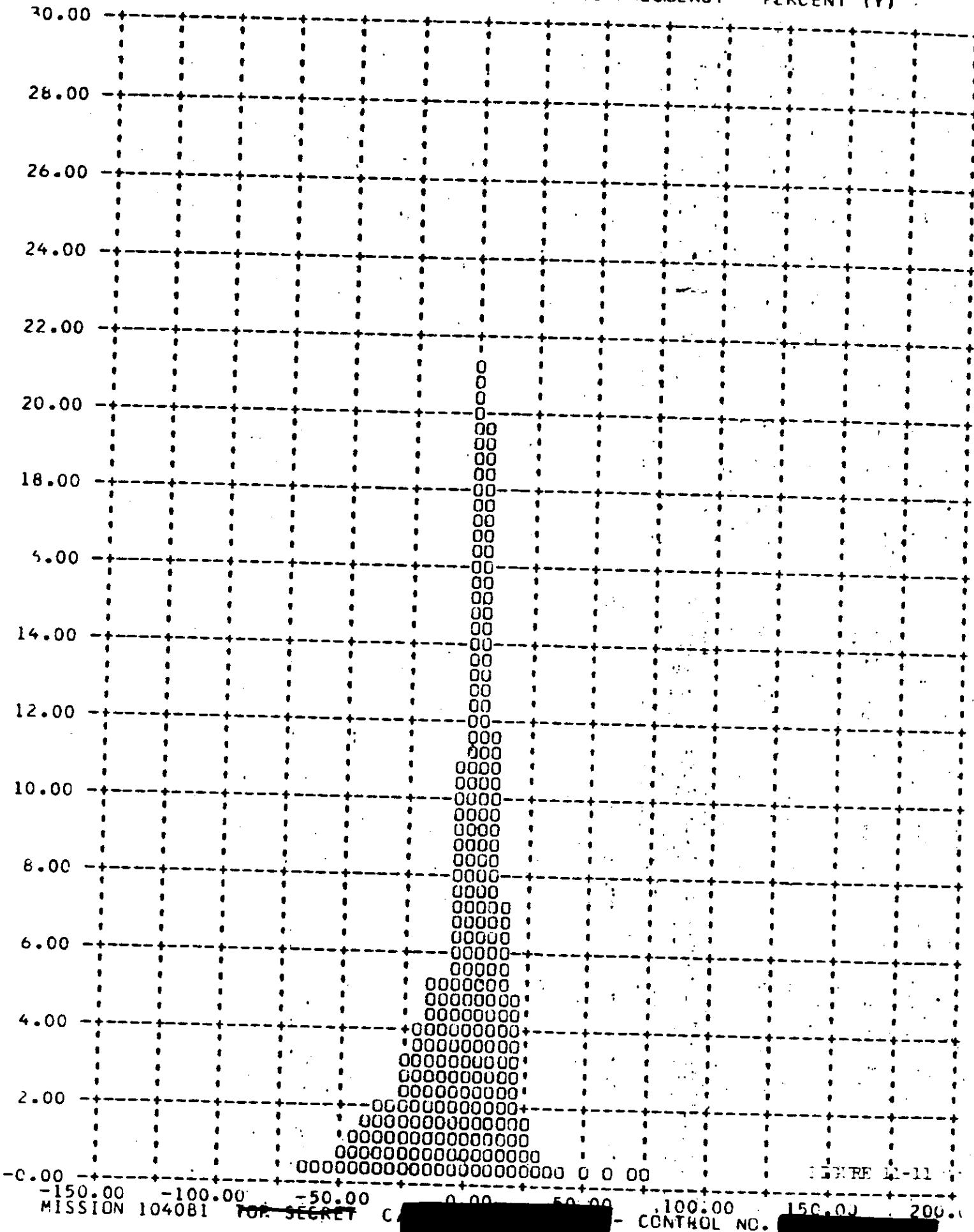
FIGURE 11-1

MISSION 104081

TAP SECRET C

- CONTROL NO.

ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 104081 FOR SECRET C - CONTROL NO.

FRAMES 1-6 OF EACH OF UNLIMITED 90 PERCENT = 20.0

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

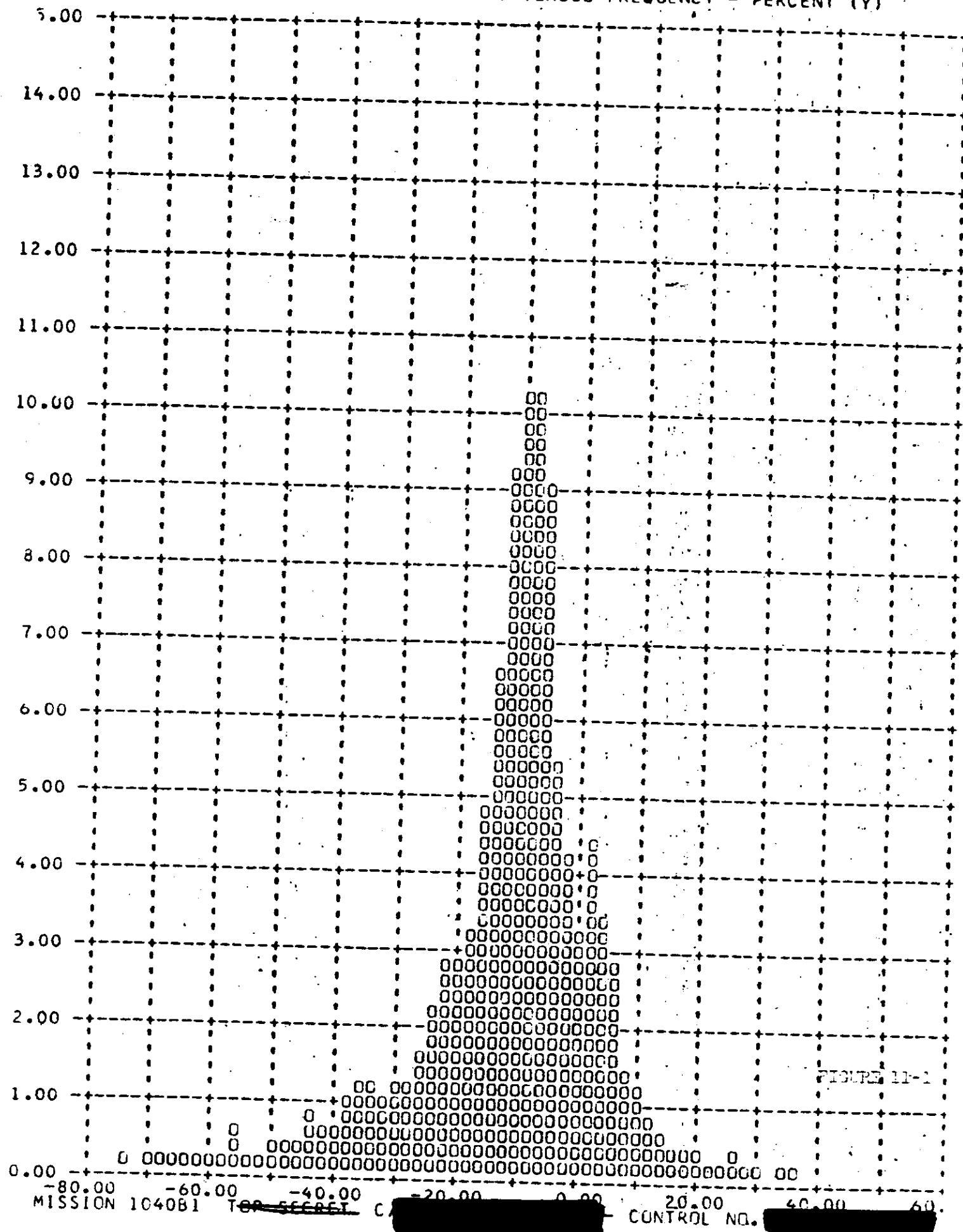


FIGURE 11-1

MISSION 1040B1 TOP SECRET C

CONTROL NO.

SECTION 12

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPTC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation of the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 12-1 through 12-16.

The summary table 12-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

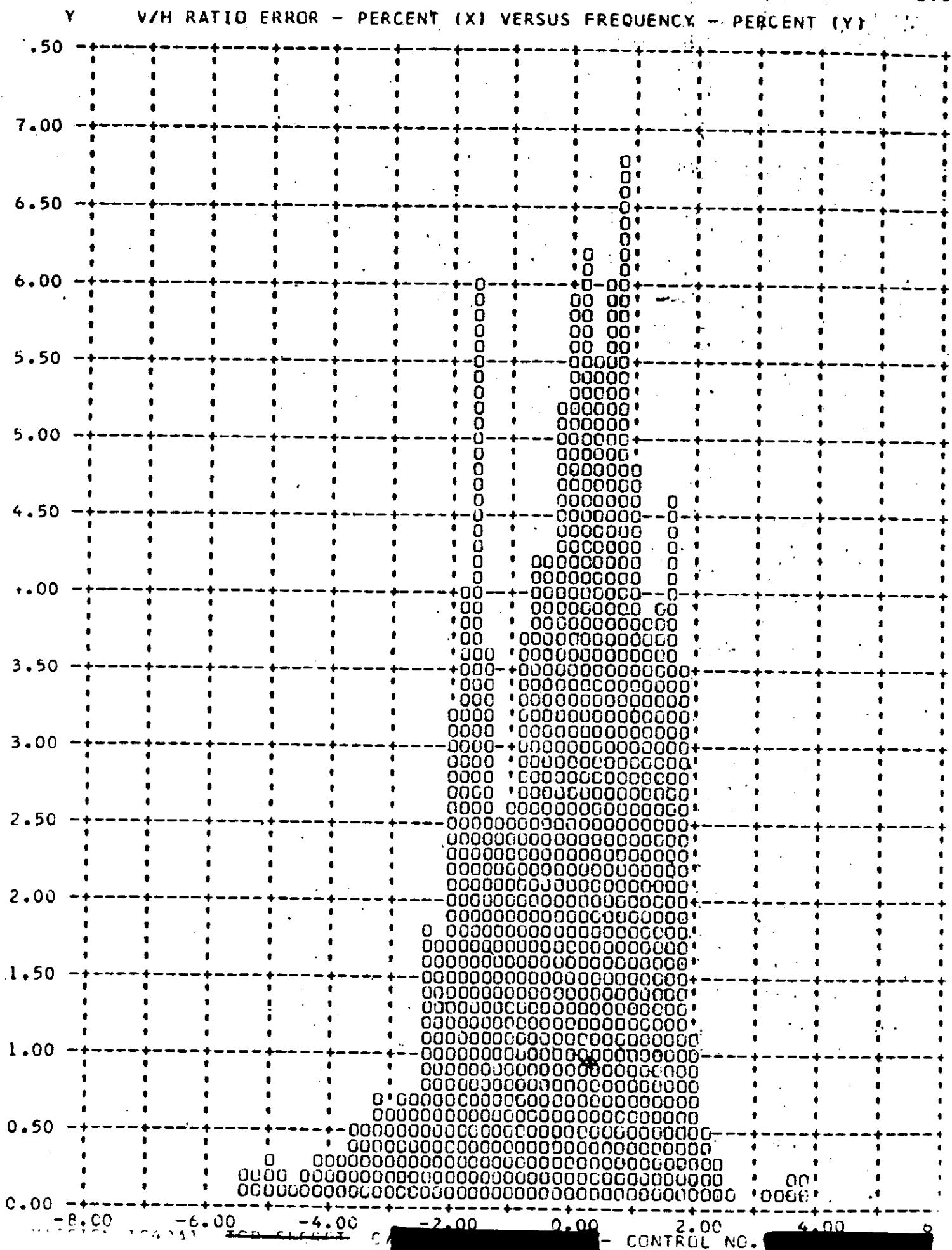
MISSION 1040
V/h RATIO AND RESOLUTION LIMITS

UNITS	CAMERA	MISSION 1040-1		MISSION 1040-2	
		20%	Range	20%	Range
V/h Ratio Error	%	2.67	-3.0 to +5.8	1.66	-3.2 to +7.2
Along Track Resolution Limit	Feet	2.15	-5.2 to +3.8	2.72	-5.6 to +5.8
Cross Track Resolution Limit	Feet	3.95	0.2 to 9.8	2.20	0.2 to 12.6
	FWD	1.99	0.2 to 5.4	2.54	0.2 to 7.6
	AFT	2.19	0.2 to 3.8	2.05	0.05 to 2.8
	AFT	2.53	0.2 to 4.6	2.28	0.2 to 3.6

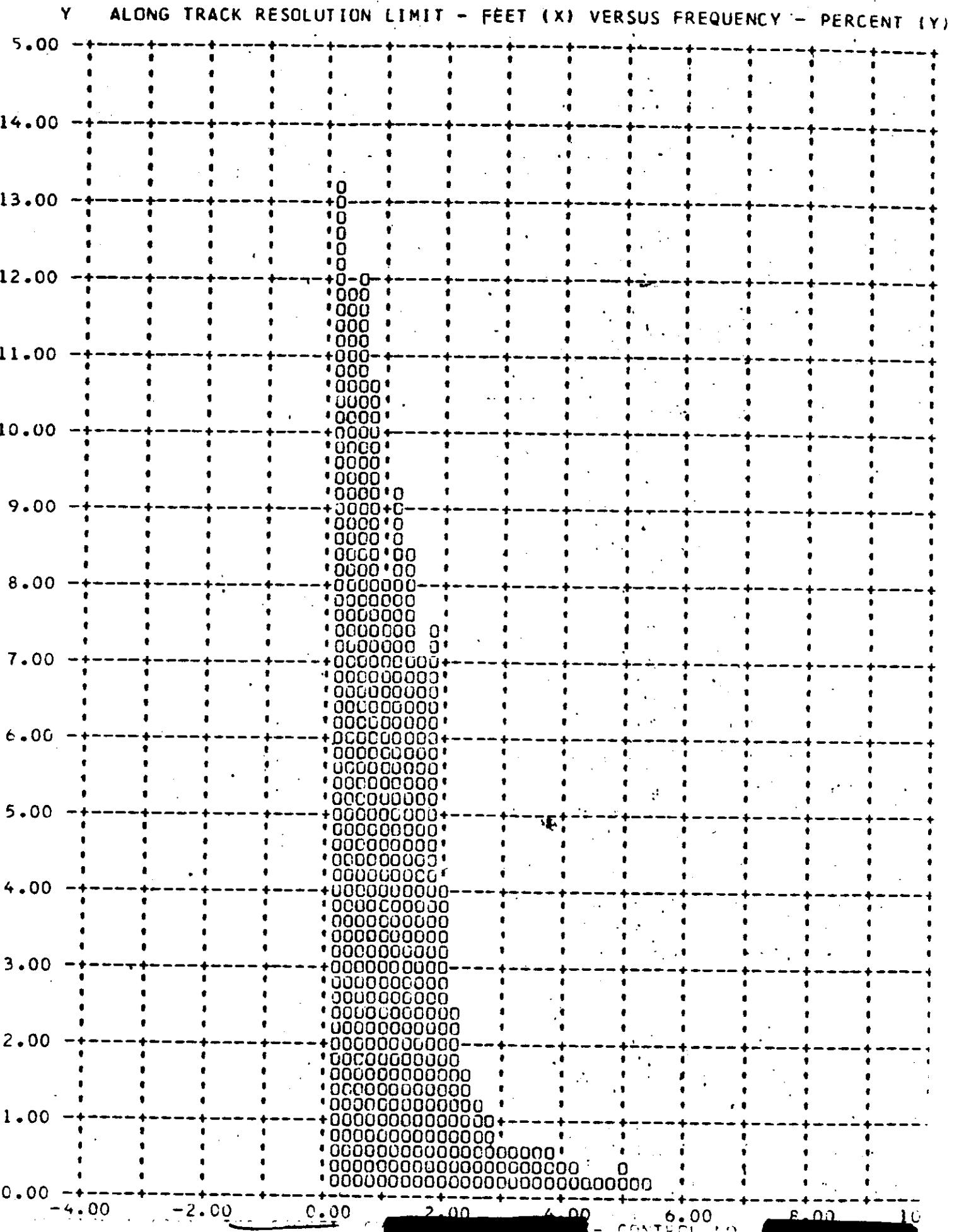
TABLE 12-1

MISSION 1C40A1 TOP SECRET

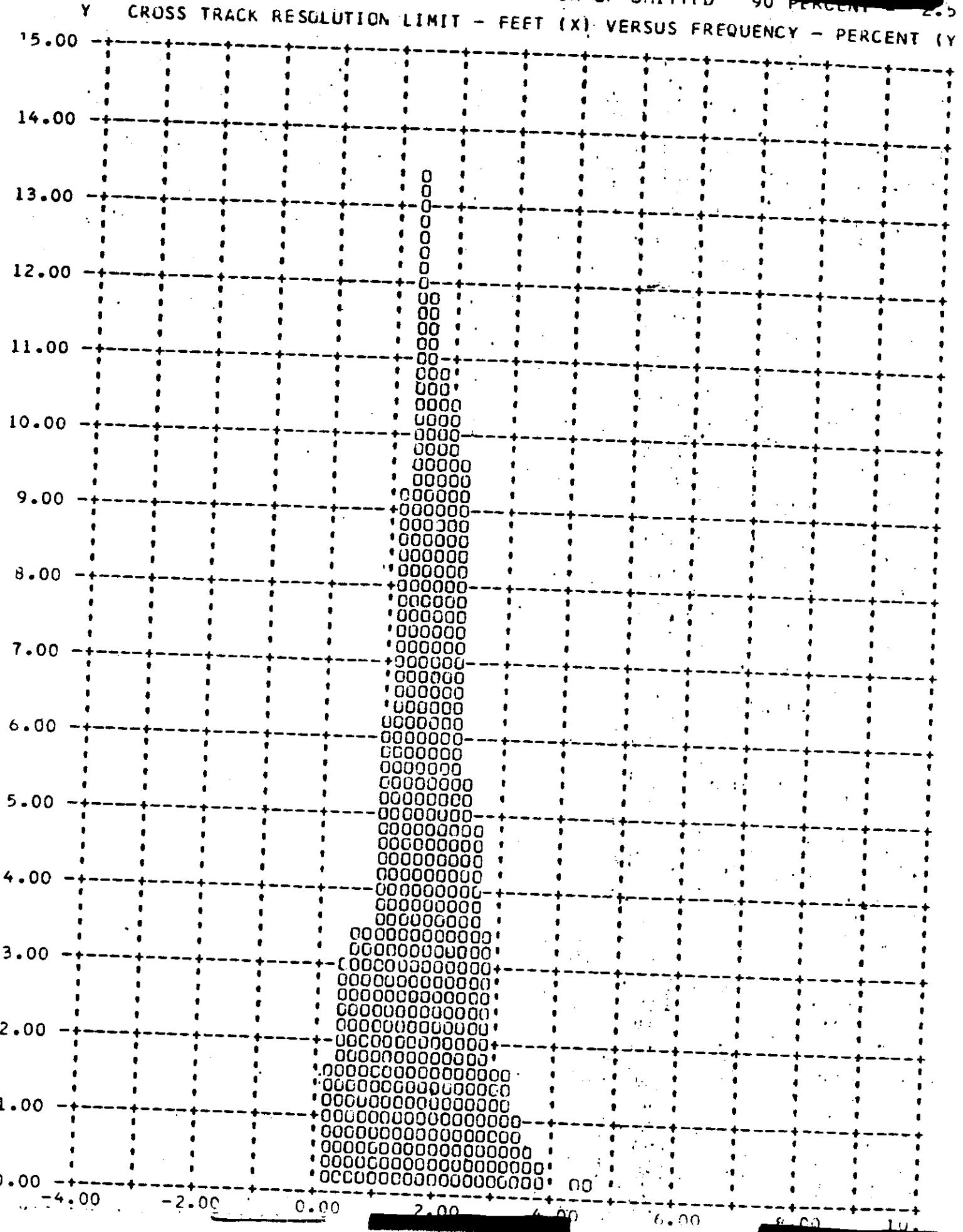
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT 2.12



MISSION 1040A1 T-6 SECRET C-1 CONTROL NO. [REDACTED] - 90 PERCENT = 1.95
FRAMES 1-6 OF EACH UP OMITTED

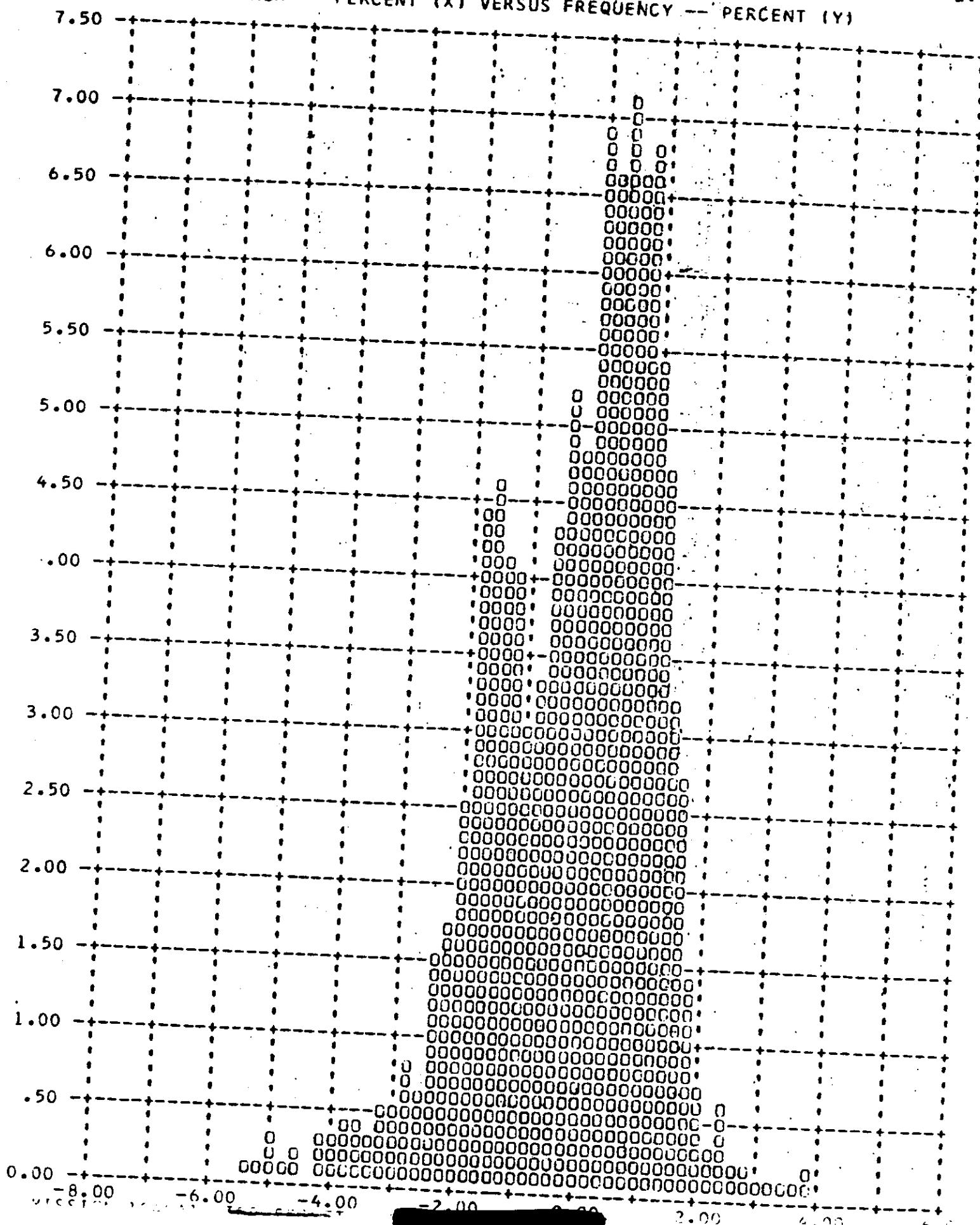


MISSION 1040A1 TOP SECRET C - CONTROL NO. [REDACTED] -
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT 2.5



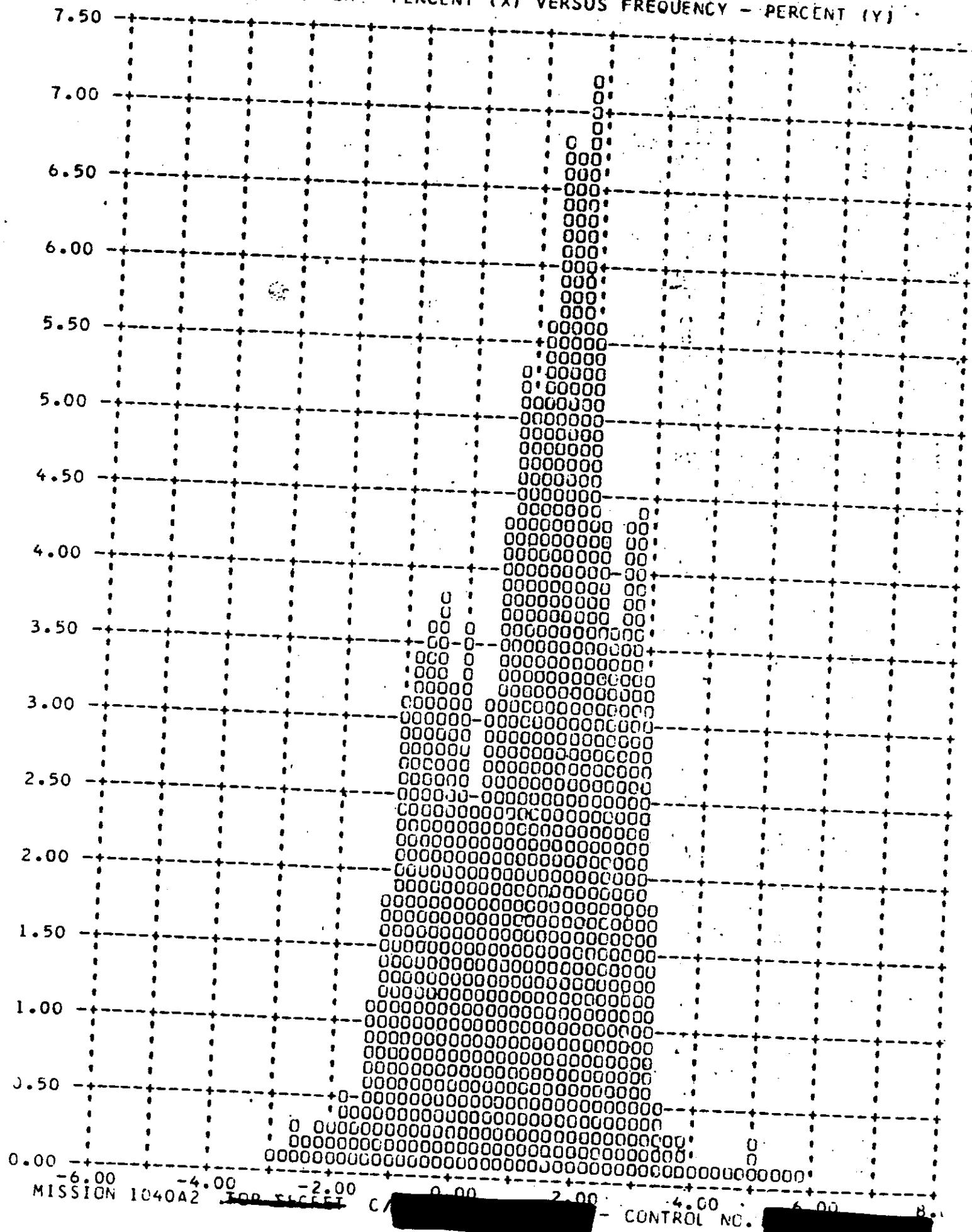
MISSION 1040AI ~~TGP SECRET~~ C - CONTROL NO. [REDACTED] - FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 2.1

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)



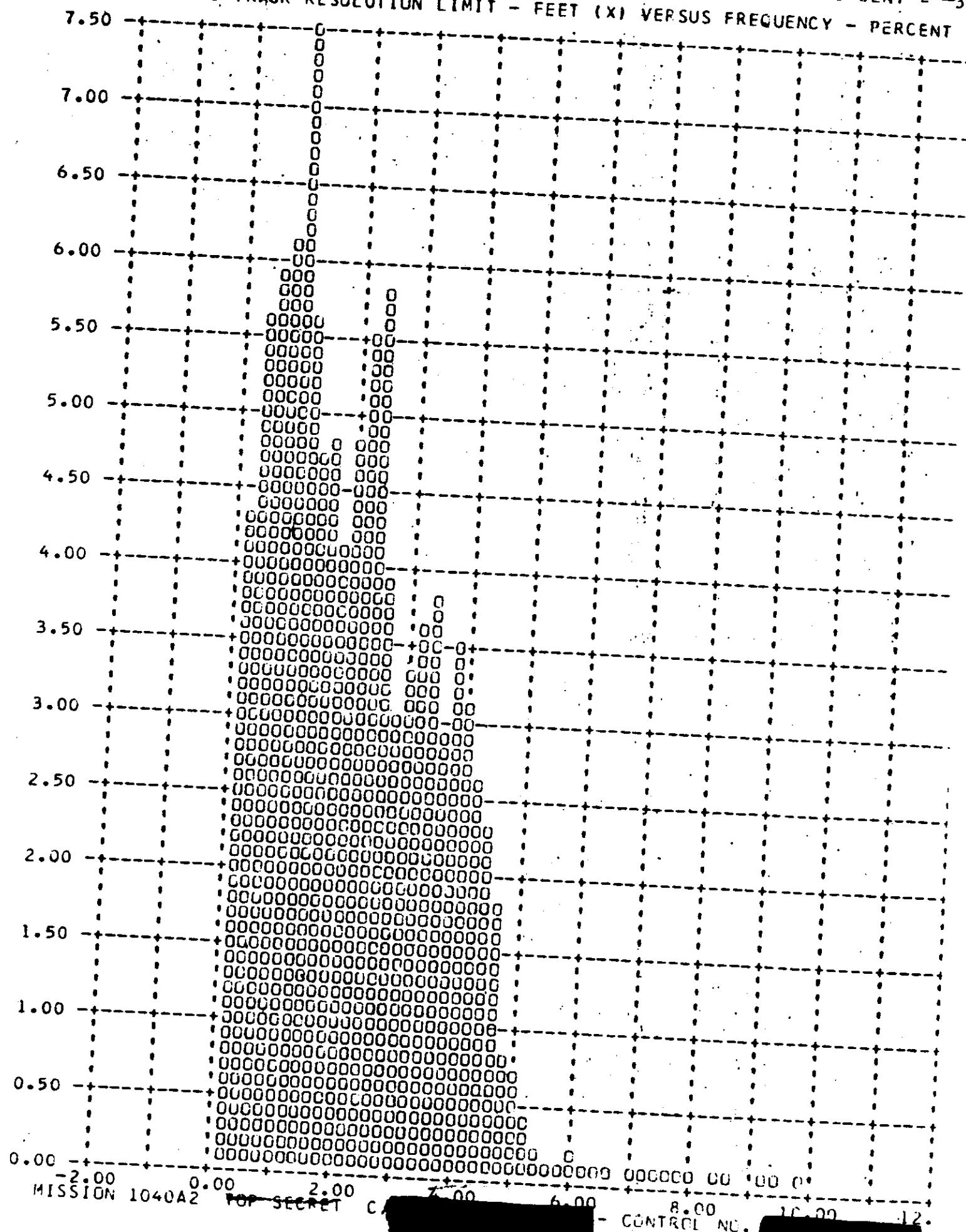
FRAMES 1-6 OF EACH DP. CHITED - 90 PERCENT = 2.6

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH UP-CHMITTED 90 PERCENT = 3

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT



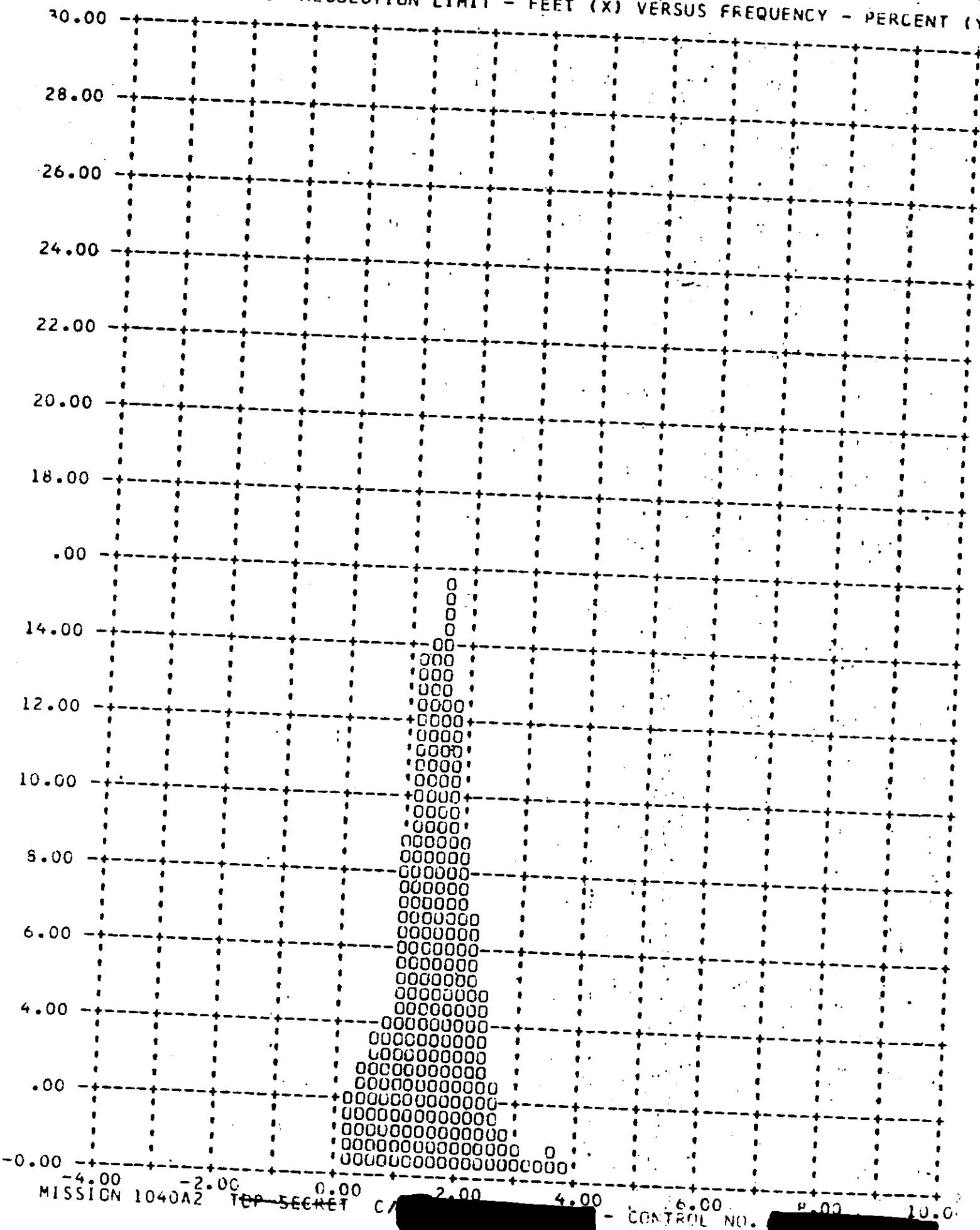
MISSION 1040A2

TOP SECRET C

- CONTROL NO. [REDACTED]

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 2.14

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

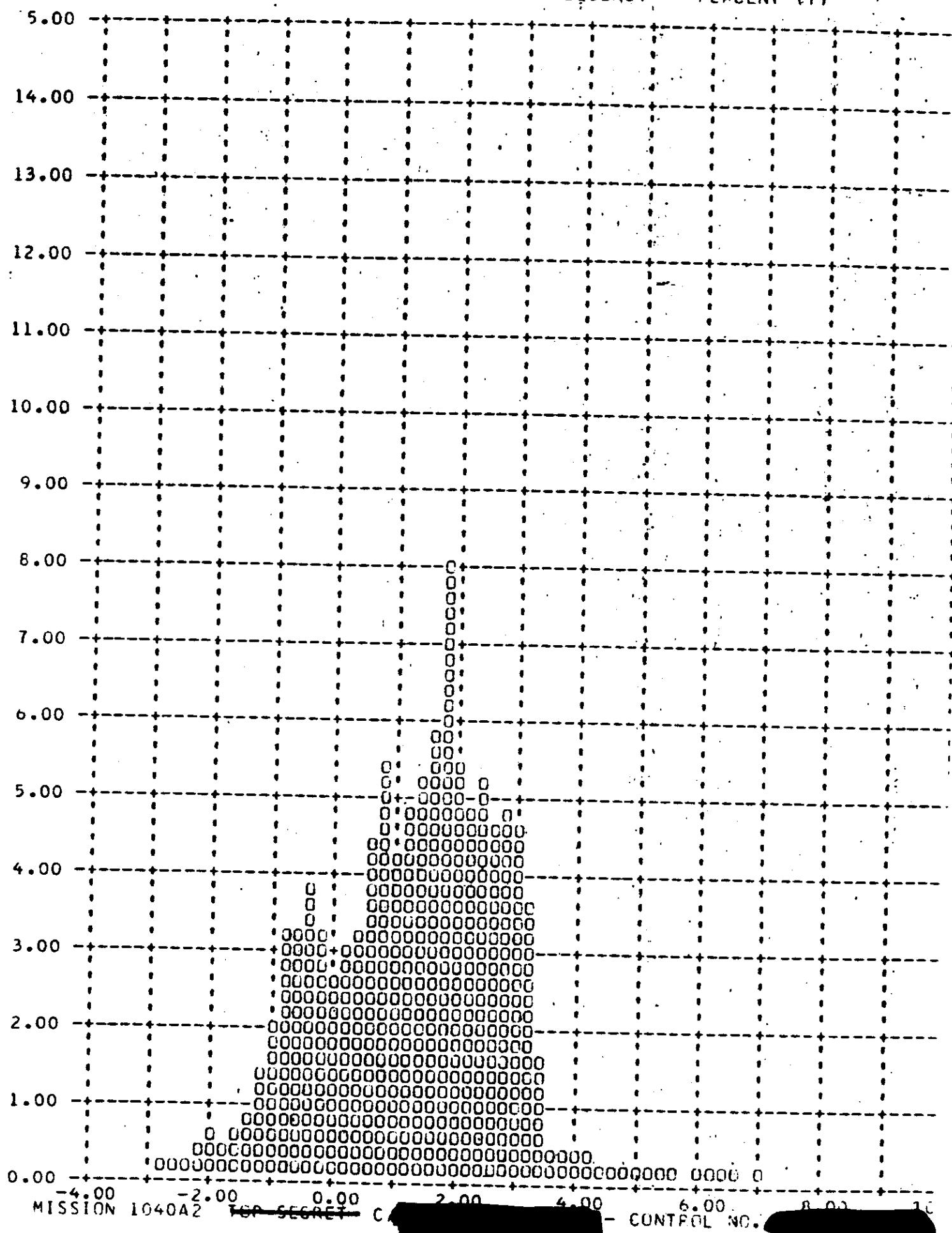


MISSION 1040A2 TEP SECRET C1

CONTROL NO.

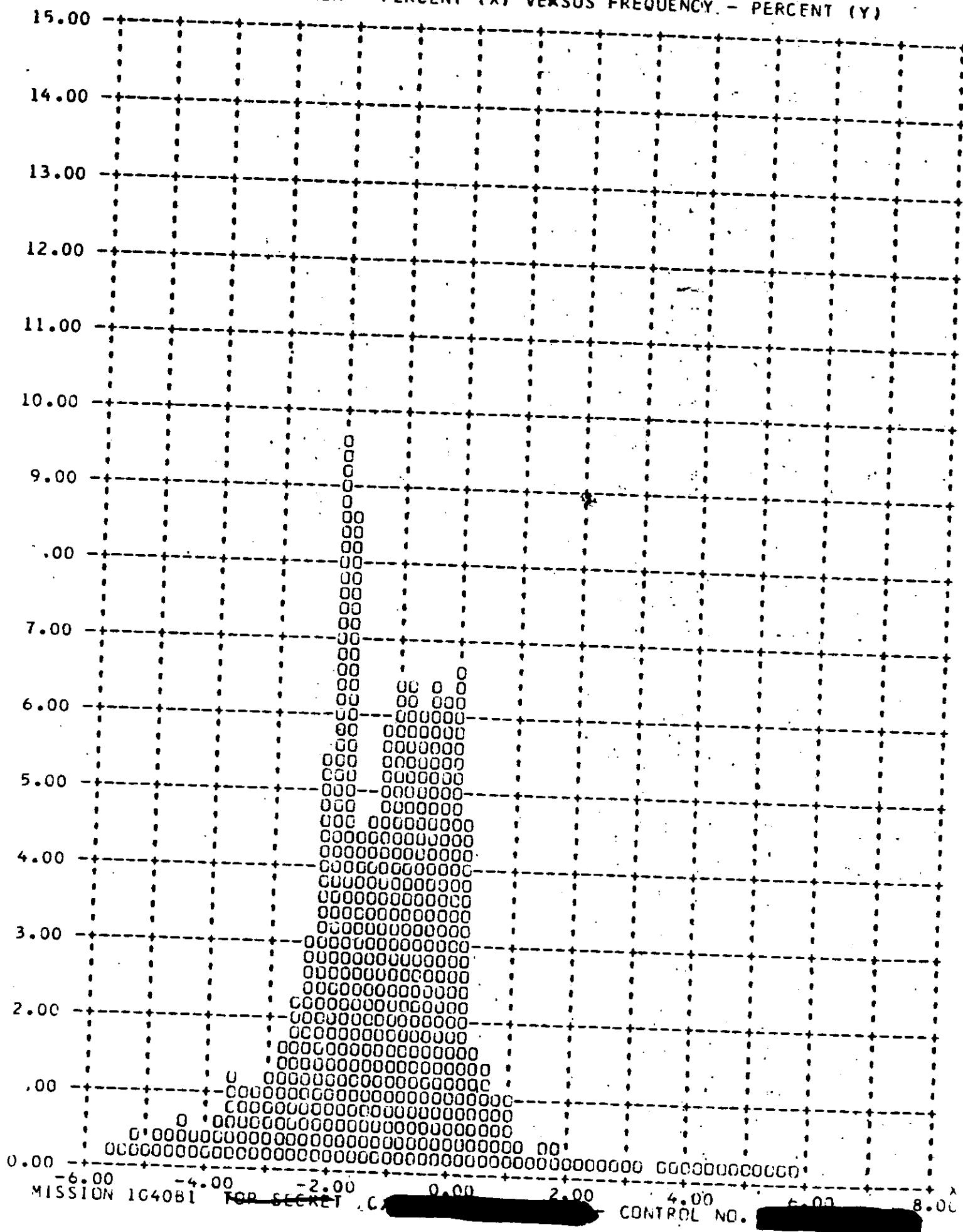
FRAMES 1-6 OMITTED 70 PERCENT

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)



FRAMES 1-6 OF EACH UP UMITTED 90 PERCENT = 2.72

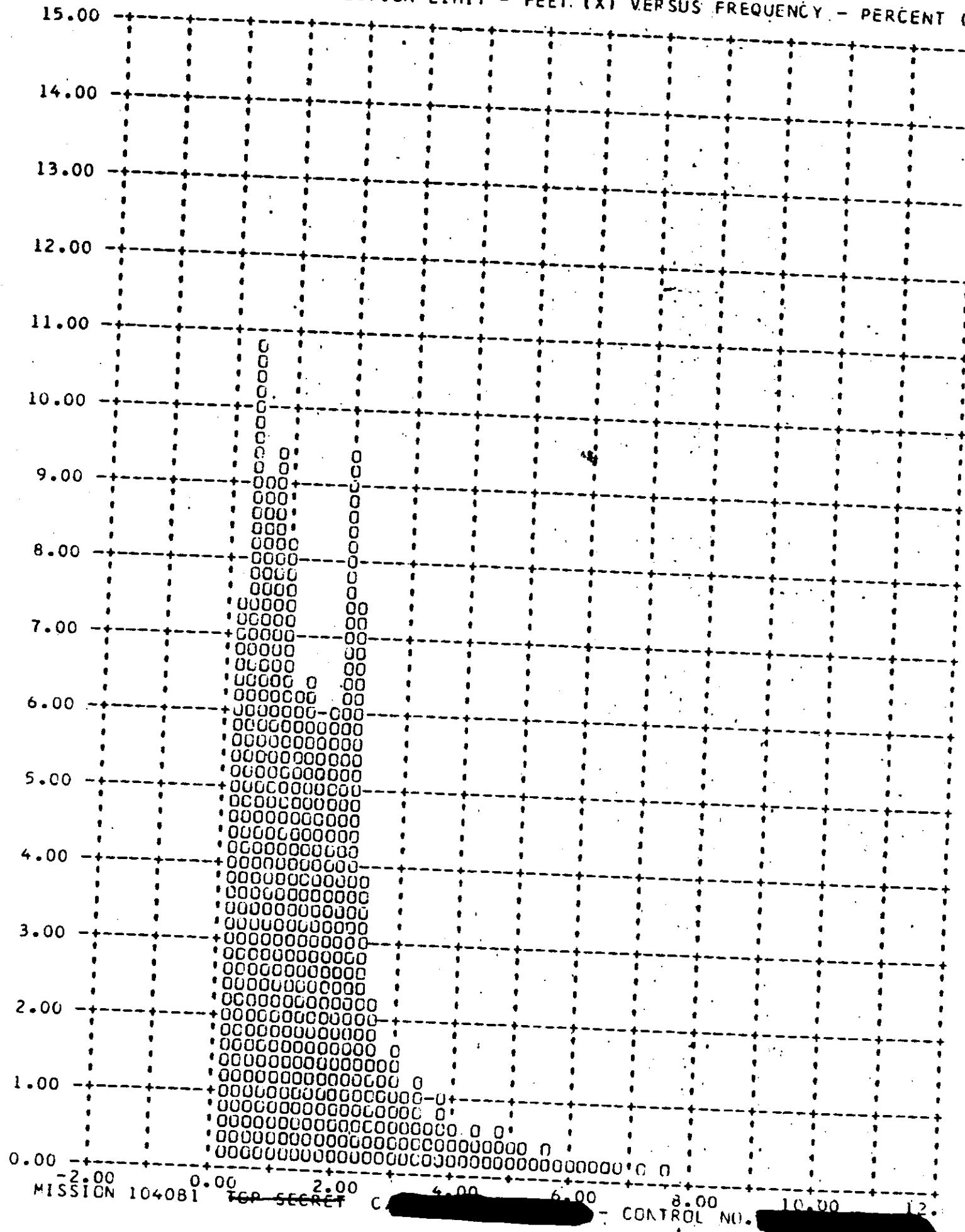
V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 104081 TOP SECRET C

CONTROL NO.

Y ALONG TRACK RESOLUTION LIMIT - FEET. (X) VERSUS FREQUENCY - PERCENT (%)



MISSION 104081

TOP SECRET

C [REDACTED]

4.00

6.00

8.00

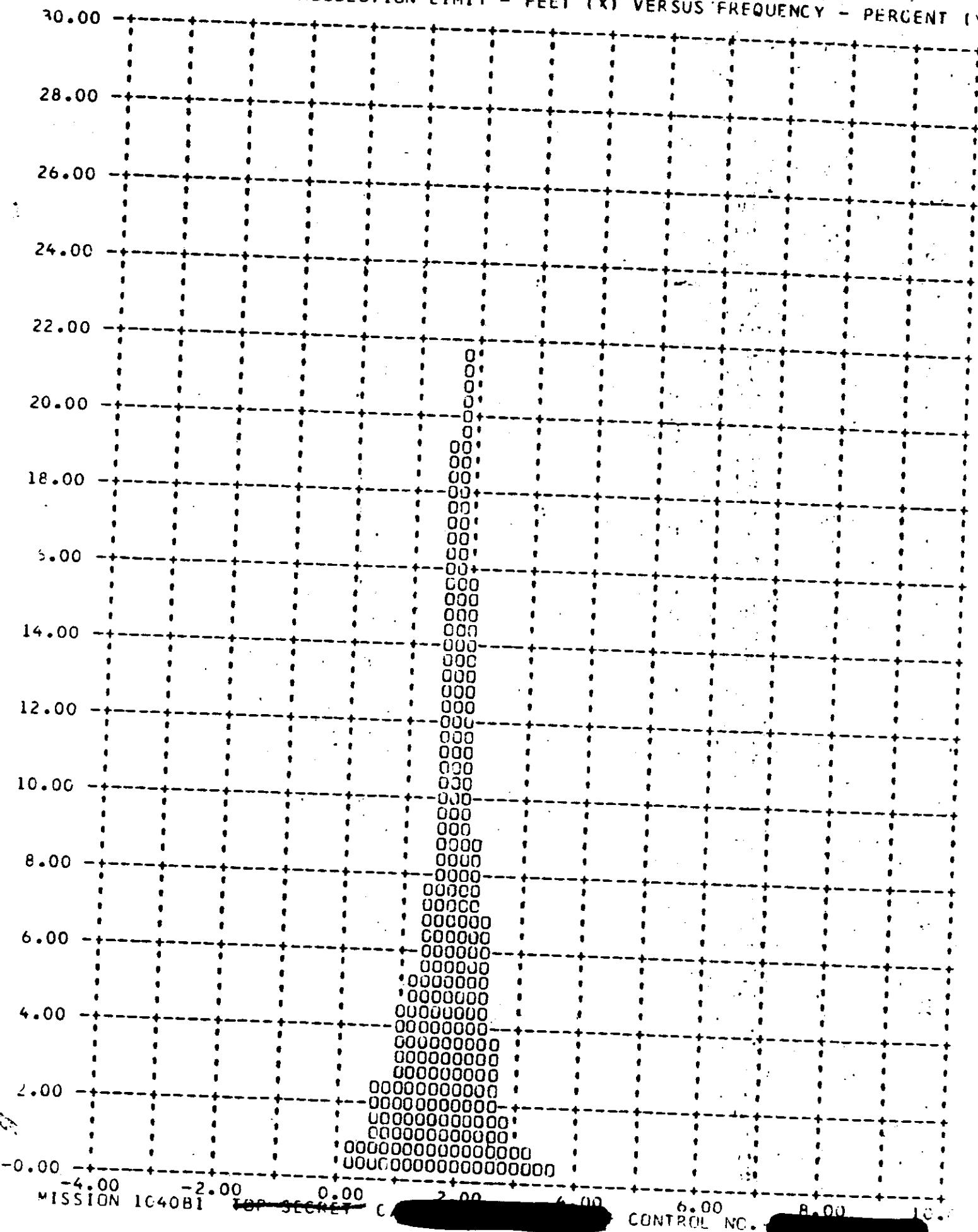
10.00

12.00

CONTROL NO. [REDACTED]

[REDACTED] FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 2.2

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



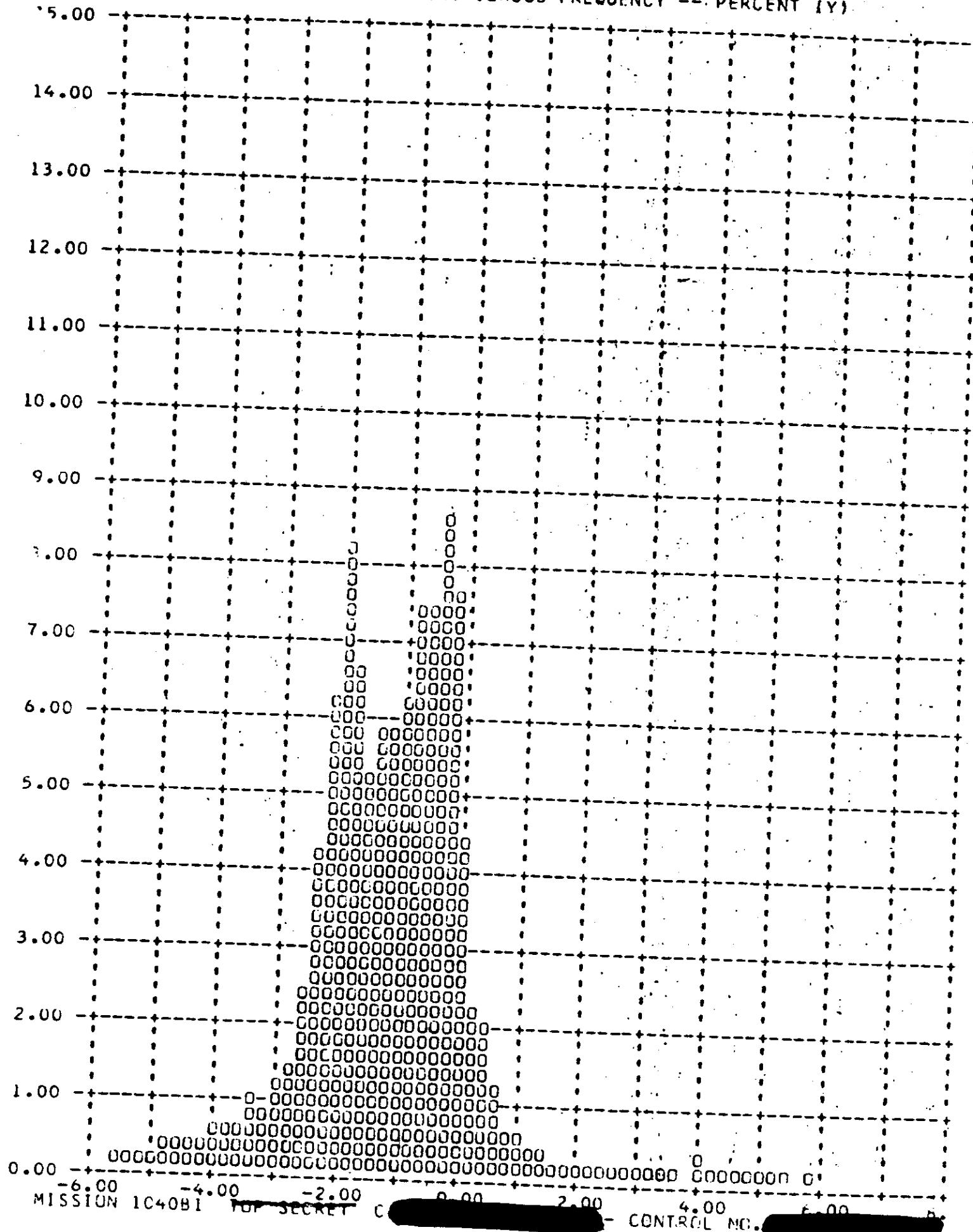
MISSION 1040B1 TOP SECRET C [REDACTED]

6.00
8.00
10.0

6.00
8.00
10.0

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 2.0

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)

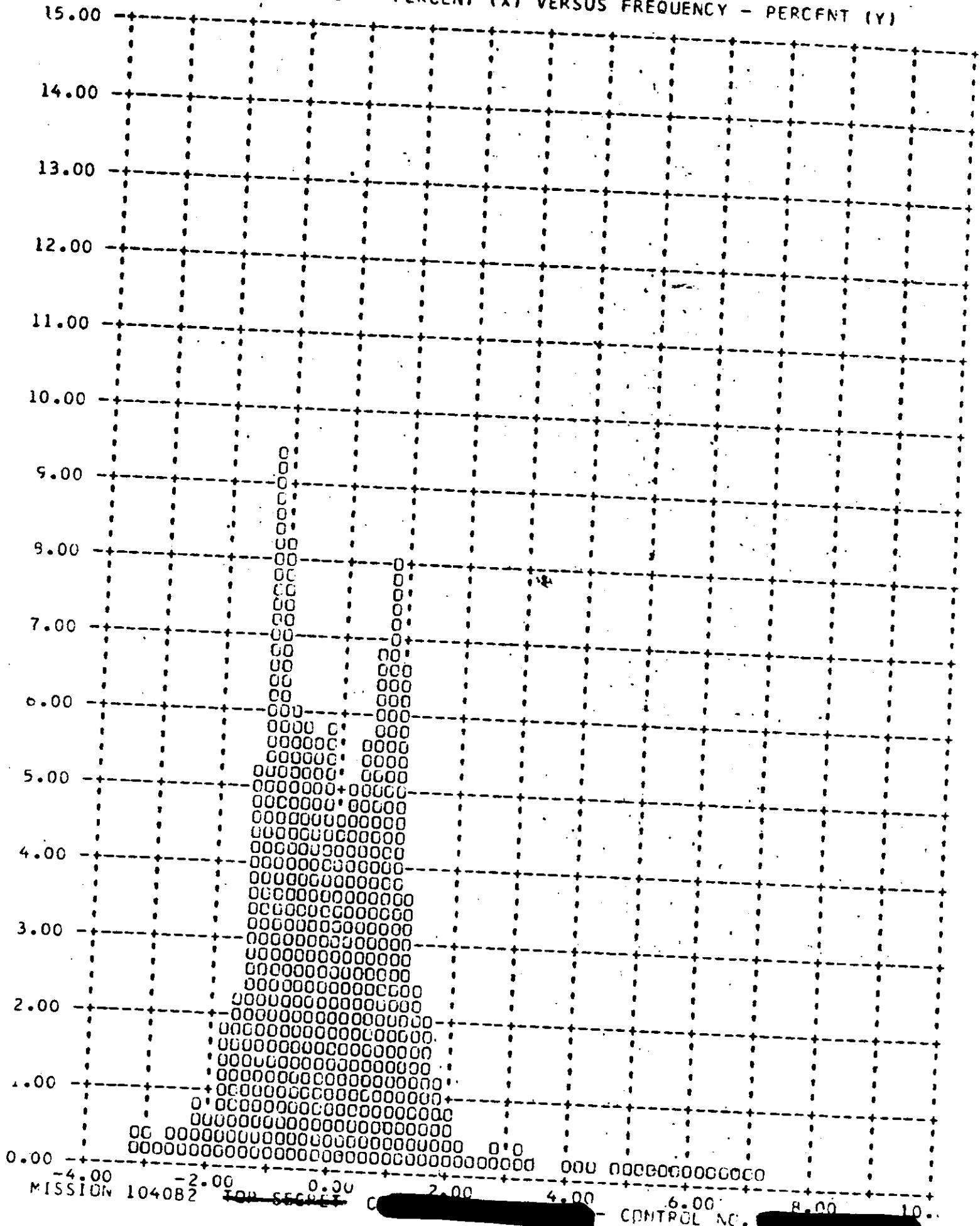


MISSION 104081 TOP SECRET C

- CONTROL NO.

FRAMES 1-5 OF EACH UP OMITTED 90 PERCENT = 1.0

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 104082

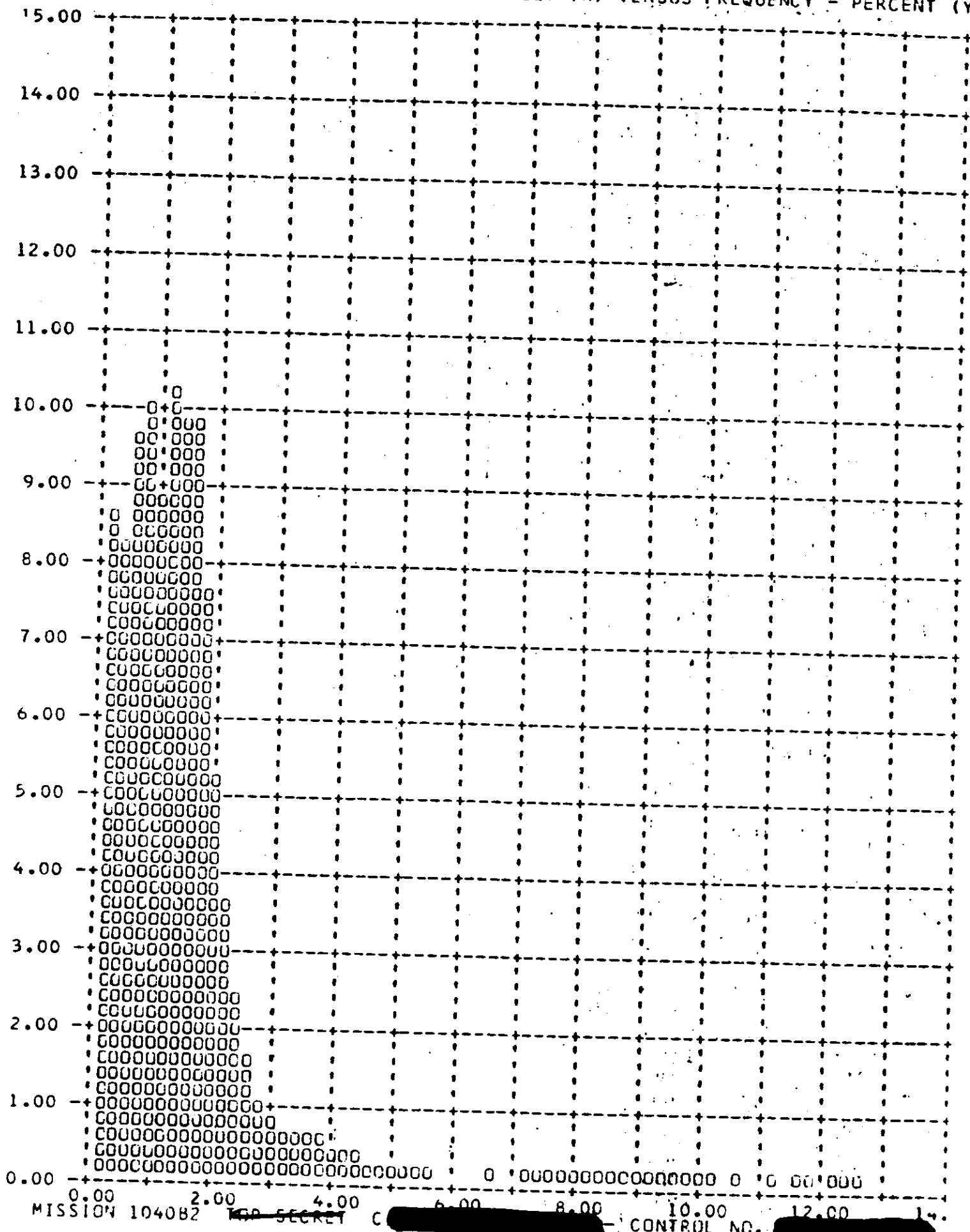
~~TOP SECRET~~

C

CONTROL NO.

FRAMES 1-6 OF EACH OF 6 MITTED 90 PERCENT = 2.2

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



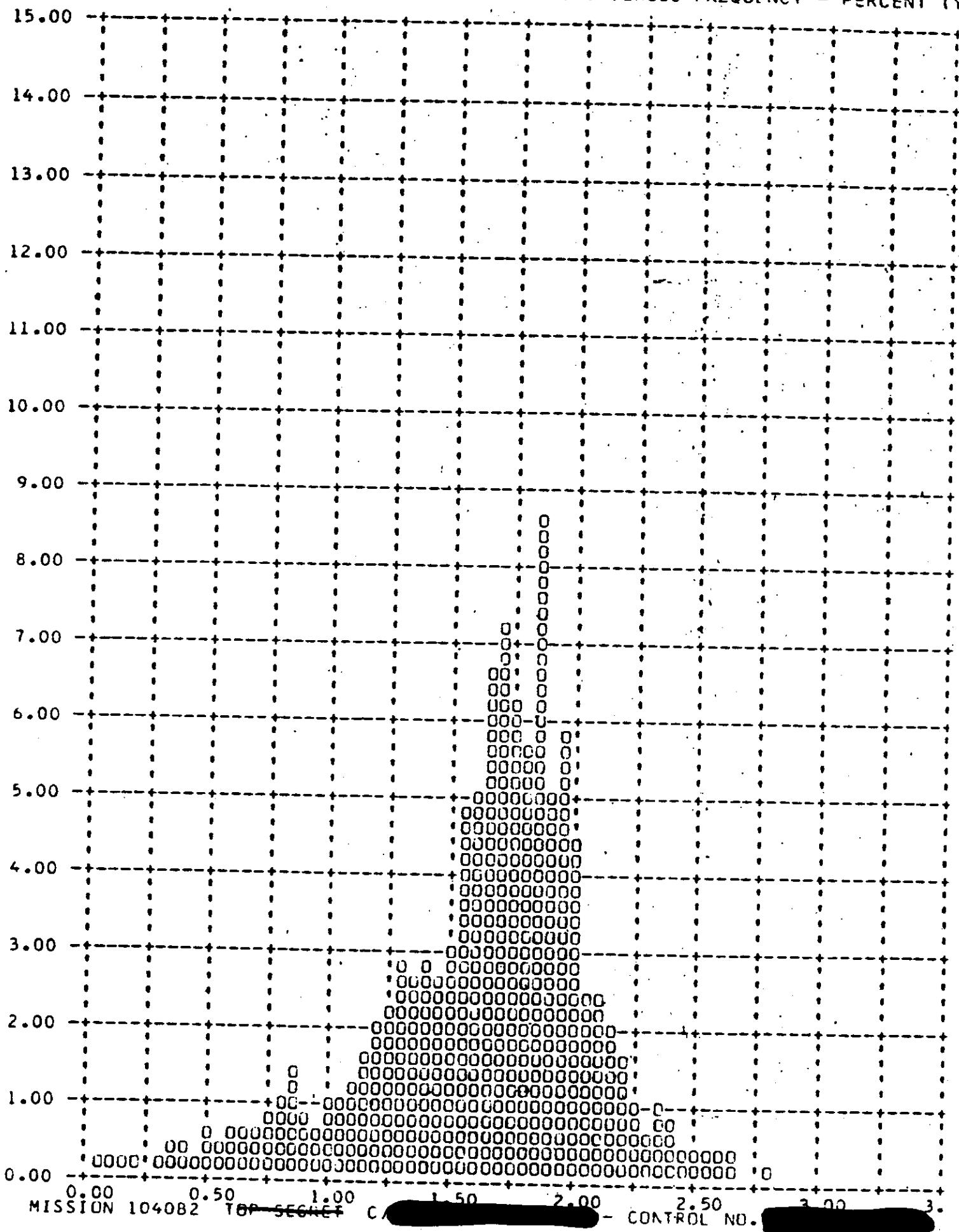
MISSION 104082 MISSION 104082

TOP SECRET C

CONTROL NO.

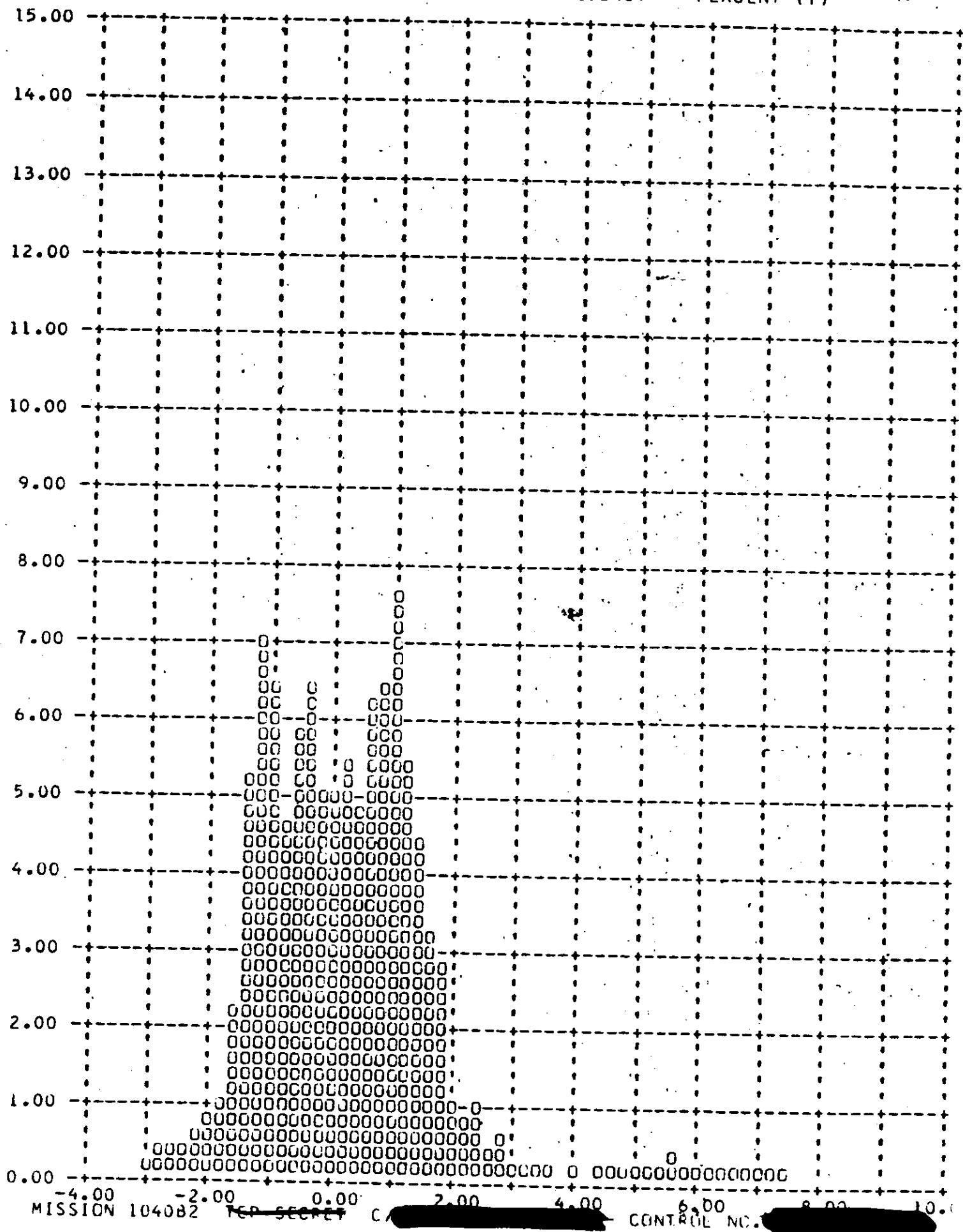
FRAMES 1-6 OF EACH UP OMITTED . 50 PERCENT = 200

Y - CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH OF UNMITTED 90 PERCENT - 1.

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)



MISSION 104082 TEP SECRET C

CONTROL NO.

SECTION 13

RADIATION DOSAGE

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips and the radiation level equivalents.

<u>Emulsion</u>	Mission 1040-1		Mission 1040-2	
	<u>B + F</u>	<u>Density</u>	<u>B + F</u>	<u>Density</u>
Type 3401	0.18	0.5 R	0.22	1.0 R
Royal X Pan	0.21	0.35 R	0.26	0.5 R

These levels are below that which will degrade the photography.

SECTION 14

SYSTEM RELIABILITY

Reliability calculations for the payload are based on a sample beginning with M-7. Hence both the major part of the Mural Program and the "J" Program are covered in the calculation. For certain auxiliaries, i.e., the Stellar-Index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode, auxiliary data recording, and Stellar-Index camera operation. A summary of estimated reliability is shown in Tables 14-1.

Panoramic Camera Reliability

Sample Size - 175 opportunities to operate.

One failure

Assume - 3000 cycles per camera per mission

Estimated Reliability = 99.0% at 50% confidence level

Main Camera Door Reliability

Sample Size - 57 vehicles x 2 doors = 114 opportunities to operate.

Estimated Reliability = 99.4% at 50% confidence level

Payload Command and Control

Sample Size - 9840 hours operation in sample

Two failures

Estimated Reliability = 97.4% at 50% confidence level

Payload Clock Reliability

Sample Size - 9840 hours operation in sample

No failures

Estimated Reliability = 99.3% at 50% confidence level

Estimated Reliability of Payload Functioning on orbit = 97.5% at
50% confidence level

Recovery System Reliability

79 opportunities to recover

1 failure - improper separation due to water seal - cutter failure

Estimated Reliability - 97.9 % at 50% confidence level

Stellar-Index Camera Reliability

Sample begins with J5

Sample size = 25,080 cycles

Four failures

Estimated Reliability = 92.4% at 50% confidence level

Horizon Camera Reliability

Sample begins with J5 - 100,500 cycles

Estimated Reliability of Single Camera = 99.0% at 50%
confidence level

Estimated Reliability of Four Horizon Cameras at a Parallel
Redundant System = 99.9% at 50% confidence level.

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS										SECONDARY FUNCTIONS									
	PANORAMIC CAMERA COMMAND & CONTROL SYSTEM					PAYLOAD CLOCK					ON-ORBIT FUNCTIONS					RECOVERY SYSTEM				
	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	FALLURES	FALLURES	FALLURES	FALLURES	FALLURES	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	FALLURES	FALLURES	FALLURES	FALLURES	FALLURES
9038 to 1008	52	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.1	96.1	96.1	96.1	96.1	0	0	0	0	0
1009	64	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.0	96.0	96.0	96.0	96.0	0	0	0	0	0
1010	66	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.2	96.2	96.2	96.2	96.2	0	0	0	0	0
1011	72	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.4	96.4	96.4	96.4	96.4	0	0	0	0	0
1012	76	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.8	96.8	96.8	96.8	96.8	0	0	0	0	0
1013	78	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.1	96.1	96.1	96.1	96.1	0	0	0	0	0
1014	82	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.2	96.2	96.2	96.2	96.2	0	0	0	0	0
1015	86	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.3	96.3	96.3	96.3	96.3	0	0	0	0	0
1016	90	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.4	96.4	96.4	96.4	96.4	0	0	0	0	0
1017	94	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.5	96.5	96.5	96.5	96.5	0	0	0	0	0
1018	96	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.7	96.7	96.7	96.7	96.7	0	0	0	0	0
1019	102	DOORS	RELIABILITY	RELIABILITY	3124 HOURS	0	0	0	0	0	96.8	96.8	96.8	96.8	96.8	0	0	0	0	0

* DESIGN FIN NEGATED PREVIOUS FAILURE CONSIDERATIONS

(PART II) 1/1-1

** 100% SAMPLE OUT OF SEQUENCE

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS			
	PANORAMIC CAMERA		COMMAND & CONTROL SYSTEM		PAYLOAD CLOCK		ON - ORBIT FUNCTIONS	
	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE
1020	FAILURES	RELIABILITY	FAILURES	RELIABILITY	FAILURES	RELIABILITY	FAILURES	RELIABILITY
1021	78	95.4	0	97.1	0	96.9	0	96.1
1022	76	95.4	0	97.1	0	96.9	0	96.0
1023	76	95.4	0	97.1	0	96.9	0	96.1
1024	80	97.8	0	97.8	0	96.9	0	96.0
1025	82	99.2	0	97.3	0	96.9	0	96.3
1026	84	99.2	0	95.8	0	96.2	0	96.3
1027	86	99.2	0	95.8	0	96.3	0	96.5
1028	88	99.2	0	96.0	0	96.4	0	96.7
1029	90	99.2	0	96.1	0	96.5	0	96.7
1030	92	99.2	0	96.3	0	96.5	0	97.0
1031	94	99.3	0	96.4	0	96.7	0	97.1
1032	96	99.3	0	96.5	0	96.8	0	97.1
1033	98	99.3	0	96.6	0	96.9	0	97.2

**ESTIMATED RELIABILITY SUMMARY
(AT 50% CONDEMNATION LEVEL)**

C

SECTION 15

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 15-1 through 15-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003, 1005 and 1032 are deleted.

MISSION SUMMARY

MISSION NUMBER	LOAD NUMBER	VEHICLE NUMBER	LAUNCH DATE	LAUNCH TIME	ORBIT #	INCLINATION (DEG)	ALTITUDE (KMH)	LOCATION	RECOVERY PASS	SHOOTER NUMBER	CAMERA NUMBER	SLIT FILTER NUMBER	SLIT FILTER NUMBER	SHOOTER NUMBER	CAMERA NUMBER
1004	J-05	1174	2/15/64	2136 1	149	99.9	29.0	49	112	124	0180	W-21	125	0200	W-21
1006	J-09	1176	2/14/64	2059 2	79.9	84.0	63.2	65	128	148	0200	W-21	149	0200	W-21
1007	J-07	1169	2/15/64	2316 2	65.6	93.2	41.5	65	126	1044	0200	W-21	135	0200	W-21
1008	J-10	1177	2/18/64	2314 2	85.0	99.4	40.8	49	112	150	0200	W-21	191	0200	W-21
1009	J-12	1165	2/14/64	2316 2	101	98.6	39.5	49	128	164	0200	W-21	183	0200	W-21
1010	J-11	1178	2/14/64	2234 2	84.9	97.4	42.6	65	144	152	0175	W-21	153	0175	W-21
1011	J-32	1176	10/5/64	2130 2	179.9	99.3	26.9	65	160	0193	W-21	161	0193	W-21	030/30/30
1012	J-13	1173	11/2/64	2130 2	180.6	99.3	26.9	65	160	0193	W-21	161	0193	W-21	037/37/37
1014	J-16	1180	11/6/64	2106 4	110.0	105.2	65.6	67	143	162	0200	W-21	159	0200	W-21
1015	J-17	1167	10/29/64	2110 5	74.6	98.7	21.6	67	179	138	0200	W-21	161	0200	W-21
1016	J-18	11608	11/16/65	2130 2	174.9	98.4	30.2	61	139	137	0250	W-21	173	0250	W-21
1017	J-14	11611	2/25/65	2144 2	75.0	97.2	25.9	61	145	140	0250	W-21	165	0175	W-21
1018	J-19	11612	3/25/65	2111 2	96.0	100.2	40.3	66	99	122	0250	W-21	123	0175	W-21
1019	J-04	11614	4/29/65	2144 2	85.0	99.1	27.1	60	—	118	0250	W-21	119	0175	W-21
1020	J-20	11613	6/9/65	2159 2	75.1	97.1	40.6	97	113	136	0250	W-21	137	0175	W-21
1021	J-21	11615	5/18/65	1803 2	75.0	109.2	24.3	61	161	166	0175	W-21	167	0250	W-21
1022	J-22	11617	7/19/65	2201 2	85.0	99.7	30.3	65	168	0250	W-21	169	0175	W-21	027/05/60
1023	J-23	11618	8/17/65	2100 2	70.0	97.0	29.0	61	144	170	0223	W-25	171	0150	W-21
1024	J-24	11619	9/22/65	2131 2	80.0	95.9	18.4	91	161	172	0225	W-25	173	0150	W-21
1025	J-28	11616	10/5/65	1746 2	75.0	112.9	44.3	61	142	175	W-21	127	0175	W-21	065/73/72
1026	J-25	11620	10/28/65	2117 2	75.0	93.0	17.0	61	160	174	0225	W-25	175	0150	W-21
1027	J-27	11621	12/9/65	2110 2	80.0	97.4	17.3	61	144	164	0250	W-25	163	0175	W-21
1028	J-26	11610	12/24/65	2106 2	80.0	97.6	28.4	61	144	176	0250	W-25	177	0175	W-21

MISSION SUMMARY

PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA SERIAL NUMBER	M I P VALUE	VISUAL RES	AFFECT	M/T AIM	SLIT AVERAGE	SLIT (%)	AVERAGE	SLIT (%)	90% ATTITUDE ERROR (°)			90% V/H ERROR (m)				
										ALL	HIGH	PITCH	ROLL	PITCH	ROLL	YAW	
1004-1	FWD	124	.95	.78	.97	109	115	127	124	0.45	0.42	1.08	30.0	25.0	21.0	9.1	
1004-1	AFT	125	.95	.86	.95	96	115	112	92	0.74	0.50	0.91	44.0	30.0	29.0	4.9	
1004-2	FWD	125	.73	.76	.88	105	106	92	95	0.74	0.50	0.91	44.0	30.0	29.0	6.5	
1005-1	FWD	148	.90	.78	.65	88	84	97	91	0.41	0.42	1.14	26.8	28.5	27.0	15.4	
1005-1	AFT	149	.90	.74	.74	43	90	320	87	92	0.42	1.14	26.8	27.0	13.0	13.0	
1006-2	FWD	149	.90	.85	.95	64	81	81	94	0.49	0.40	1.08	31.1	27.9	30.0	11.6	
1006-2	AFT	149	.93	.83	.72	90	87	94	90	0.49	0.40	1.08	31.1	27.9	30.0	10.1	
1007-1	FWD	144	.85	.80	.60	87	92	91	97	0.58	0.46	1.43	37.4	29.9	29.9	5.4	
1007-2	AFT	145	.85	.79	.95	43	83	320	68	74	0.50	0.47	43.0	25.0	24.0	7.6	
1008-1	FWD	150	.85	.80	.80	95	95	91	95	0.59	0.59	0.94	43.4	23.9	23.9	5.9	
1008-2	FWD	151	.85	.76	.95	73	43	65	96	0.55	0.55	0.71	42.6	24.0	32.0	5.4	
1008-2	AFT	151	.79	.82	.84	91	83	85	91	0.63	0.36	0.71	42.6	24.0	32.0	4.2	
1009-1	FWD	154	.85	.92	.60	—	—	75	68	0.65	0.65	0.71	29.2	22.7	27.6	5.5	
1009-2	AFT	155	.85	.94	.85	65	—	60	75	0.65	0.65	0.55	33.6	23.9	23.9	5.6	
1010-1	FWD	152	.85	.86	.86	80	80	80	82	0.48	0.65	0.65	33.6	23.9	27.0	4.9	
1010-2	FWD	153	.95	.90	.90	90	68	80	82	82	0.70	1.21	0.71	23.6	23.6	27.0	5.9
1011-1	FWD	160	.90	.84	.95	76	80	80	82	0.59	0.70	1.21	49.4	23.6	30.7	4.8	
1011-1	AFT	161	.84	.94	.95	77	80	80	82	0.59	0.70	1.21	49.4	23.6	30.7	4.8	
1012-1	FWD	156	.85	.92	.86	91	91	91	93	0.77	0.39	0.97	43.1	28.9	31.1	5.3	
1012-1	AFT	157	.85	.91	.91	—	—	87	95	0.77	0.39	0.97	43.1	28.9	31.1	5.3	
1013-1	FWD	158	.85	.85	.77	91	91	91	93	0.65	0.51	—	47.1	33.2	33.2	4.6	
1013-1	AFT	159	.85	.85	.85	—	—	80	95	0.65	0.51	—	47.1	33.2	33.2	4.6	
1014-1	FWD	162	.80	.87	.87	91	91	91	93	0.97	0.77	0.91	45.2	30.7	20.4	5.3	
1014-2	FWD	158	.80	.83	.83	—	—	80	95	0.97	0.77	0.91	45.2	30.7	20.4	5.3	
1014-2	AFT	159	.80	.86	.86	91	87	87	95	0.97	0.77	0.91	45.2	30.7	20.4	5.3	
1015-1	FWD	138	.85	.97	.87	—	—	76	86	0.62	0.41	1.46	55.0	36.1	36.5	4.6	
1015-2	AFT	141	.87	.87	.82	82	80	80	82	0.62	0.41	1.44	54.8	36.0	36.3	4.6	
1016-1	FWD	132	.85	.85	.83	91	80	80	82	0.62	0.41	1.44	54.8	36.0	36.3	4.6	
1016-2	FWD	133	.85	.90	.81	—	—	80	82	0.62	0.41	1.44	54.8	36.0	36.3	4.6	
1017-1	FWD	140	.72	.75	.85	80	80	80	82	0.62	0.41	1.44	54.8	36.0	36.3	4.6	
1017-2	FWD	165	.85	.85	.85	—	—	80	85	0.62	0.41	1.44	54.8	36.0	36.3	4.6	
1018-1	FWD	122	.85	.79	.77	—	—	80	84	0.62	0.41	1.44	47.4	36.7	36.7	4.6	
1018-2	AFT	123	.85	.84	.87	—	—	80	75	0.62	0.41	1.44	47.4	36.7	36.7	4.6	
1018-2	FWD	123	.85	.87	.87	—	—	71	91	0.62	0.41	1.44	47.4	36.7	36.7	4.6	
1018-2	AFT	123	.85	.87	.87	—	—	71	91	0.62	0.41	1.44	47.4	36.7	36.7	4.6	

PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA SERIAL NUMBER	IN-PILOT VISUAL RES.	AF SPPF	MTF/AIM	SLIT AVERAGE (μ)	SLIT AVERAGE (μ)	SLIT AVERAGE (μ)	MTF/AIM	90% ATTITUDE ERROR (°)	90% ATTITUDE RATE (°/HR)	90% V/H ERROR (IN)	90% RESOLUTION LIMIT (FEET) CROSS TRACK	
									PITCH	ROLL	YAW		
1019-1	FWD 118	.85	.91	—	80	76	80	.97	.97	.97	.97	.91	.91
	APT 119	—	—	—	80	83	101	.43	.36	.36	.36	.65	.65
1020-1	FWD 135	60	65	—	—	69	78	.90	.46	.35	.34	.64	.64
	APT 136	—	—	—	80	82	80	.46	.35	.35	.35	.59	.59
1020-2	FWD 137	—	—	—	—	—	—	.41	.17	.17	.17	.76	.76
	APT 138	—	—	—	—	—	—	.41	.17	.17	.17	2.6	2.6
1021-1	FWD 166	.65	.88	—	—	77	86	.99	.55	.37	.34	.6	.6
	APT 167	.50	.85	—	—	80	90	.98	.55	.38	.34	.55	.55
1021-2	FWD 167	.85	.74	—	—	80	74	.90	.55	.38	.34	.55	.55
	APT 168	—	—	—	—	62	62	—	—	—	—	—	—
1022-1	FWD 168	.85	.88	—	—	86	78	.91	.47	.51	.48	.55	.55
	APT 169	.91	.90	—	—	80	74	.84	.47	.51	.49	.62	.62
1022-2	FWD 169	.85	.92	—	—	92	99	.90	.40	.51	.50	.60	.60
	APT 170	—	—	—	—	—	—	—	—	—	—	—	—
1023-1	FWD 170	.85	—	—	—	94	97	.90	.49	.33	.30	.55	.55
	APT 171	.85	—	—	—	87	80	.93	.49	.33	.30	.55	.55
1023-2	FWD 171	—	—	—	—	89	87	.87	.42	.36	.33	.58	.58
	APT 172	—	—	—	—	89	86	.88	.43	.37	.33	.58	.58
1024-1	FWD 172	.85	—	—	—	79	90	.92	.42	.25	.22	.47	.47
	APT 173	.85	—	—	—	80	95	.94	.42	.25	.22	.47	.47
1024-2	FWD 173	—	—	—	—	80	86	.90	.36	.31	.29	.54	.54
	APT 174	—	—	—	—	95	95	.95	.36	.31	.29	.54	.54
1025-1	FWD 174	.85	—	—	—	97	80	.97	.50	.41	.38	.55	.55
	APT 175	.85	—	—	—	80	97	.97	.51	.42	.40	.55	.55
1025-2	FWD 175	.85	—	—	—	80	85	.96	.52	.44	.42	.55	.55
	APT 176	—	—	—	—	91	91	.91	.52	.44	.42	—	—
1026-1	FWD 176	.85	—	—	—	76	80	.92	.65	.24	.20	.67	.67
	APT 177	.85	—	—	—	80	88	.98	.65	.24	.20	.67	.67
1026-2	FWD 177	.85	—	—	—	85	92	.92	.65	.24	.20	.67	.67
	APT 178	—	—	—	—	93	93	.90	.59	.44	.40	—	—
1027-1	FWD 178	.85	—	—	—	80	69	.90	.51	.37	.37	.47	.47
	APT 179	—	—	—	—	79	80	.92	—	—	—	—	—
1028-1	FWD 179	.85	—	—	—	80	91	.89	—	—	—	—	—
	APT 180	—	—	—	—	80	92	.93	—	—	—	—	—
1028-2	FWD 180	—	—	—	—	80	88	.87	—	—	—	—	—
	APT 181	—	—	—	—	77	84	.78	—	—	—	—	—
1029-1	FWD 181	.85	—	—	—	80	95	.80	—	—	—	—	—
	APT 182	—	—	—	—	83	82	.73	—	—	—	—	—
1029-2	FWD 182	.85	—	—	—	83	82	.77	—	—	—	—	—
	APT 183	—	—	—	—	91	94	.94	—	—	—	—	—
1030-1	FWD 183	.85	—	—	—	80	74	.76	—	—	—	—	—
	APT 184	—	—	—	—	80	79	.77	—	—	—	—	—
1030-2	FWD 184	.85	—	—	—	81	71	.71	—	—	—	—	—
	APT 185	—	—	—	—	71	74	.71	—	—	—	—	—
1031-1	FWD 185	.85	—	—	—	80	65	.76	—	—	—	—	—
	APT 186	—	—	—	—	80	71	.80	—	—	—	—	—
1031-2	FWD 186	.85	—	—	—	80	74	.74	—	—	—	—	—
	APT 187	—	—	—	—	81	94	.91	—	—	—	—	—
1033-1	FWD 187	.85	—	—	—	80	67	.77	—	—	—	—	—
	APT 188	—	—	—	—	77	93	.93	—	—	—	—	—
1033-2	FWD 188	.85	—	—	—	80	71	.80	—	—	—	—	—
	APT 189	—	—	—	—	75	92	.92	—	—	—	—	—

TABLE 15-2

PERFORMANCE SUMMARY

MISSION NUMBER	CARRIER	SERIAL NUMBER	M.I.P. VALUE	APPROX MTG/AIM			90% ATTITUDE ERROR (°)			90% ALTITUDE RATES (FPM)			TDS VHM (THROTTLE)			ROTATION RATE (DEG/SEC)			GROSS TRACK ERROR			L.M.C. ERROR		
				AVERAGE	BEST	WORST	PITCH	ROLL	YAW	PITCH	ROLL	YAW	PITCH	ROLL	YAW	PITCH	ROLL	YAW	PITCH	ROLL	YAW	PITCH	ROLL	
1034-1	FWD	106	80	76	75	80	0.18	0.10	0.15	18.3	20.4	24.9	0.24	0.15	0.20	24.9	26.3	27.1	27.5	27.5	27.5	27.5	27.5	27.5
1034-2	APT	107	80	74	70	80	0.19	0.10	0.15	19.3	20.4	24.9	0.24	0.15	0.20	24.9	26.3	27.1	27.5	27.5	27.5	27.5	27.5	27.5
1036-1	FWD	108	75	66	60	70	0.16	0.11	0.17	16.9	27.3	32.4	0.31	0.21	0.29	27.3	32.4	33.5	34.0	34.0	34.0	34.0	34.0	34.0
1035-2	FWD	109	85	80	81	80	0.16	0.11	0.17	16.4	23.4	28.3	0.30	0.20	0.29	23.4	28.3	30.5	31.6	31.6	31.6	31.6	31.6	31.6
1036-1	FWD	110	89	89	80	90	0.16	0.11	0.17	16.8	24.7	30.3	0.31	0.21	0.29	24.7	30.3	31.5	32.5	32.5	32.5	32.5	32.5	32.5
1036-2	FWD	101	86	84	80	86	0.16	0.11	0.17	16.9	23.4	28.3	0.30	0.20	0.29	23.4	28.3	30.5	31.6	31.6	31.6	31.6	31.6	31.6
1037-1	FWD	108	89	89	71	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4
1037-2	FWD	103	86	84	73	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4
1038-1	FWD	102	80	83	76	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4
1039-2	FWD	103	80	80	63	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4
1040-1	FWD	106	85	85	71	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4
1040-2	FWD	107	86	86	65	80	—	—	—	16.0	22.8	28.7	0.30	0.20	0.29	22.8	28.7	32.4	35.4	35.4	35.4	35.4	35.4	35.4

EXPOSURE-PROCESSING SUMMARY

SESSION NUMBER	CAMERA	ELEVATION (ft.)	SOLAR AZIMUTH RANGE (°)	PREDICTED PROCESSING TIME (min.)	REPORTED PROCESSING TIME (min.)	COMPUTED PROCESSING TIME (min.)	TERRAIN D-MIN.			TERRAIN D-MAX.			CLOUD D-MAX.			OVER-PROCESSED (%)	OVER-EXPOSED (%)	CLOUD COVER (%)	
							LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN				
019-1	FWD	24	70°	192	81	79	22	46	45	40	92	71	50	92	71	60	2.26	1.94	2.00
	APT	25	70°	152	92	86	26	55	19	38	87	10	15	70	66	65	2.30	2.02	1.95
020-1	FWD	30	75°	158	61	13	48	39	158	41	23	30	55	32	80	2.28	1.57	1.54	
	APT	29	75°	156	60	14	36	15	36	29	0	23	20	55	54	0.70	2.20	1.47	
020-2	FWD	47	69°	118	66	46	66	17	35	32	14	39	47	52	47	0.25	1.90	0.64	
	APT	48	69°	117	55	41	52	15	35	47	0	57	43	52	47	0.17	1.70	0.65	
021-1	FWD	15	66°	148	23	0	68	32	14	39	47	1	52	47	52	47	0.25	1.90	0.64
	APT	14	66°	147	25	0	69	31	15	38	47	0	57	43	52	47	0.17	1.70	0.65
021-2	FWD	15	52°	135	41	15	29	71	52	41	46	0	57	43	52	47	0.17	1.70	0.65
	APT	15	52°	135	41	15	100	0	53	26	0	50	30	50	30	0.21	1.38	0.56	
022-1	FWD	26	67°	30	150	0	36	64	9	36	56	0	42	58	0.16	1.49	0.45	0.10	
	APT	27	67°	28	150	0	69	11	77	42	51	0	53	47	0.24	1.48	0.57	0.50	
022-2	FWD	29	74°	21	152	0	6	92	-	37	62	0	43	57	0.20	0.99	0.39	0.35	
	APT	28	74°	19	152	0	100	0	10	44	46	0	53	47	0.21	1.40	0.48	0.44	
023-1	FWD	22	82°	9	164	0	55	19	54	27	72	26	0.15	1.26	0.39	0.35	0.43	0.21	
	APT	20	81°	5	163	0	11	89	0	39	61	0	42	58	0.20	1.40	0.53	0.48	
023-2	FWD	29	81°	13	177	0	7	93	0	19	81	0	16	82	0.22	1.38	0.48	0.42	
	APT	28	80°	-13	178	0	3	97	0	34	66	0	28	72	0.22	1.60	0.52	0.48	
024-1	FWD	10	61°	24	137	0	0	0	0	57	43	0	72	28	0.17	1.74	0.35	0.32	
	APT	9	61°	21	136	0	0	100	0	26	72	0	82	18	0.20	1.22	0.40	0.37	
024-2	FWD	9	79°	-1	151	0	0	100	-12	19	69	0	25	75	0.24	1.17	0.46	0.42	
	APT	8	79°	9	151	0	0	100	0	11	22	77	0	66	34	0.20	0.97	0.47	0.40
025-1	FWD	1	70°	-12	153	0	68	32	10	41	49	0	56	44	0.18	1.42	0.43	0.40	
	APT	0	70°	0	56°	-124	-31	0	71	28	5	49	43	0	61	39	0.18	1.69	0.49
025-2	FWD	0	56°	0	56	-122	-33	0	73	27	3	45	52	0	51	49	0.21	1.32	0.53
	APT	0	56°	0	56	-122	-33	0	73	27	3	45	52	0	51	49	0.21	1.32	0.53
026-1	FWD	3	63	26	110	0	0	100	0	100	0	0	100	0	100	0	0.97	0.97	1.00
	APT	2	63	26	108	0	0	100	0	100	0	21	79	0	20	80	0.26	1.34	0.53
026-2	FWD	3	73	15	135	0	4	96	0	4	96	0	16	84	0	20	89	0.22	
	APT	1	73	15	133	0	5	95	0	4	96	0	5	94	0	15	85	0.23	
026-3	FWD	2	61	5	145	0	5	97	0	5	97	0	28	74	0	20	85	0.22	
	APT	1	60	5	145	0	10	90	0	6	94	0	6	94	0	22	74	0.22	
027-1	FWD	3	63	26	110	0	0	100	0	0	100	0	1	97	0	100	0	0.97	
	APT	2	63	26	108	0	0	100	0	0	100	0	21	79	0	20	80	0.26	
028-1	FWD	3	73	15	135	0	4	96	0	4	96	0	11	89	0	20	86	0.22	
	APT	1	73	15	133	0	5	95	0	4	96	0	11	89	0	20	86	0.22	
028-2	FWD	2	61	5	145	0	5	97	0	5	97	0	28	74	0	20	85	0.22	
	APT	1	60	5	145	0	10	90	0	6	94	0	6	94	0	22	74	0.22	
029-1	FWD	3	63	18	130	0	20	80	0	21	79	0	25	75	0	20	86	0.22	
	APT	2	62	18	128	0	21	79	0	22	70	0	20	80	0	20	86	0.22	
029-2	FWD	0	60	4	145	0	14	96	0	22	70	0	28	72	0	20	86	0.22	
	APT	1	60	3	145	0	10	90	0	22	74	0	25	75	0	20	86	0.22	
030-1	FWD	1	70	20	140	0	99	1	18	34	48	0	51	49	0	25	67	0.22	
	APT	1	70	18	140	0	96	14	43	42	32	55	0	51	47	0	25	67	0.22
030-2	FWD	1	63	22	129	0	53	47	0	46	54	0	71	29	0	25	67	0.22	
	APT	1	62	10	158	0	42	57	0	53	47	0	70	30	0	24	67	0.22	
031-1	FWD	0	41	46	135	0	69	11	0	3	97	0	2	98	0	28	70	0.22	
	APT	1	47	45	135	0	10	90	1	8	69	0	1	94	0	20	70	0.22	
031-2	FWD	0	54	34	131	0	67	0	67	1	1	—	0	67	0	20	70	0.22	
	APT	0	54	34	131	0	—	—	—	—	—	—	0	67	0	20	70	0.22	
033-1	FWD	0	41	46	135	0	69	11	0	3	97	0	2	98	0	28	70	0.22	
	APT	1	47	45	135	0	10	90	1	8	69	0	1	94	0	20	70	0.22	
033-2	FWD	0	54	34	131	0	67	0	67	1	1	—	0	67	0	20	70	0.22	
	APT	0	54	34	131	0	—	—	—	—	—	—	0	67	0	20	70	0.22	

INSUFFICIENT DATA

EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA RAKE (°)	SOLAR AZIMUTH		PREDICTED PROCESSING		REPORTED PROCESSING		COMPUTED PROCESSING		TERRAIN D-MIN		TERRAIN D-MAX		CLOUD RANGE		CLOUD D-MAX		UNDER EXPOSED		OVER EXPOSED		CLOUD COVER (%)							
		P	F	P	F	P	F	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH					
1004-1	FWD	61	25	124	5	76	19	4	79	17	0.79	21	0.26	1.89	0.83	0.78	0.43	2.43	1.97	2.02	1.00	2.43	1.20	2.00	0	44			
1004-2	AFT	73	61	26	124	5	74	21	4	79	17	0.80	20	0.22	1.56	0.76	0.70	0.93	2.45	1.92	1.94	1.00	2.43	1.36	2.03	0	35		
1004-3	FWD	68	10	131	7	75	17	37	50	13	0.83	13	0.29	1.50	0.70	0.63	0.78	2.36	2.30	2.30	0.91	0.41	2.37	1.87	1.93	27			
1004-4	AFT	68	10	131	7	76	17	37	50	13	4	77	19	0.81	0.73	0.36	2.39	1.89	1.99	0.91	0.43	2.46	1.89	1.86	0	35			
1005-1	FWD	58	66	52	140	-	99	0	1	91	48	0	51	49	0.23	1.81	0.71	0.68	0.60	2.31	1.90	1.52	1.11	2.40	2.20	2.24	0	44	
1005-2	AFT	56	64	52	140	-	99	0	0	83	77	0	24	76	0.36	1.66	0.87	0.84	0.96	2.35	1.72	1.44	1.40	2.34	2.00	2.00	0	35	
1005-3	FWD	52	64	56	147	-	98	0	17	90	41	1	59	50	0.21	1.34	0.82	0.85	0.95	2.19	1.46	1.47	1.56	2.40	2.12	2.16	0	40	
1005-4	AFT	52	64	56	147	2	98	0	35	40	25	21	54	25	0.26	1.34	0.82	0.85	0.95	2.19	1.46	1.47	1.56	2.40	2.12	2.16	0	45	
1007-1	FWD	12	49	50	103	0	65	-	20	79	0	25	75	0.26	1.22	0.92	0.47	0.62	2.80	1.44	1.40	1.22	1.36	2.17	2.21	2.0	45		
1007-2	AFT	11	49	48	102	0	100	0	10	42	48	6	77	17	0.26	1.76	0.59	0.55	0.78	2.31	1.32	1.32	1.54	2.39	2.30	2.24	0	45	
1007-3	FWD	32	57	49	112	0	100	0	23	76	3	28	66	0.26	1.74	0.59	0.55	0.60	0.58	0.44	2.37	2.16	2.20	1.6	1.53	0	45		
1007-4	AFT	31	57	58	117	0	100	0	19	41	40	3	68	0.26	1.56	0.60	0.58	0.64	2.27	1.30	1.32	1.54	2.34	2.28	2.24	0	45		
1008-1	FWD	30	51	59	102	0	100	0	4	32	64	-	55	64	0.32	1.48	0.86	0.62	0.78	2.24	1.55	1.54	1.46	2.35	2.21	2.24	0	45	
1008-2	AFT	29	51	52	105	0	100	0	3	31	66	0	30	67	0.29	1.71	0.57	0.69	0.71	2.21	1.57	1.58	1.08	2.37	2.21	2.24	0	45	
1009-1	FWD	12	49	42	132	0	100	0	-	26	73	0	54	66	0.32	1.40	0.65	0.62	0.65	2.41	1.53	1.52	0.83	2.51	2.30	2.36	0	45	
1009-2	AFT	12	49	42	132	0	100	0	40	60	0	45	55	0.28	1.42	0.70	0.64	0.92	2.28	1.55	1.55	0.63	2.51	2.32	2.36	0	50		
1009-3	FWD	25	55	55	158	2	98	0	21	76	0	40	60	0.29	1.55	0.71	0.69	0.64	2.42	1.61	1.60	0.62	2.52	2.25	2.30	0	55		
1010-1	FWD	18	47	45	63	0	21	79	0	15	87	0	9	91	0.28	1.4	0.52	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	0	45	
1010-2	AFT	18	47	45	63	0	21	79	0	15	87	0	9	91	0.28	1.4	0.52	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	0	45	
1011-1	FWD	2	55	33	66	0	64	36	3	23	73	2	23	75	0.18	1.4	0.52	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	0	45	
1012-1	AFT	0	55	33	66	0	67	33	3	24	70	0	37	63	0.24	1.4	0.60	0.56	0.60	2.35	1.37	1.35	1.11	2.42	2.16	2.20	0	45	
1012-2	FWD	0	45	38	71	0	64	36	7	56	37	0	65	55	0.25	1.30	0.59	0.57	0.61	2.35	1.37	1.35	1.11	2.42	2.16	2.20	0	45	
1012-3	AFT	0	45	38	71	0	64	36	7	56	37	0	65	55	0.25	1.30	0.59	0.57	0.61	2.35	1.37	1.35	1.11	2.42	2.16	2.20	0	45	
1012-4	FWD	0	55	34	106	0	77	23	6	44	50	0	49	51	0.30	1.29	0.58	0.55	0.73	2.35	1.49	1.48	1.00	2.44	2.22	2.26	0	45	
1013-1	FWD	0	56	28	63	0	63	36	2	42	58	0	50	60	0.27	1.06	0.62	0.62	0.68	2.36	1.48	1.48	1.00	2.44	2.22	2.26	0	40	
1013-2	AFT	0	56	28	62	0	64	36	2	42	58	0	50	60	0.27	1.06	0.62	0.62	0.68	2.36	1.48	1.48	1.00	2.44	2.22	2.26	0	40	
1014-1	FWD	5	68	19	71	0	21	79	14	39	61	0	63	37	0.17	0.99	0.40	0.36	0.56	2.36	1.40	1.42	0.90	2.36	2.00	2.27	0	45	
1014-2	AFT	5	68	19	71	0	21	79	14	39	61	0	63	37	0.17	0.99	0.40	0.36	0.56	2.36	1.40	1.42	0.90	2.36	2.00	2.27	0	45	
1014-3	FWD	0	55	14	69	0	31	69	0	13	87	0	35	64	0.18	1.26	0.51	0.48	0.54	2.36	1.42	1.42	0.90	2.36	2.00	2.27	0	45	
1014-4	AFT	0	55	14	69	0	31	69	0	13	87	0	35	64	0.18	1.26	0.51	0.48	0.54	2.36	1.42	1.42	0.90	2.36	2.00	2.27	0	45	
1015-1	FWD	0	72	12	71	0	72	79	0	9	91	0	9	91	0.26	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1015-2	AFT	0	72	12	71	0	72	79	0	9	91	0	9	91	0.26	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1015-3	FWD	5	68	18	76	0	7	93	-	41	58	0	42	58	0.22	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1015-4	AFT	5	68	18	76	0	7	93	-	41	58	0	42	58	0.22	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1016-1	FWD	0	69	12	76	0	27	73	0	18	92	0	7	93	0.26	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1016-2	AFT	0	69	12	76	0	27	73	0	18	92	0	7	93	0.26	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1017-1	FWD	-11	50	24	99	0	0	0	13	63	24	0	0	0	0.00	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1017-2	AFT	-1	57	19	98	0	17	83	29	54	18	0	4	90	0	0.00	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40
1018-1	FWD	8	77	15	134	0	0	0	100	63	24	0	0	0	0.00	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	
1018-2	AFT	8	77	15	134	0	0	0	100	63	24	0	0	0	0.00	1.03	0.69	0.60	0.65	2.36	1.37	1.38	0.88	2.40	2.17	2.21	0	40	

EXPOSURE-PROCESSING SUMMARY

MISSION NUMBER	CAMERA	ELEVATION RANGE (°)	SOLAR RANGE (°)	AZIMUTH RANGE (°)	PREDICTED PROCESSING TIME (min)		REPORTED PROCESSING TIME (min)		COMPUTED PROCESSING TIME (min)		GND (min)		AIRCRAFT (min)		GND (min)		AIRCRAFT (min)		GND (min)			
					LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH		
1034-1	FWD	23.77	18.10	166.00	55.00	145.00	21.00	0.20	1.80	0.23	1.80	0.50	0.50	0.50	0.50	1.58	1.61	0.88	2.45	1.22	2.26	
	APT	23.77	10.00	178.00	55.00	125.00	22.00	0.67	0.84	0.24	1.63	0.65	0.65	0.65	0.65	1.55	1.55	1.50	2.45	1.22	2.26	
1034-2	FWD	29.88	20.00	178.00	55.00	125.00	22.00	0.22	0.72	0.19	1.52	0.67	0.67	0.67	0.67	1.55	1.55	1.50	2.45	1.22	2.26	
	APT	30.88	20.00	178.00	55.00	125.00	22.00	0.37	0.57	0.00	1.54	0.54	0.54	0.54	0.54	1.55	1.55	1.50	2.45	1.22	2.26	
1035-1	FWD	12.68	19.00	144.00	0.00	17.00	0.00	0.11	0.69	0.00	0.95	0.28	1.30	0.32	0.45	0.61	2.44	1.40	1.06	2.43	1.15	2.22
	APT	13.68	18.00	144.00	0.00	17.00	0.00	0.14	0.65	0.00	0.81	0.30	1.38	0.30	0.43	0.60	2.44	1.40	1.06	2.43	1.15	2.22
1035-2	FWD	4.57	10.00	158.00	10.00	22.00	75.00	0.18	0.82	0.02	1.50	0.50	0.50	0.50	0.50	1.55	1.55	1.50	2.45	1.22	2.26	
	APT	5.57	9.00	158.00	10.00	22.00	77.00	0.21	0.82	0.02	1.59	0.55	0.55	0.55	0.55	1.54	1.54	1.50	2.45	1.22	2.26	
1036-1	FWD	13.82	17.00	170.00	0.00	34.00	0.00	0.00	14.78	1.4	14.85	0.20	1.91	0.48	0.42	0.60	2.40	1.54	1.53	2.47	1.20	2.29
	APT	14.82	16.00	170.00	0.00	34.00	0.00	0.00	15.88	1.0	16.80	0.20	1.90	0.52	0.52	0.65	2.42	1.54	1.53	2.47	1.20	2.29
1036-2	FWD	10.00	12.00	178.00	55.00	125.00	22.00	0.00	18.85	1.0	19.80	0.20	1.92	0.52	0.52	0.65	2.42	1.54	1.53	2.47	1.20	2.29
	APT	11.00	12.00	178.00	55.00	125.00	22.00	0.00	19.85	1.0	20.80	0.20	1.94	0.52	0.52	0.65	2.42	1.54	1.53	2.47	1.20	2.29
1037-1	FWD	9.84	17.00	172.00	-6.00	20.00	71.00	0.10	19.82	0.0	19.88	0.51	1.47	0.64	0.38	0.61	2.38	1.54	1.53	2.47	1.20	2.29
	APT	10.84	17.00	172.00	-6.00	20.00	71.00	0.10	19.82	0.0	19.88	0.51	1.47	0.64	0.38	0.61	2.38	1.54	1.53	2.47	1.20	2.29
1037-2	FWD	9.87	17.00	172.00	-5.00	20.00	75.00	0.14	19.82	0.0	19.88	0.28	1.49	0.66	0.51	0.62	2.38	1.54	1.53	2.47	1.20	2.29
	APT	10.87	17.00	172.00	-5.00	20.00	75.00	0.14	19.82	0.0	19.88	0.28	1.49	0.66	0.51	0.62	2.38	1.54	1.53	2.47	1.20	2.29
1038-1	FWD	5.65	18.00	150.00	-1.00	22.00	76.00	0.15	15.85	0.0	15.85	0.21	1.40	0.58	0.37	0.52	2.31	1.52	1.52	2.47	1.20	2.29
	APT	5.65	18.00	150.00	-1.00	22.00	76.00	0.15	15.85	0.0	15.85	0.21	1.40	0.58	0.37	0.52	2.31	1.52	1.52	2.47	1.20	2.29
1038-2	FWD	5.67	18.00	150.00	-1.00	22.00	76.00	0.15	15.85	0.0	15.85	0.21	1.40	0.58	0.37	0.52	2.31	1.52	1.52	2.47	1.20	2.29
	APT	5.67	18.00	150.00	-1.00	22.00	76.00	0.15	15.85	0.0	15.85	0.21	1.40	0.58	0.37	0.52	2.31	1.52	1.52	2.47	1.20	2.29
1039-1	FWD	6.62	27.00	140.00	0.00	40.00	63.00	0.22	70.00	0.0	71.00	0.21	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
	APT	7.62	27.00	140.00	0.00	40.00	63.00	0.22	70.00	0.0	71.00	0.21	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
1039-2	FWD	6.64	27.00	140.00	0.00	40.00	63.00	0.22	70.00	0.0	71.00	0.21	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
	APT	7.64	27.00	140.00	0.00	40.00	63.00	0.22	70.00	0.0	71.00	0.21	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
1040-1	FWD	11.22	22.00	145.00	-1.00	45.00	70.00	0.10	31.00	0.0	32.00	0.25	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
	APT	11.22	22.00	145.00	-1.00	45.00	70.00	0.10	31.00	0.0	32.00	0.25	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
1040-2	FWD	11.23	22.00	145.00	-1.00	45.00	70.00	0.10	31.00	0.0	32.00	0.25	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29
	APT	11.23	22.00	145.00	-1.00	45.00	70.00	0.10	31.00	0.0	32.00	0.25	1.47	0.63	0.58	0.77	2.39	1.78	1.78	2.47	1.20	2.29

~~TOP SECRET~~

C

SECTION A

APPENDIX

~~TOP SECRET C~~

~~TOP SECRET C~~

MISSION # 1040-1 * INSTRUMENT * FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.01	0 0	0	0 0	0 0
0.02	000 00	0	000 0	000 0
0.03	000 00	0	000 0	000 0
0.04	000 00	0	000 0	000 0
0.05	000 00	0	000 0	000 0
0.06	000 00	0	000 0	000 0
0.07	000 00	0	000 0	000 0
0.08	000 00	0	000 0	000 0
0.09	000 00	0	000 0	000 0
0.10	000 00	0	000 0	000 0
0.11	000 00	0	000 0	000 0
0.12	000 00	0	000 0	000 0
0.13	000 00	0	000 0	000 0
0.14	000 00	0	000 0	000 0
0.15	000 00	0	000 0	000 0
0.16	000 00	0	000 0	000 0
0.17	000 00	0	000 0	000 0
0.18	000 00	0	000 0	000 0
0.19	000 00	0	000 0	000 0
0.20	000 00	0	000 0	000 0
0.21	000 00	0	000 0	000 0
0.22	000 00	0	000 0	000 0
0.23	000 00	0	000 0	000 0
0.24	000 00	0	000 0	000 0
0.25	000 00	0	000 0	000 0
0.26	000 00	0	000 0	000 0
0.27	000 00	0	000 0	000 0
0.28	000 00	0	000 0	000 0
0.29	000 00	0	000 0	000 0
0.30	000 00	0	000 0	000 0
0.31	000 00	0	000 0	000 0
0.32	000 00	0	000 0	000 0
0.33	000 00	0	000 0	000 0
0.34	000 00	0	000 0	000 0
0.35	000 00	0	000 0	000 0
0.36	000 00	0	000 0	000 0
0.37	000 00	0	000 0	000 0
0.38	000 00	0	000 0	000 0
0.39	000 00	0	000 0	000 0
0.40	000 00	0	000 0	000 0
0.41	000 00	0	000 0	000 0
0.42	000 00	0	000 0	000 0
0.43	000 00	0	000 0	000 0
0.44	000 00	0	000 0	000 0
0.45	000 00	0	000 0	000 0
0.46	000 00	0	000 0	000 0
0.47	000 00	0	000 0	000 0
0.48	000 00	0	000 0	000 0
0.49	000 00	0	000 0	000 0
0.50	000 00	0	000 0	000 0
SUBTOTAL	1	0	17	21
				39

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION # 1040-1 * INSTRUMENT # FWD 5/23/67 DENSITY FREQ. DISTR.

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.51	0 0	0 0	4 0	6 0
0.52	0 0	0 0	0 0	0 0
0.53	0 0	0 0	0 0	0 0
0.54	0 0	0 0	0 0	0 0
0.55	0 0	0 0	0 0	0 0
0.56	0 0	0 0	0 0	0 0
0.57	0 0	0 0	0 0	0 0
0.58	0 0	0 0	0 0	0 0
0.59	0 0	0 0	0 0	0 0
0.60	0 0	0 0	0 0	0 0
0.61	0 0	0 0	0 0	0 0
0.62	0 0	0 0	0 0	0 0
0.63	0 0	0 0	0 0	0 0
0.64	0 0	0 0	0 0	0 0
0.65	0 0	0 0	0 0	0 0
0.66	0 0	0 0	0 0	0 0
0.67	0 0	0 0	0 0	0 0
0.68	0 0	0 0	0 0	0 0
0.69	0 0	0 0	0 0	0 0
0.70	0 0	0 0	0 0	0 0
0.71	0 0	0 0	0 0	0 0
0.72	0 0	0 0	0 0	0 0
0.73	0 0	0 0	0 0	0 0
0.74	0 0	0 0	0 0	0 0
0.75	0 0	0 0	0 0	0 0
0.76	0 0	0 0	0 0	0 0
0.77	0 0	0 0	0 0	0 0
0.78	0 0	0 0	0 0	0 0
0.79	0 0	0 0	0 0	0 0
0.80	0 0	0 0	0 0	0 0
0.81	0 0	0 0	0 0	0 0
0.82	0 0	0 0	0 0	0 0
0.83	0 0	0 0	0 0	0 0
0.84	0 0	0 0	0 0	0 0
0.85	0 0	0 0	0 0	0 0
0.86	0 0	0 0	0 0	0 0
0.87	0 0	0 0	0 0	0 0
0.88	0 0	0 0	0 0	0 0
0.89	0 0	0 0	0 0	0 0
0.90	0 0	0 0	0 0	0 0
0.91	0 0	0 0	0 0	0 0
0.92	0 0	0 0	0 0	0 0
0.93	0 0	0 0	0 0	0 0
0.94	0 0	0 0	0 0	0 0
0.95	0 0	0 0	0 0	0 0
0.96	0 0	0 0	0 0	0 0
0.97	0 0	0 0	0 0	0 0
0.98	0 0	0 0	0 0	0 0
0.99	0 0	0 0	0 0	0 0
1.00	200 0	0 0	51 0	103 0
SUBTOTAL	200 0	0 0	0 0	156 0

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * FWD 5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01	0 0	0	4	0 0
1.02	0 0	0	0	0 0
1.03	0 0	0	0	0 0
1.04	0 0	0	0	0 0
1.05	0 0	0	0	0 0
1.06	0 0	0	0	0 0
1.07	0 0	0	0	0 0
1.08	0 0	0	0	0 0
1.09	0 0	0	0	0 0
1.10	0 0	0	0	0 0
1.11	0 0	0	0	0 0
1.12	0 0	0	0	0 0
1.13	0 0	0	0	0 0
1.14	0 0	0	0	0 0
1.15	0 0	0	0	0 0
1.16	0 0	0	0	0 0
1.17	0 0	0	0	0 0
1.18	0 0	0	0	0 0
1.19	0 0	0	0	0 0
1.20	0 0	0	0	0 0
1.21	0 0	0	0	0 0
1.22	0 0	0	0	0 0
1.23	0 0	0	0	0 0
1.24	0 0	0	0	0 0
1.25	0 0	0	0	0 0
1.26	0 0	0	0	0 0
1.27	0 0	0	0	0 0
1.28	0 0	0	0	0 0
1.29	0 0	0	0	0 0
1.30	0 0	0	0	0 0
1.31	0 0	0	0	0 0
1.32	0 0	0	0	0 0
1.33	0 0	0	0	0 0
1.34	0 0	0	0	0 0
1.35	0 0	0	0	0 0
1.36	0 0	0	0	0 0
1.37	0 0	0	0	0 0
1.38	0 0	0	0	0 0
1.39	0 0	0	0	0 0
1.40	0 0	0	0	0 0
1.41	0 0	0	0	0 0
1.42	0 0	0	0	0 0
1.43	0 0	0	0	0 0
1.44	0 0	0	0	0 0
1.45	0 0	0	0	0 0
1.46	0 0	0	0	0 0
1.47	0 0	0	0	0 0
1.48	0 0	0	0	0 0
1.49	0 0	0	0	0 0
1.50	0 0	0	0	0 0
SUBTOTAL	0 0	0	17	20 20

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * FWD

5/23/67 DENSITY FREQ.DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.51	0 0	0	0	0 0
1.52	0 0	0	0	0 0
1.53	0 0	0	0	0 0
1.54	0 0	0	0	0 0
1.55	0 0	0	0	0 0
1.56	0 0	0	0	0 0
1.57	0 0	0	0	0 0
1.58	0 0	0	0	0 0
1.59	0 0	0	0	0 0
1.60	0 0	0	0	0 0
1.61	0 0	0	0	0 0
1.62	0 0	0	0	0 0
1.63	0 0	0	0	0 0
1.64	0 0	0	0	0 0
1.65	0 0	0	0	0 0
1.66	0 0	0	0	0 0
1.67	0 0	0	0	0 0
1.68	0 0	0	0	0 0
1.69	0 0	0	0	0 0
1.70	0 0	0	0	0 0
1.71	0 0	0	0	0 0
1.72	0 0	0	0	0 0
1.73	0 0	0	0	0 0
1.74	0 0	0	0	0 0
1.75	0 0	0	0	0 0
1.76	0 0	0	0	0 0
1.77	0 0	0	0	0 0
1.78	0 0	0	0	0 0
1.79	0 0	0	0	0 0
1.80	0 0	0	0	0 0
1.81	0 0	0	0	0 0
1.82	0 0	0	0	0 0
1.83	0 0	0	0	0 0
1.84	0 0	0	0	0 0
1.85	0 0	0	0	0 0
1.86	0 0	0	0	0 0
1.87	0 0	0	0	0 0
1.88	0 0	0	0	0 0
1.89	0 0	0	0	0 0
1.90	0 0	0	0	0 0
1.91	0 0	0	0	0 0
1.92	0 0	0	0	0 0
1.93	0 0	0	0	0 0
1.94	0 0	0	0	0 0
1.95	0 0	0	0	0 0
1.96	0 0	0	0	0 0
1.97	0 0	0	0	0 0
1.98	0 0	0	0	0 0
1.99	0 0	0	0	0 0
2.00	0 0	0	0	0 0
SUBTOTAL	0 0	0 0	0 0	0 0

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * FWD

5/23/67 DENSITY-FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0 0	0	0	1
2.02	0 0	0	0	1
2.03	0 0	0	0	1
2.04	0 0	0	0	1
2.05	0 0	0	0	1
2.06	0 0	0	0	1
2.07	0 0	0	0	1
2.08	0 0	0	0	1
2.09	0 0	0	0	1
2.10	0 0	0	0	1
2.11	0 0	0	0	1
2.12	0 0	0	0	1
2.13	0 0	0	0	1
2.14	0 0	0	0	1
2.15	0 0	0	0	1
2.16	0 0	0	0	1
2.17	0 0	0	0	1
2.18	0 0	0	0	1
2.19	0 0	0	0	1
2.20	0 0	0	0	1
2.21	0 0	0	0	1
2.22	0 0	0	0	1
2.23	0 0	0	0	1
2.24	0 0	0	0	1
2.25	0 0	0	0	1
2.26	0 0	0	0	1
2.27	0 0	0	0	1
2.28	0 0	0	0	1
2.29	0 0	0	0	1
2.30	0 0	0	0	1
2.31	0 0	0	0	1
2.32	0 0	0	0	1
2.33	0 0	0	0	1
2.34	0 0	0	0	1
2.35	0 0	0	0	1
2.36	0 0	0	0	1
2.37	0 0	0	0	1
2.38	0 0	0	0	1
2.39	0 0	0	0	1
2.40	0 0	0	0	1
2.41	0 0	0	0	1
2.42	0 0	0	0	1
2.43	0 0	0	0	1
2.44	0 0	0	0	1
2.45	0 0	0	0	1
2.46	0 0	0	0	1
2.47	0 0	0	0	1
2.48	0 0	0	0	1
2.49	0 0	0	0	1
2.50	0 0	0	0	1
SUBTOTAL	0 0	0	0	0
		19	16	27
			98	47
				114

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION # 1040-1 * INSTRUMENT * FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	3	3	3	76	76	61	137	138	121	216	217	185

MISSION 1040-1 INSTR - FWD

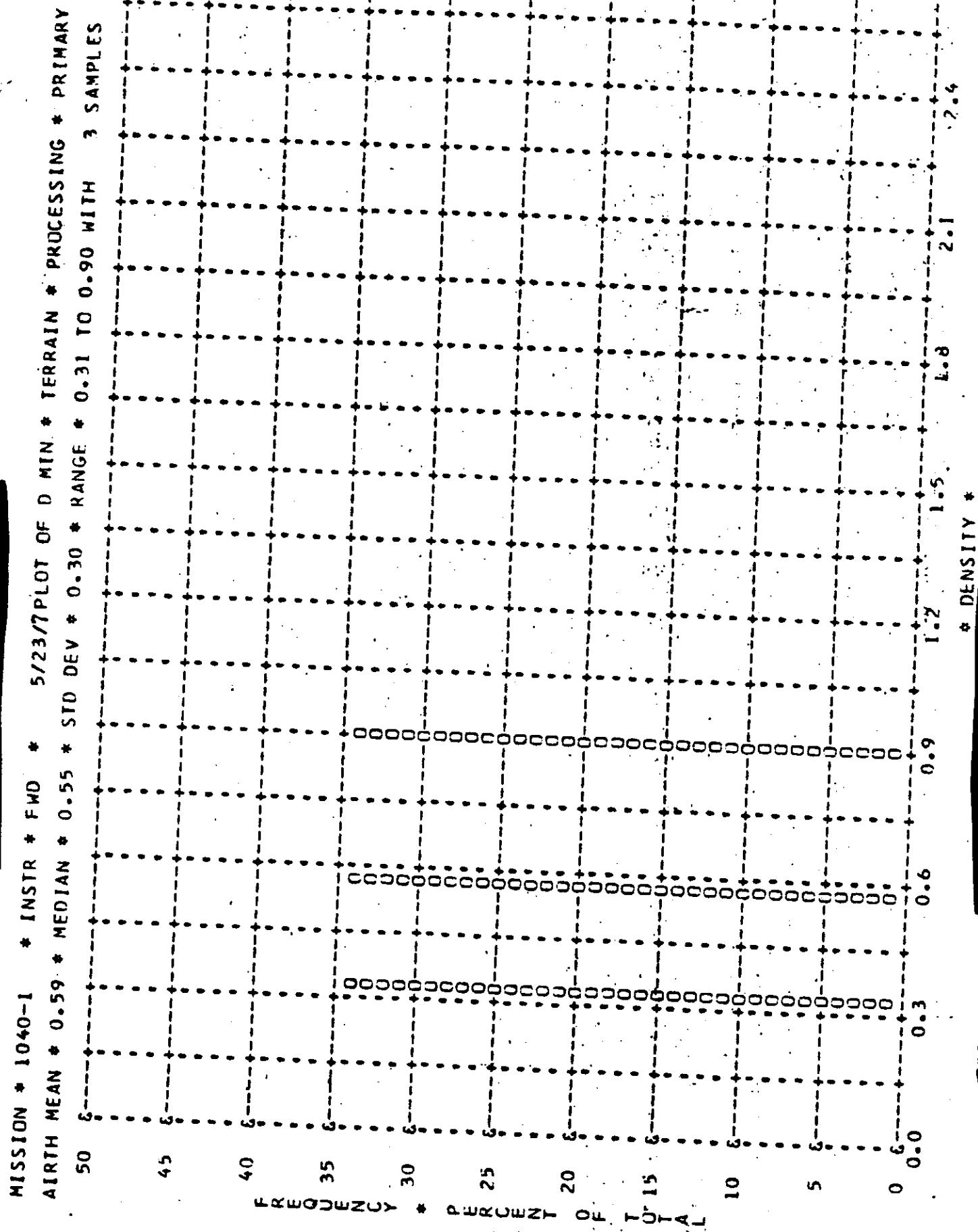
5/23/

PROCESSING AND EXPOSURE AT

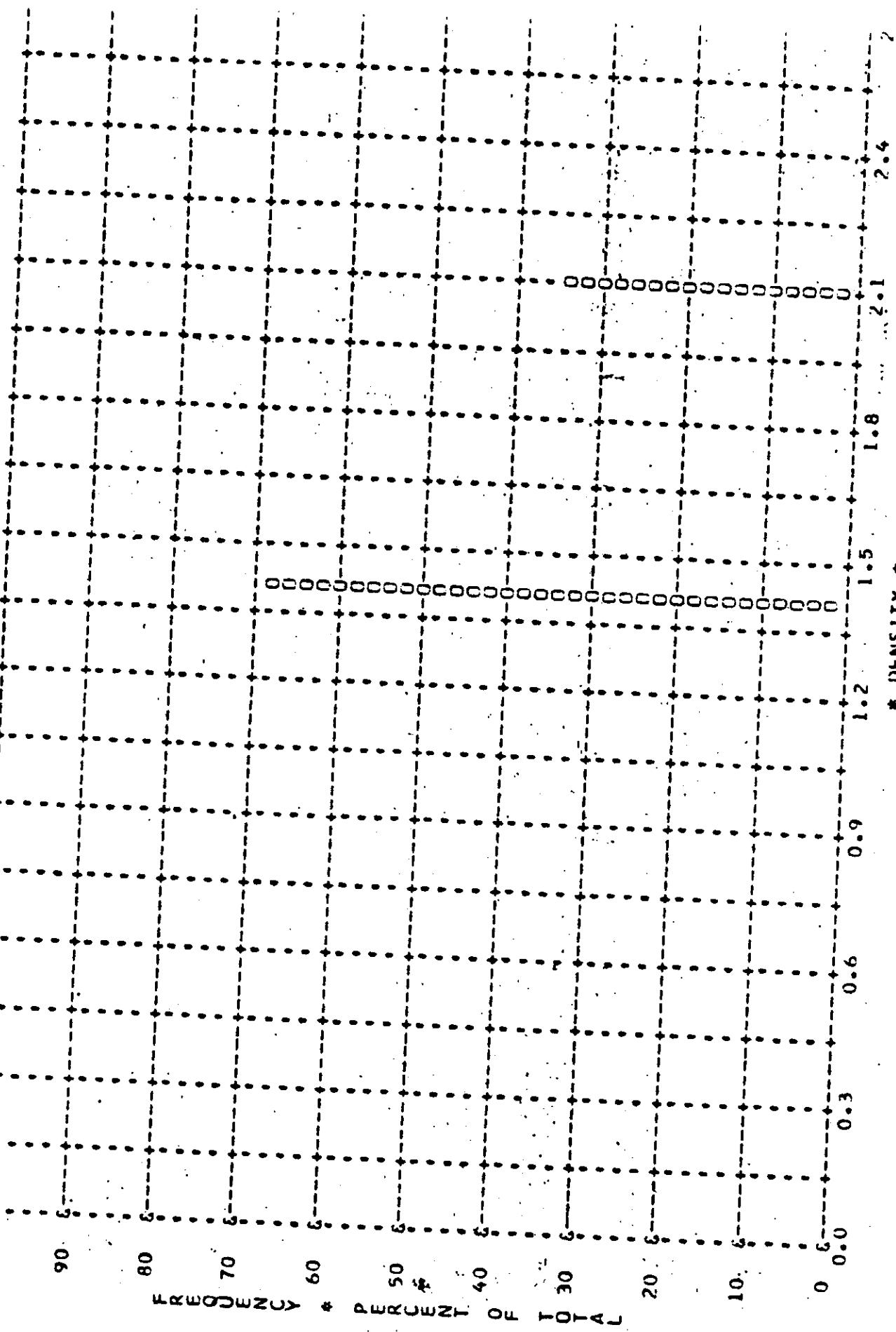
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXP
PRIMARY	3	0 PC	33 PC	67 PC	0 PC	0
INTERMEDIATE	76	0 PC	7 PC	74 PC	20 PC	20
FULL	137	1 PC	0 PC	82 PC	16 PC	16
ALL LEVELS	216	0 PC	3 PC	79 PC	17 PC	17
PROCESS LEVEL	BASE & FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXP
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70

~~TOP SECRET C~~

TABLE A-1



TOP SECRET C [REDACTED]
MISSION * 1040-1 * INSTR * FWD * 5/23/77 PLOT OF D MAX * TERRAIN * PROCESSING * PRIMARY
AIRTH MEAN * 1.63 * MEDIAN * 1.41 * STD DFV * 0.40 * RANGE * 1.39 TO 2.10 WITH 3 SAMPLES



TOP SECRET C

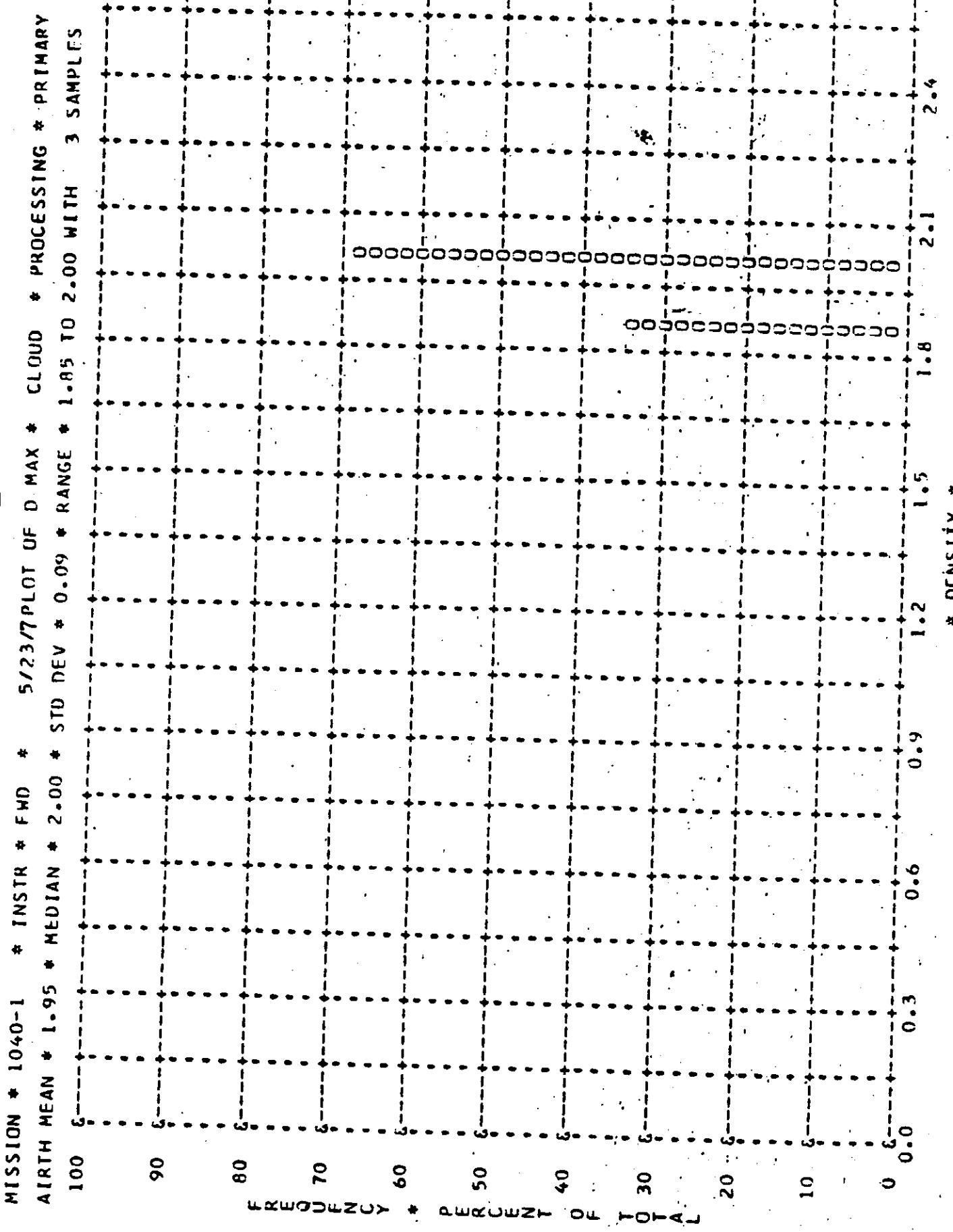


FIGURE A-9

TOP SECRET C

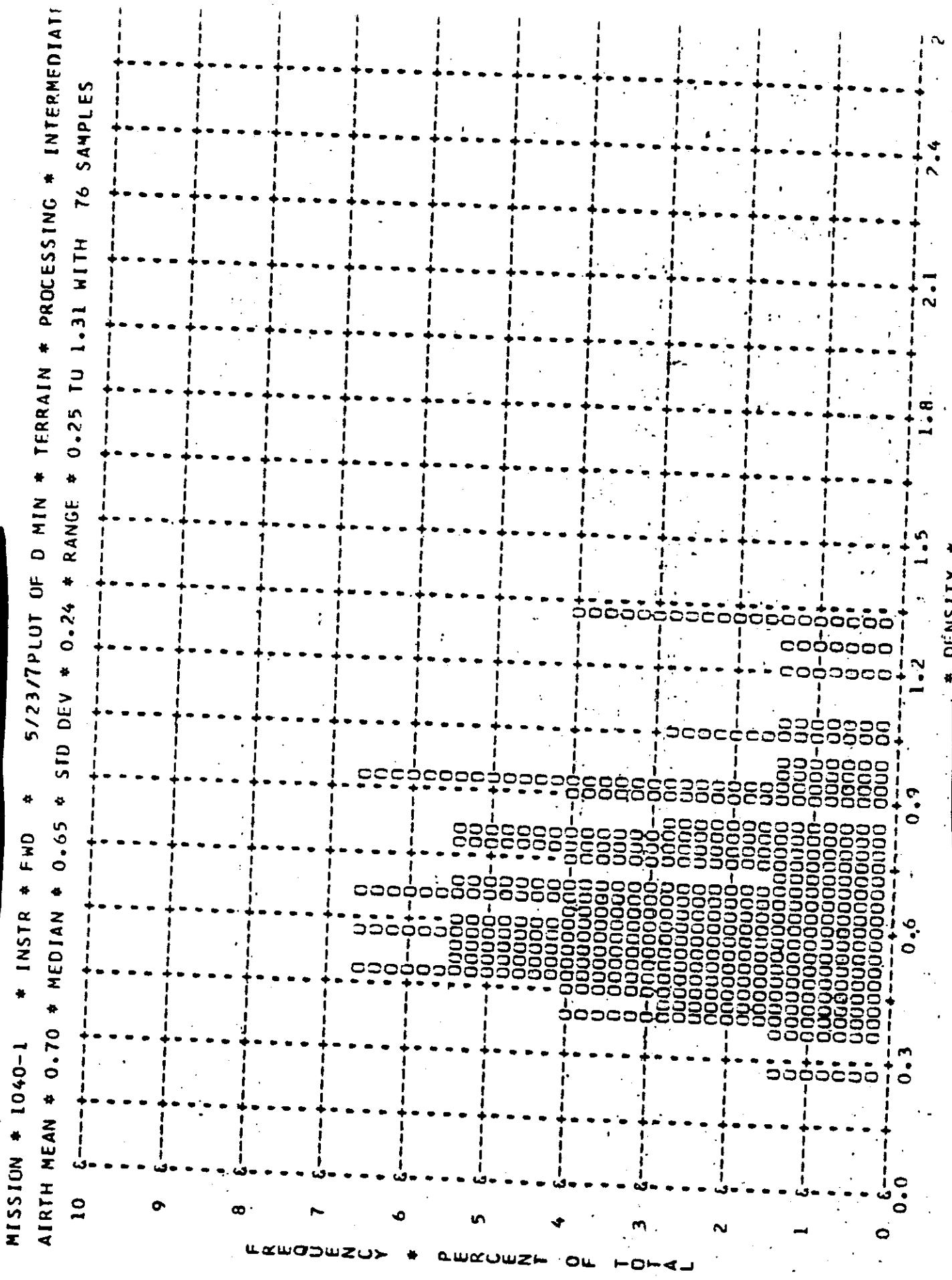
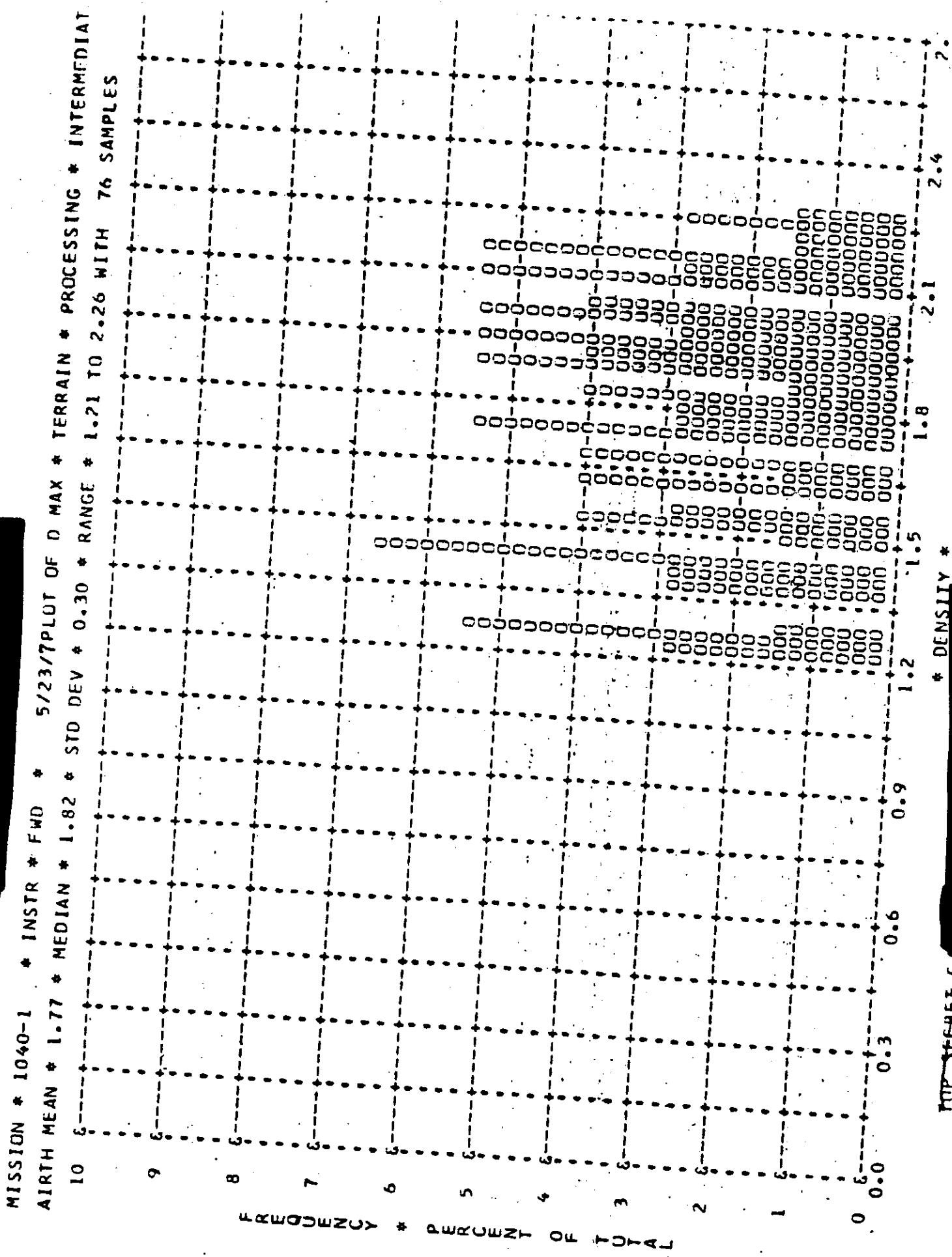
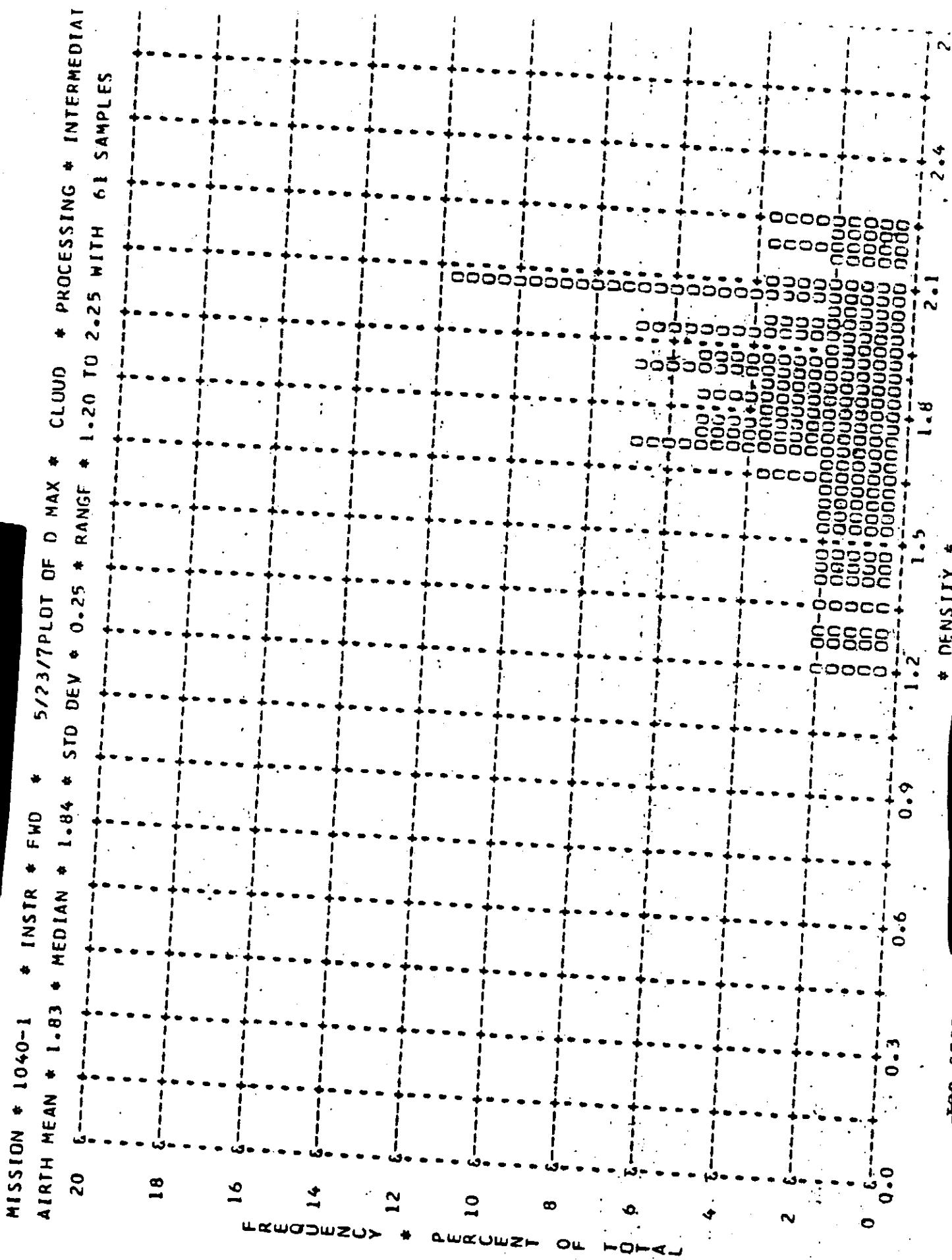


FIGURE A-1

TOP SECRET C



TOP SECRET C



TOP SECRET C

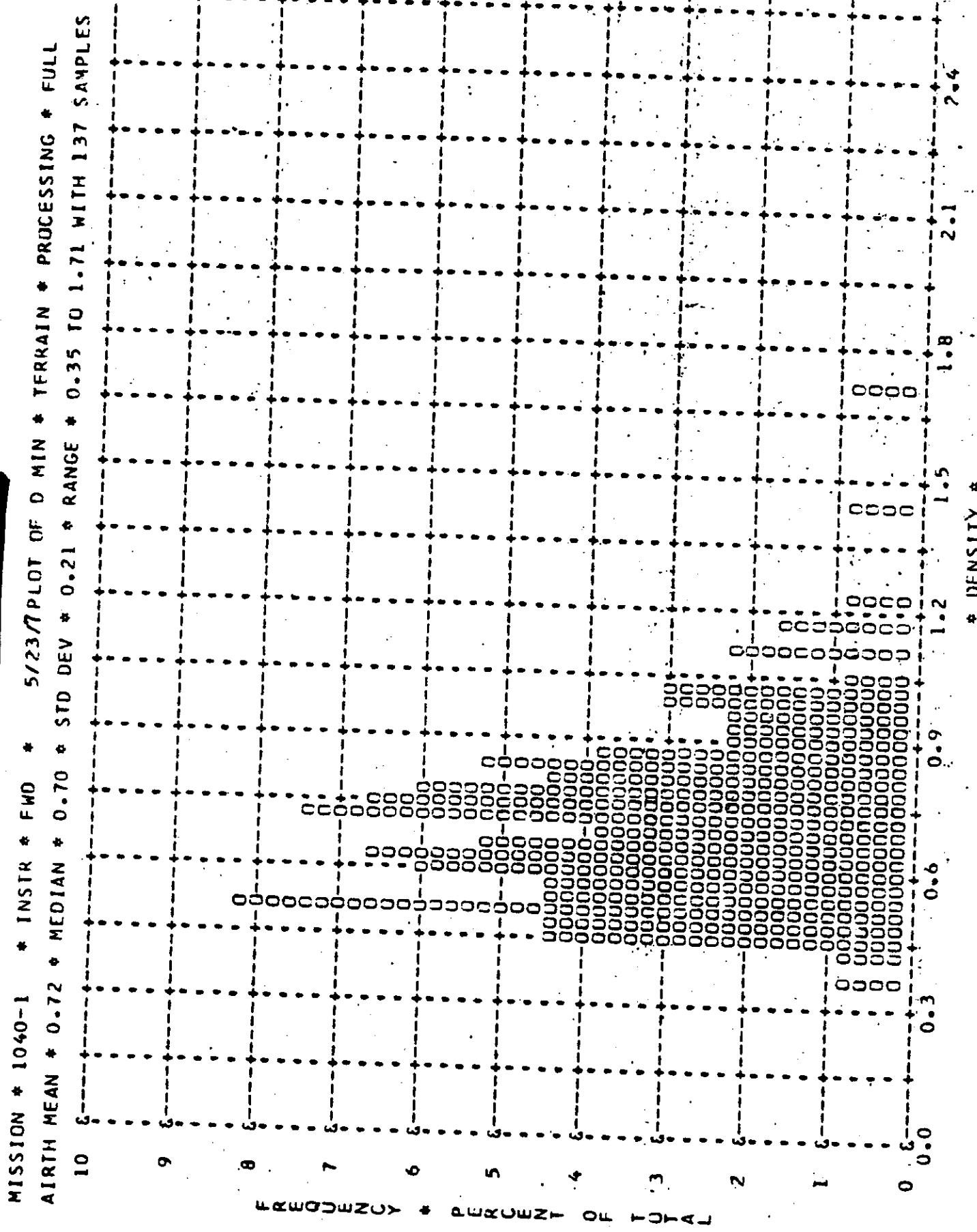
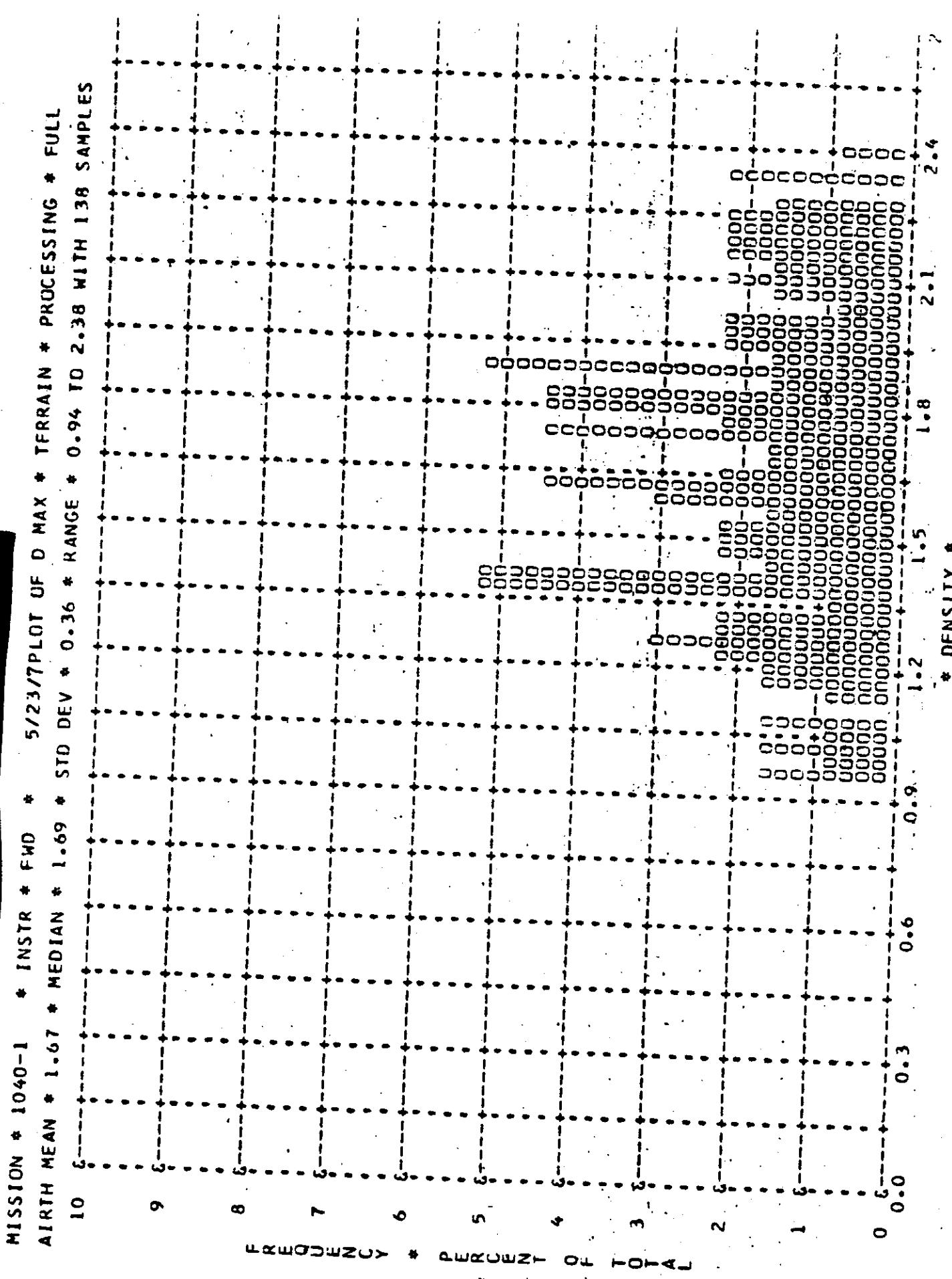
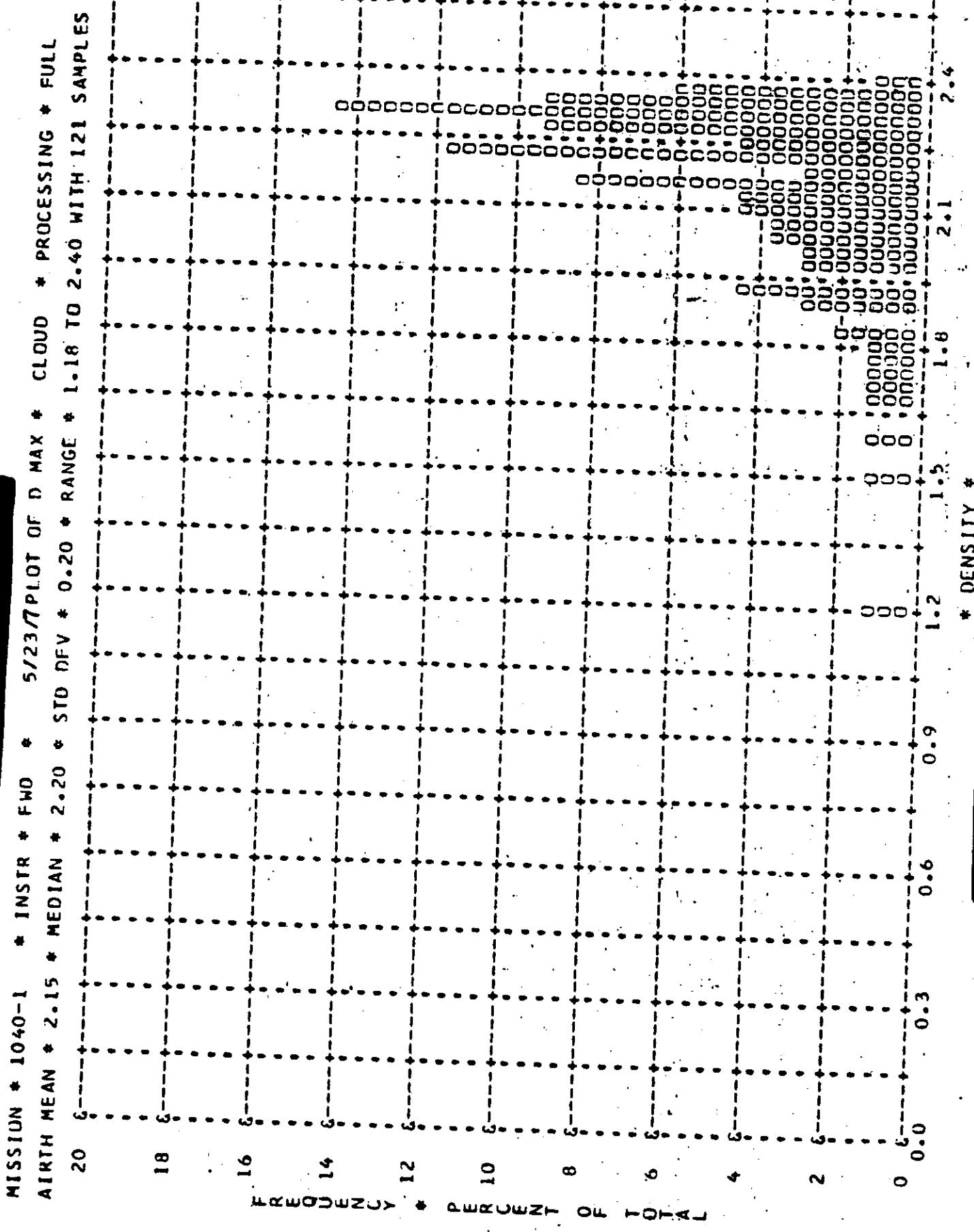


FIGURE A-7

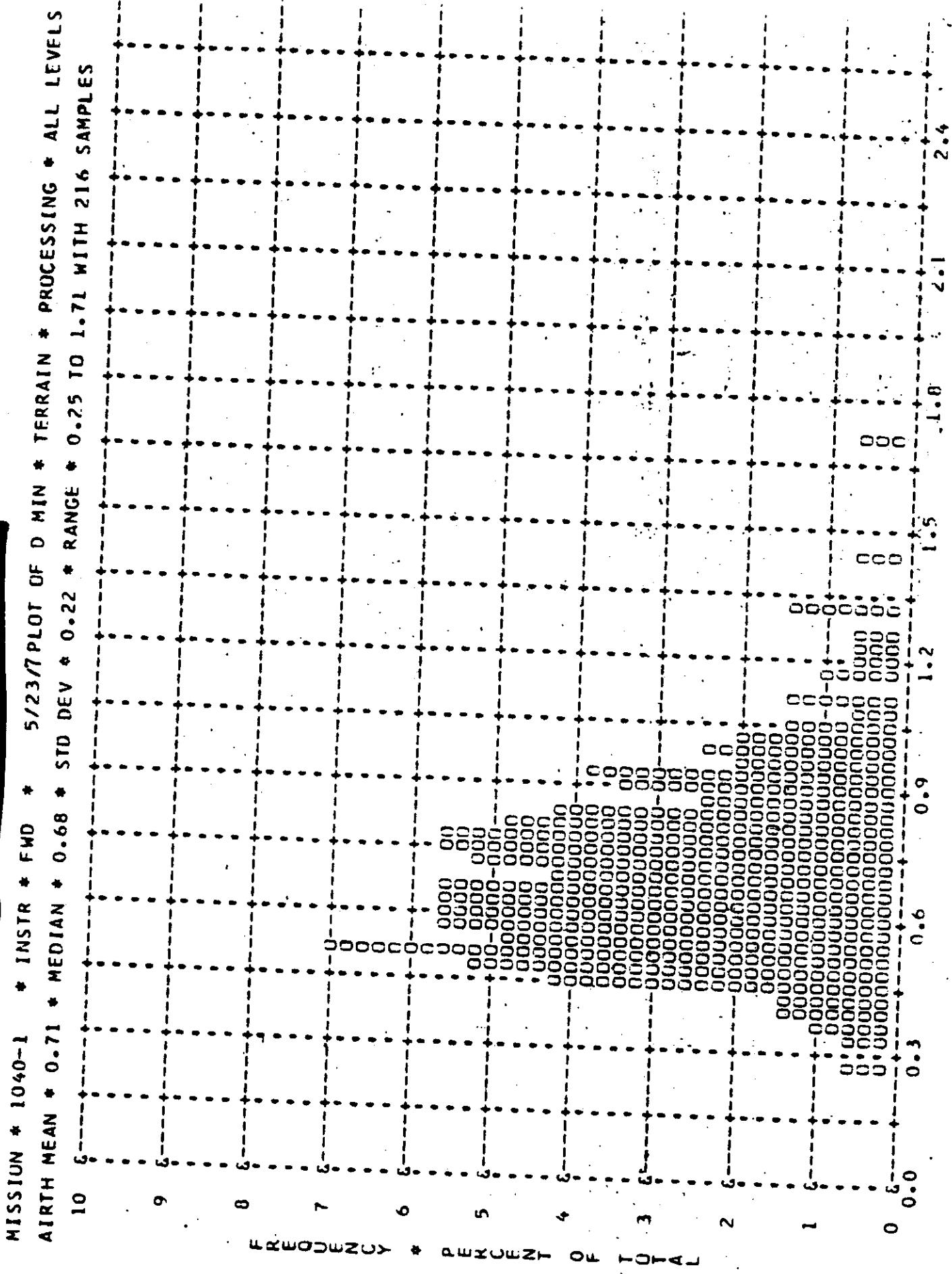
TOP SECRET C



TOP SECRET C



TOP SECRET C



TOP SECRET C

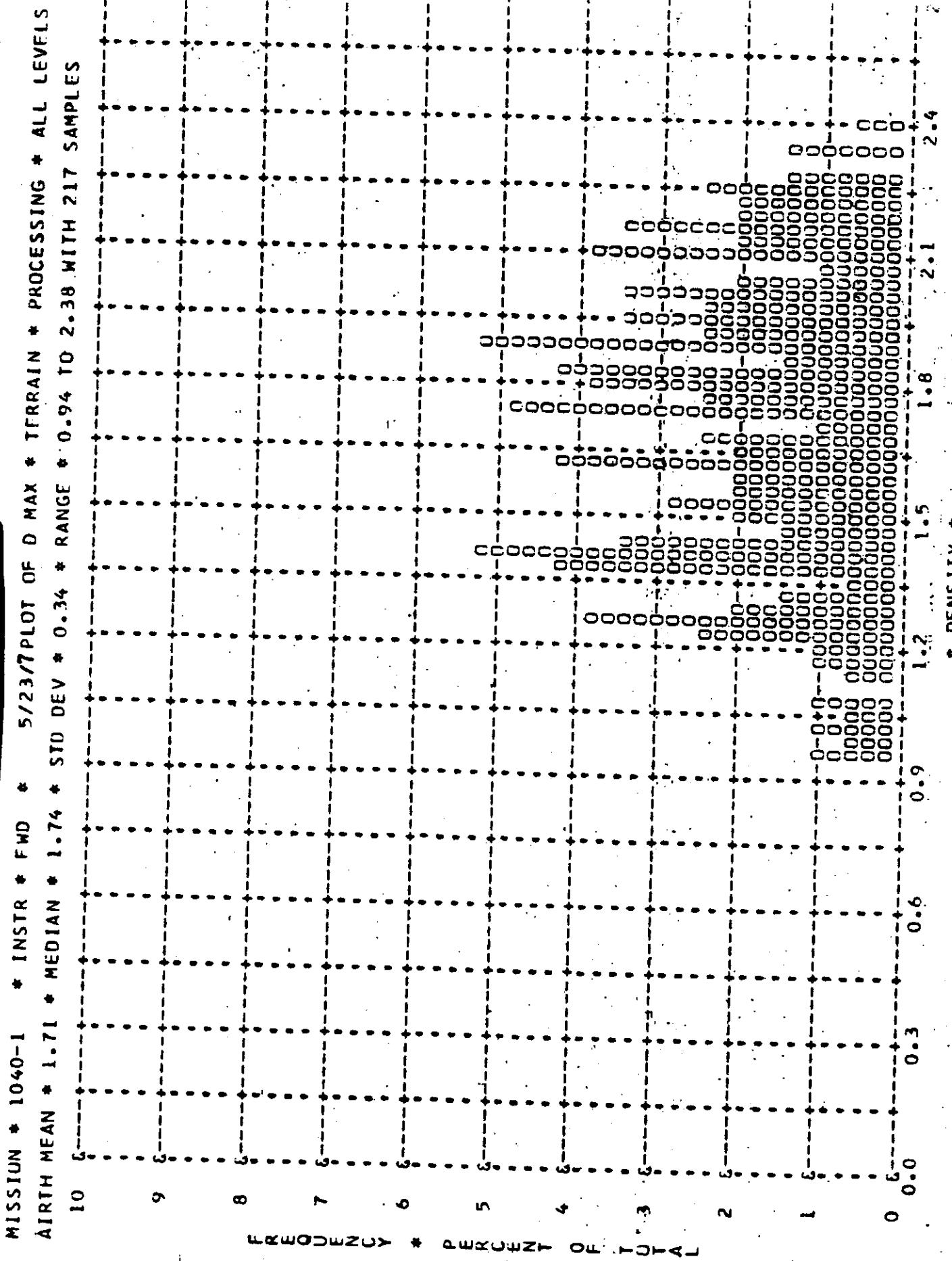


FIGURE A-11

TOP SECRET C

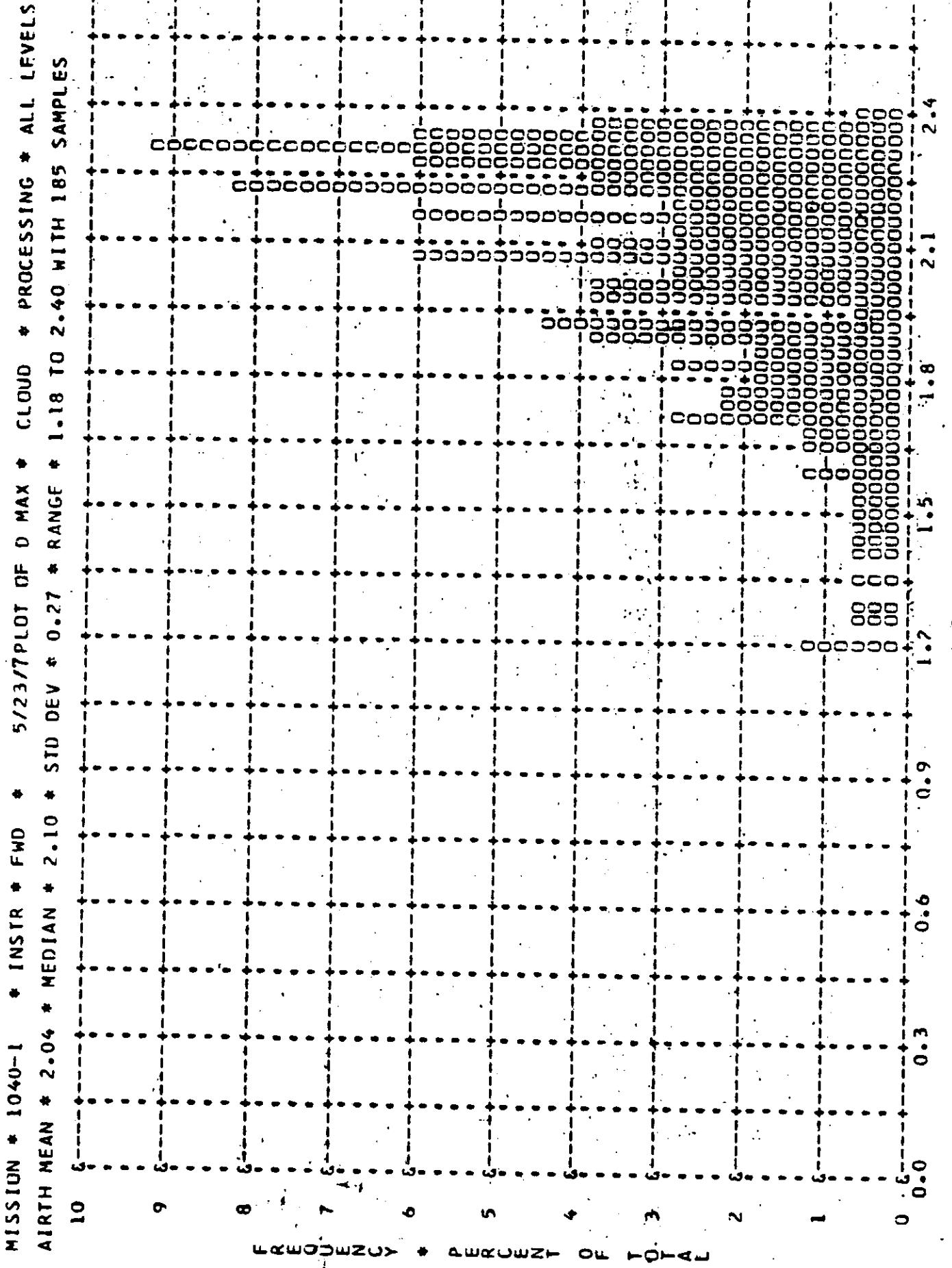


FIGURE A-12

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM.	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.01	0	0	0	0
0.02	0	0	0	0
0.03	0	0	0	0
0.04	0	0	0	0
0.05	0	0	0	0
0.06	0	0	0	0
0.07	0	0	0	0
0.08	0	0	0	0
0.09	0	0	0	0
0.10	0	0	0	0
0.11	0	0	0	0
0.12	0	0	0	0
0.13	0	0	0	0
0.14	0	0	0	0
0.15	0	0	0	0
0.16	0	0	0	0
0.17	0	0	0	0
0.18	0	0	0	0
0.19	0	0	0	0
0.20	0	0	0	0
0.21	0	0	0	0
0.22	0	0	0	0
0.23	0	0	0	0
0.24	0	0	0	0
0.25	0	0	0	0
0.26	0	0	0	0
0.27	0	0	0	0
0.28	0	0	0	0
0.29	0	0	0	0
0.30	0	0	0	0
0.31	0	0	0	0
0.32	0	0	0	0
0.33	0	0	0	0
0.34	0	0	0	0
0.35	0	0	0	0
0.36	0	0	0	0
0.37	0	0	0	0
0.38	0	0	0	0
0.39	0	0	0	0
0.40	0	0	0	0
0.41	0	0	0	0
0.42	0	0	0	0
0.43	0	0	0	0
0.44	0	0	0	0
0.45	0	0	0	0
0.46	0	0	0	0
0.47	0	0	0	0
0.48	0	0	0	0
0.49	0	0	0	0
0.50	0	0	0	0
SUBTOTAL	5	34	24	63543

~~TOP SECRET C~~

TABLE A-2

TOP SECRET C

MISSION * 1040-1 * INSTRUMENT * AET

5/23/67 DENSITY FRQ DISTR

TOP SECRET C

TABLE A-2

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
1.01	0	0	0	0	0	0	0	0
1.02	0	0	0	0	0	0	0	0
1.03	0	0	0	0	0	0	0	0
1.04	0	0	0	0	0	0	0	0
1.05	0	0	0	0	0	0	0	0
1.06	0	0	0	0	0	0	0	0
1.07	0	0	0	0	0	0	0	0
1.08	0	0	0	0	0	0	0	0
1.09	0	0	0	0	0	0	0	0
1.10	0	0	0	0	0	0	0	0
1.11	0	0	0	0	0	0	0	0
1.12	0	0	0	0	0	0	0	0
1.13	0	0	0	0	0	0	0	0
1.14	0	0	0	0	0	0	0	0
1.15	0	0	0	0	0	0	0	0
1.16	0	0	0	0	0	0	0	0
1.17	0	0	0	0	0	0	0	0
1.18	0	0	0	0	0	0	0	0
1.19	0	0	0	0	0	0	0	0
1.20	0	0	0	0	0	0	0	0
1.21	0	0	0	0	0	0	0	0
1.22	0	0	0	0	0	0	0	0
1.23	0	0	0	0	0	0	0	0
1.24	0	0	0	0	0	0	0	0
1.25	0	0	0	0	0	0	0	0
1.26	0	0	0	0	0	0	0	0
1.27	0	0	0	0	0	0	0	0
1.28	0	0	0	0	0	0	0	0
1.29	0	0	0	0	0	0	0	0
1.30	0	0	0	0	0	0	0	0
1.31	0	0	0	0	0	0	0	0
1.32	0	0	0	0	0	0	0	0
1.33	0	0	0	0	0	0	0	0
1.34	0	0	0	0	0	0	0	0
1.35	0	0	0	0	0	0	0	0
1.36	0	0	0	0	0	0	0	0
1.37	0	0	0	0	0	0	0	0
1.38	0	0	0	0	0	0	0	0
1.39	0	0	0	0	0	0	0	0
1.40	0	0	0	0	0	0	0	0
1.41	0	0	0	0	0	0	0	0
1.42	0	0	0	0	0	0	0	0
1.43	0	0	0	0	0	0	0	0
1.44	0	0	0	0	0	0	0	0
1.45	0	0	0	0	0	0	0	0
1.46	0	0	0	0	0	0	0	0
1.47	0	0	0	0	0	0	0	0
1.48	0	0	0	0	0	0	0	0
1.49	0	0	0	0	0	0	0	0
1.50	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	4	2	7	40	13	9
							37	
								16
								81

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * AFT 5/23/67 DENSITY FRQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.51	0 0	0	0	0 0
1.52	0 0	0	0	0 0
1.53	0 0	0	0	0 0
1.54	0 0	0	0	0 0
1.55	0 0	0	0	0 0
1.56	0 0	0	0	0 0
1.57	0 0	0	0	0 0
1.58	0 0	0	0	0 0
1.59	0 0	0	0	0 0
1.60	0 0	0	0	0 0
1.61	0 0	0	0	0 0
1.62	0 0	0	0	0 0
1.63	0 0	0	0	0 0
1.64	0 0	0	0	0 0
1.65	0 0	0	0	0 0
1.66	0 0	0	0	0 0
1.67	0 0	0	0	0 0
1.68	0 0	0	0	0 0
1.69	0 0	0	0	0 0
1.70	0 0	0	0	0 0
1.71	0 0	0	0	0 0
1.72	0 0	0	0	0 0
1.73	0 0	0	0	0 0
1.74	0 0	0	0	0 0
1.75	0 0	0	0	0 0
1.76	0 0	0	0	0 0
1.77	0 0	0	0	0 0
1.78	0 0	0	0	0 0
1.79	0 0	0	0	0 0
1.80	0 0	0	0	0 0
1.81	0 0	0	0	0 0
1.82	0 0	0	0	0 0
1.83	0 0	0	0	0 0
1.84	0 0	0	0	0 0
1.85	0 0	0	0	0 0
1.86	0 0	0	0	0 0
1.87	0 0	0	0	0 0
1.88	0 0	0	0	0 0
1.89	0 0	0	0	0 0
1.90	0 0	0	0	0 0
1.91	0 0	0	0	0 0
1.92	0 0	0	0	0 0
1.93	0 0	0	0	0 0
1.94	0 0	0	0	0 0
1.95	0 0	0	0	0 0
1.96	0 0	0	0	0 0
1.97	0 0	0	0	0 0
1.98	0 0	0	0	0 0
1.99	0 0	0	0	0 0
2.00	0 0	0	0	0 0
SUBTOTAL	0 3	0 0	55 39	107 50

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0 0	0 0	0 2	0 3
2.02	0 0	0 0	1 1	1 3
2.03	0 0	0 0	0 0	1 1
2.04	0 0	0 0	0 0	1 1
2.05	0 0	0 0	0 0	1 1
2.06	0 0	0 0	0 0	1 1
2.07	0 0	0 0	0 0	1 1
2.08	0 0	0 0	0 0	1 1
2.09	0 0	0 0	0 0	1 1
2.10	0 0	0 0	0 0	1 1
2.11	0 0	0 0	0 0	1 1
2.12	0 0	0 0	0 0	1 1
2.13	0 0	0 0	0 0	1 1
2.14	0 0	0 0	0 0	1 1
2.15	0 0	0 0	0 0	1 1
2.16	0 0	0 0	0 0	1 1
2.17	0 0	0 0	0 0	1 1
2.18	0 0	0 0	0 0	1 1
2.19	0 0	0 0	0 0	1 1
2.20	0 0	0 0	0 0	1 1
2.21	0 0	0 0	0 0	1 1
2.22	0 0	0 0	0 0	1 1
2.23	0 0	0 0	0 0	1 1
2.24	0 0	0 0	0 0	1 1
2.25	0 0	0 0	0 0	1 1
2.26	0 0	0 0	0 0	1 1
2.27	0 0	0 0	0 0	1 1
2.28	0 0	0 0	0 0	1 1
2.29	0 0	0 0	0 0	1 1
2.30	0 0	0 0	0 0	1 1
2.31	0 0	0 0	0 0	1 1
2.32	0 0	0 0	0 0	1 1
2.33	0 0	0 0	0 0	1 1
2.34	0 0	0 0	0 0	1 1
2.35	0 0	0 0	0 0	1 1
2.36	0 0	0 0	0 0	1 1
2.37	0 0	0 0	0 0	1 1
2.38	0 0	0 0	0 0	1 1
2.39	0 0	0 0	0 0	1 1
2.40	0 0	0 0	0 0	1 1
2.41	0 0	0 0	0 0	1 1
2.42	0 0	0 0	0 0	1 1
2.43	0 0	0 0	0 0	1 1
2.44	0 0	0 0	0 0	1 1
2.45	0 0	0 0	0 0	1 1
2.46	0 0	0 0	0 0	1 1
2.47	0 0	0 0	0 0	1 1
2.48	0 0	0 0	0 0	1 1
2.49	0 0	0 0	0 0	1 1
2.50	0 0	0 0	0 0	1 1
SUBTOTAL	0 0	0 0	24 33	61 114

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~

MISSION * 1040-1 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	6	7	2	121	122	86	103	106	92	230	235	180

MISSION 1040-1 INSTR - AFT

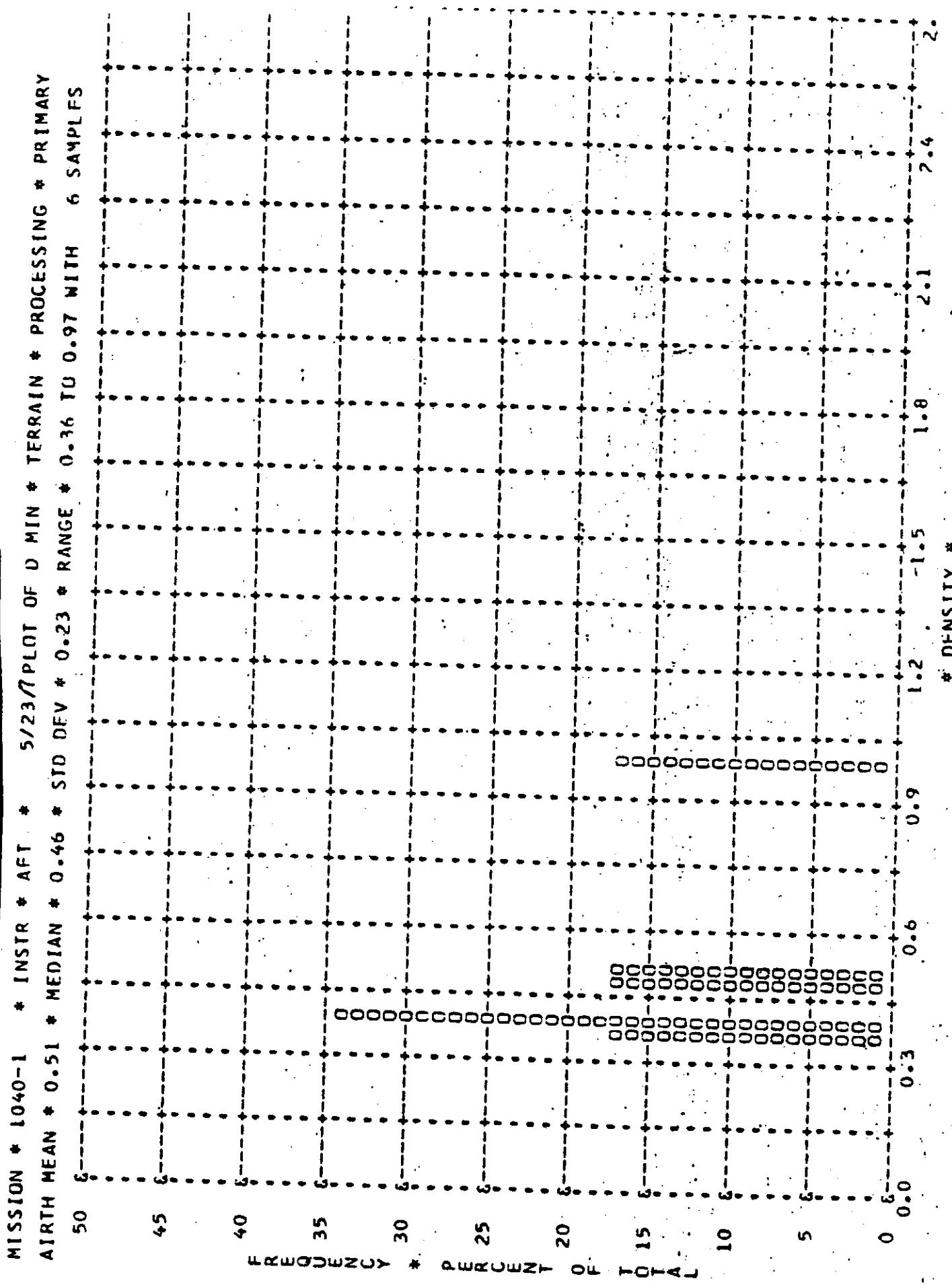
5/23/ PROCESSING AND EXPOSURE ANALYS.

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	6	0 PC	50 PC	33 PC	0 PC	17 PC
INTERMEDIATE	121	0 PC	9 PC	.78 PC	12 PC	1 PC
FULL	103	3 PC	0 PC	.83 PC	14 PC	0 PC
ALL LEVELS	230	1 PC	6 PC	.79 PC	13 PC	1 PC
PROCESS LEVEL	BASE & FUG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~



~~TOP SECRET C~~

FIGURE A-1.

TOP SECRET C

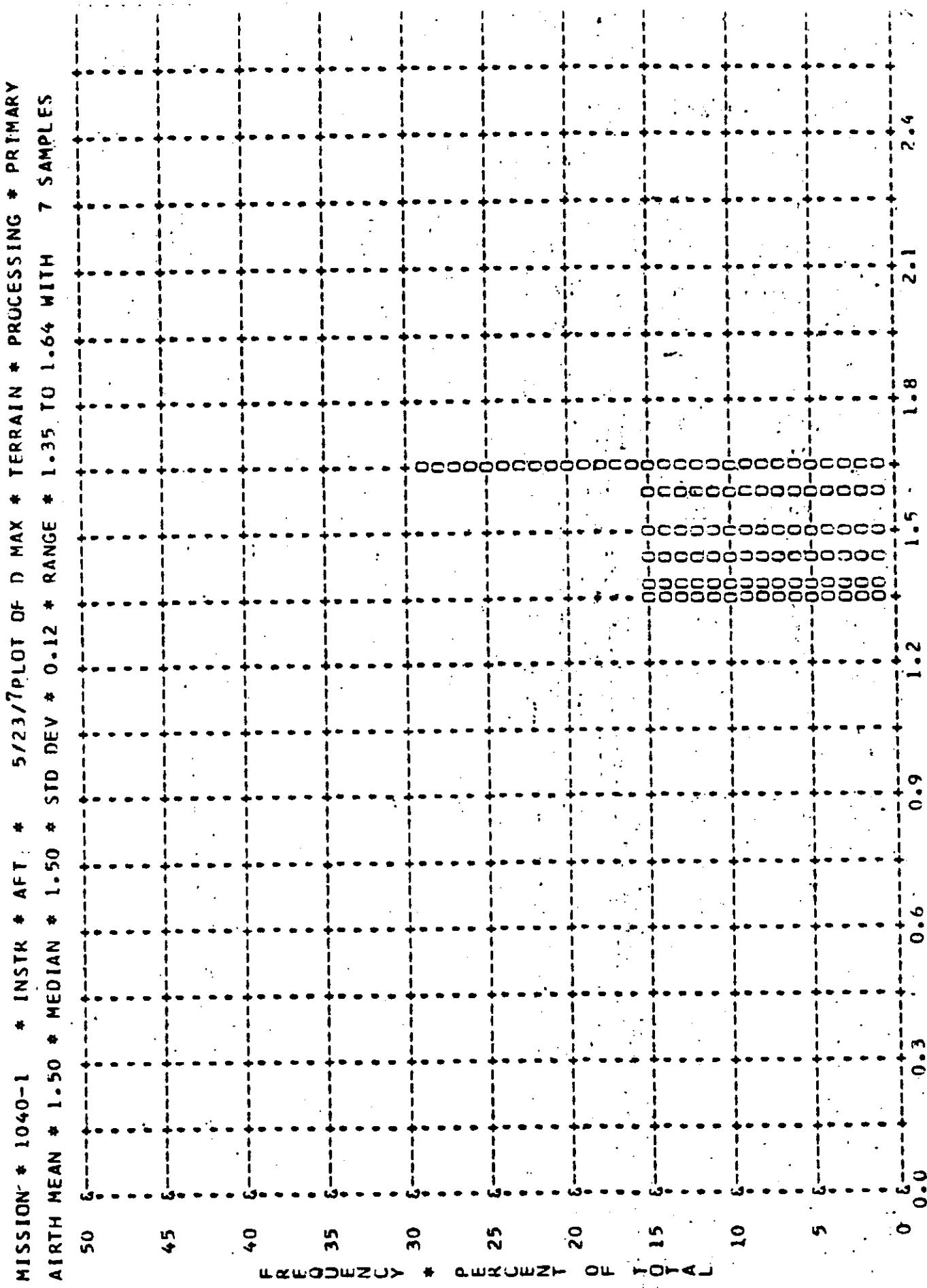
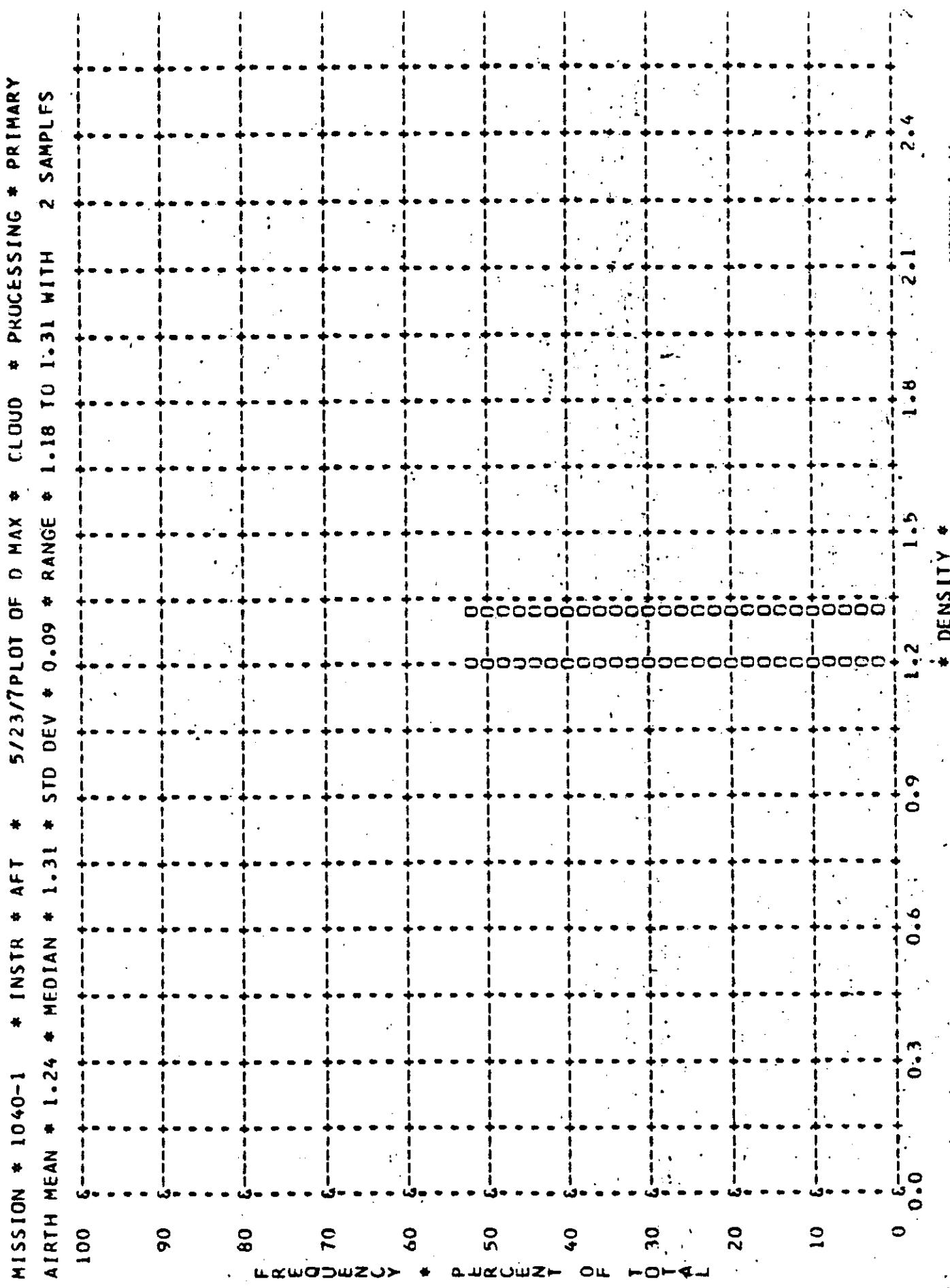


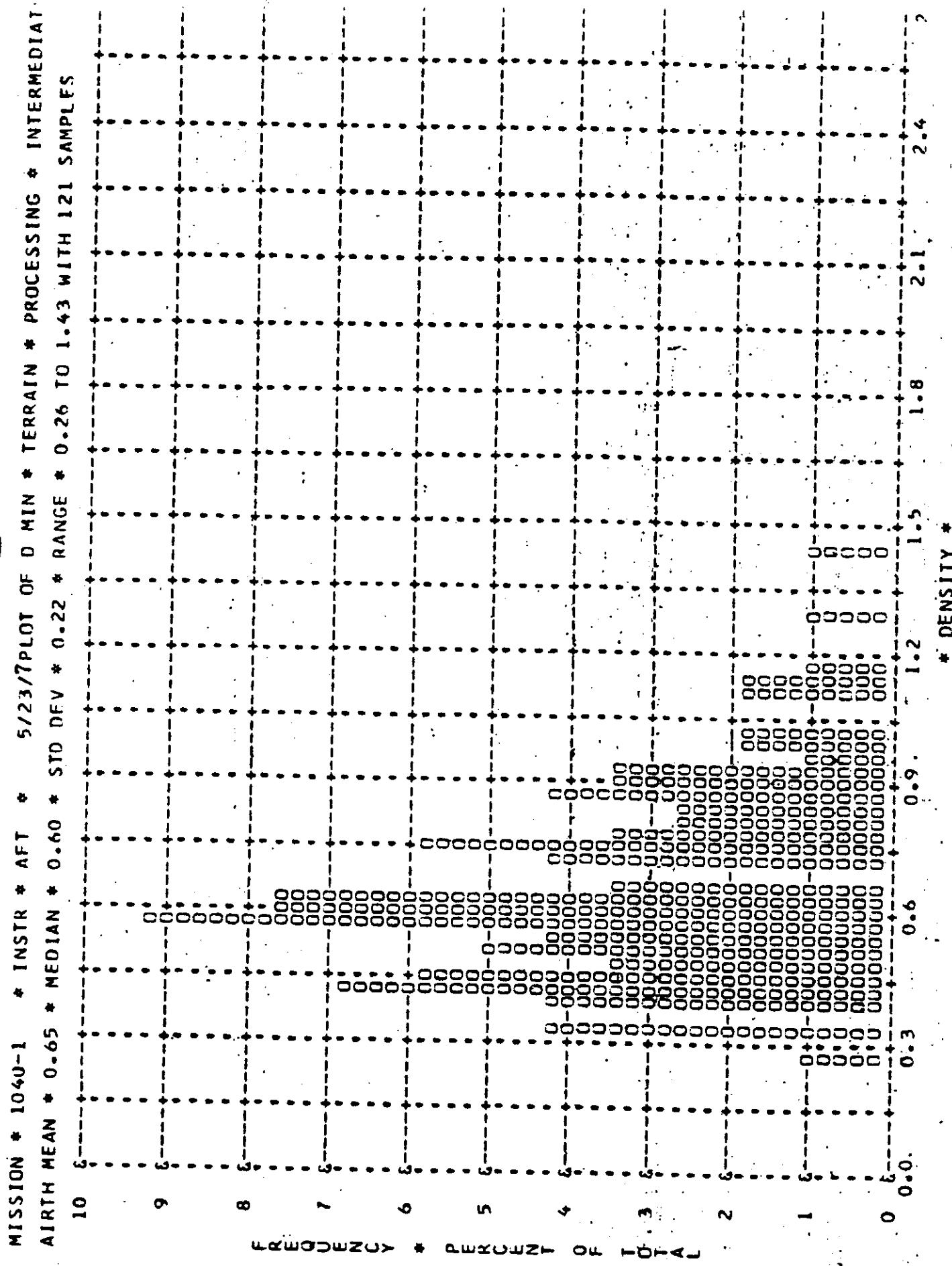
FIGURE A-1h

TOP SECRET C

TOP SECRET C



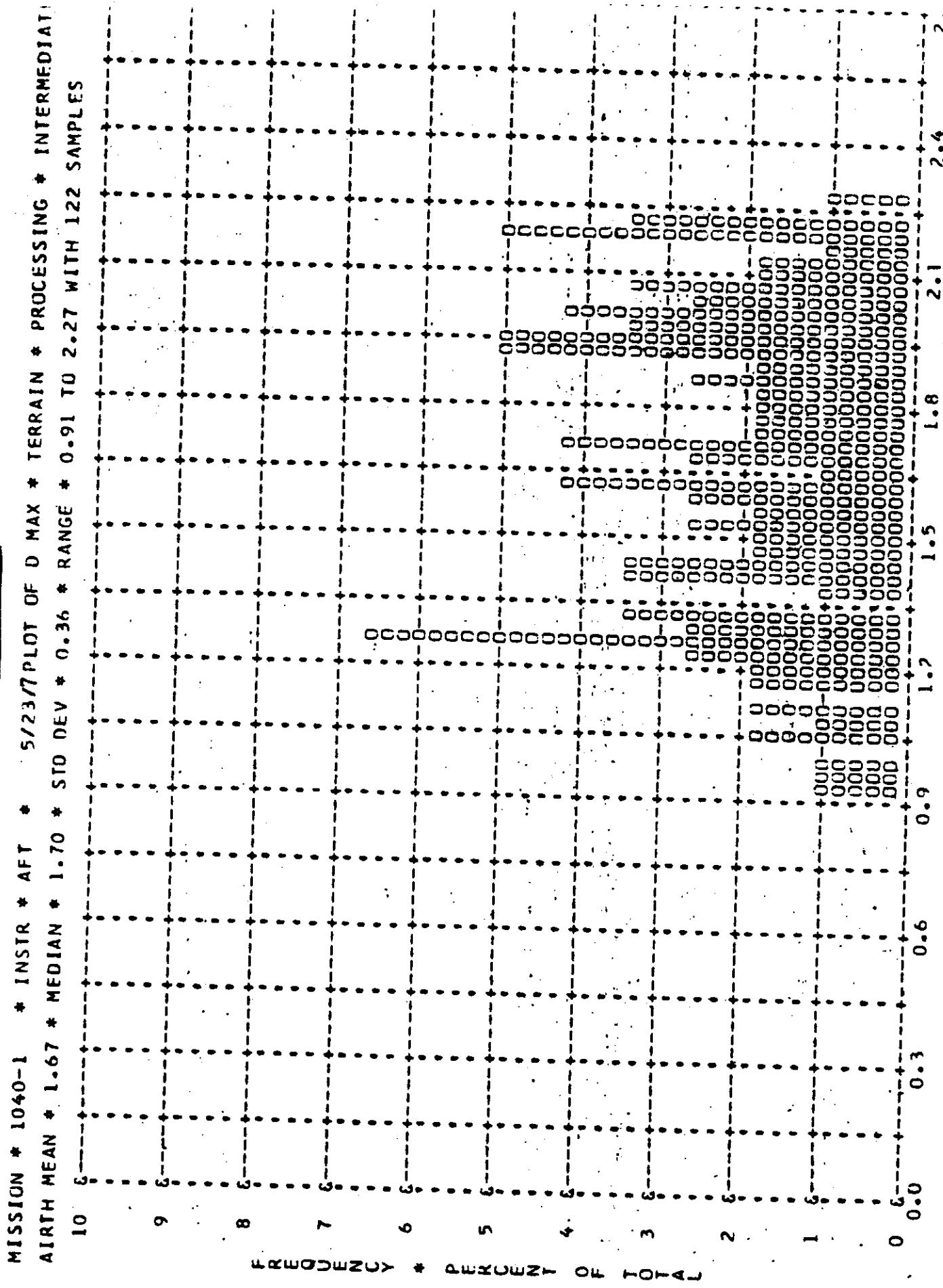
TOP SECRET C



TOP SECRET C

FIGURE A-16

TOP SECRET C

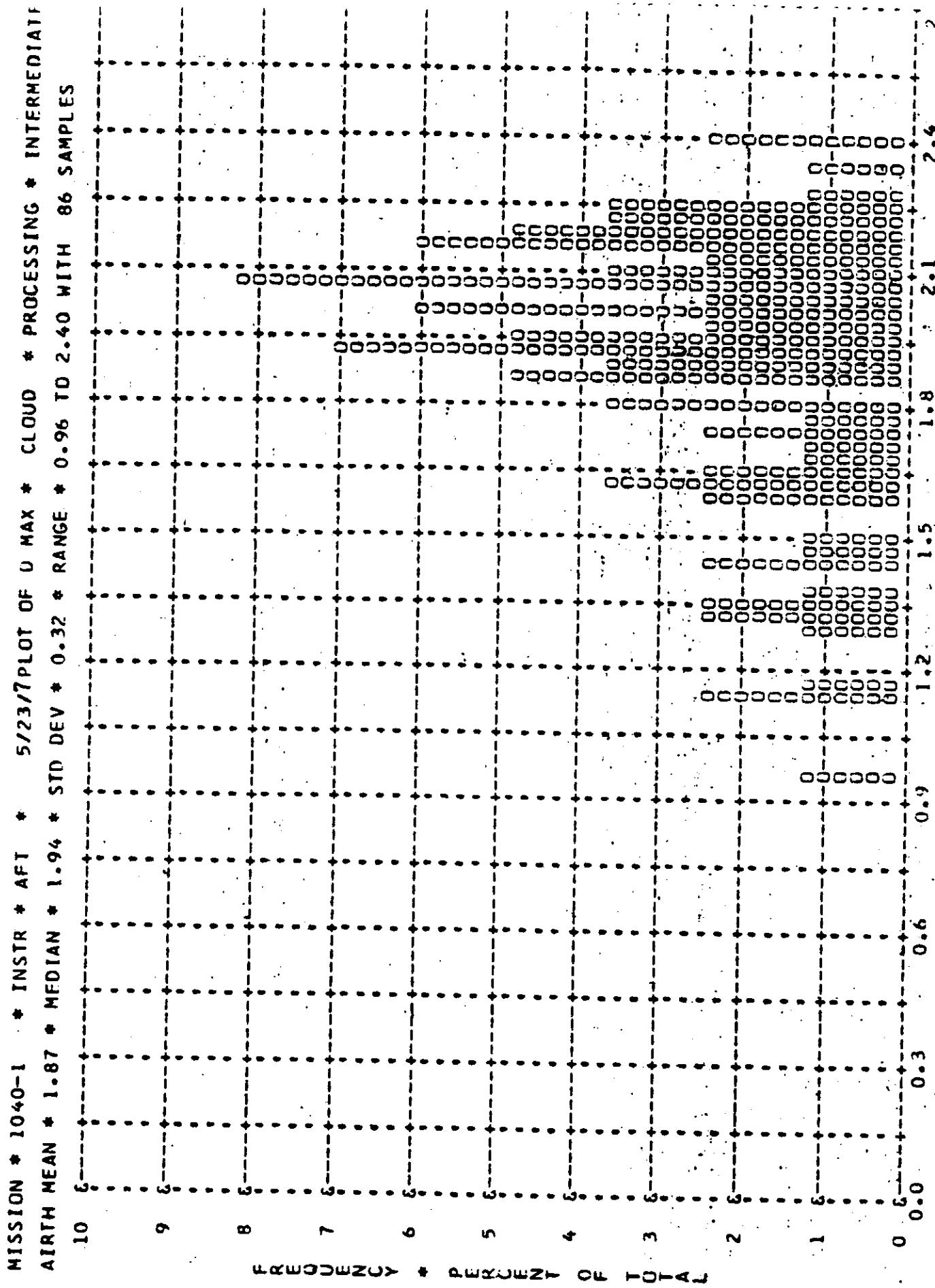


TOP SECRET C

TOP SECRET C

TOP SECRET C

TOP SECRET C



PTCPIE A-18

MISSION * 1040-1 * INSTR * AFT * 5/23/7 PLOT OF 0 MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.67 * MEDIAN * 0.61 * STD DEV * 0.24 * RANGE * 0.36 TO 1.62 WITH 103 SAMPLES

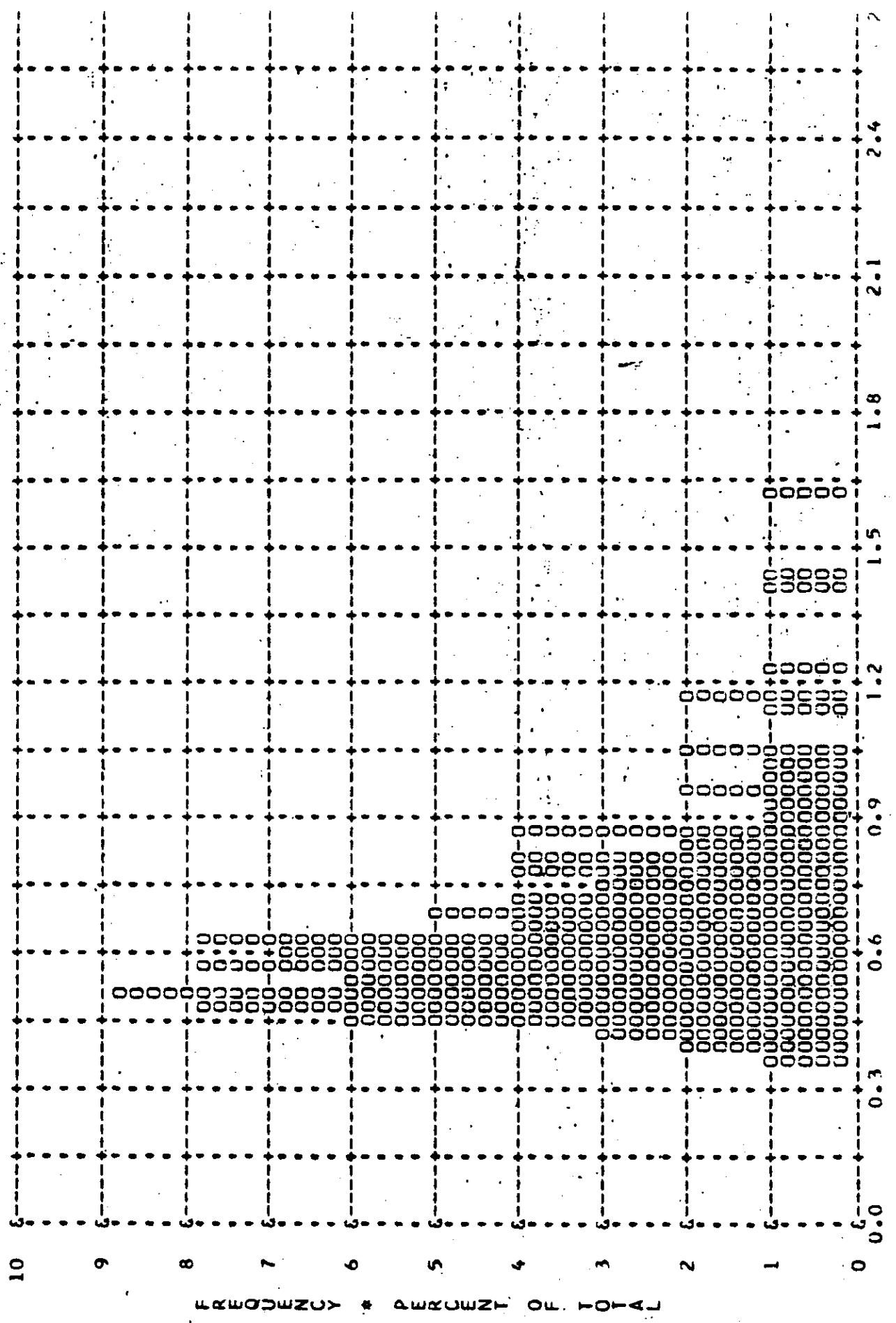


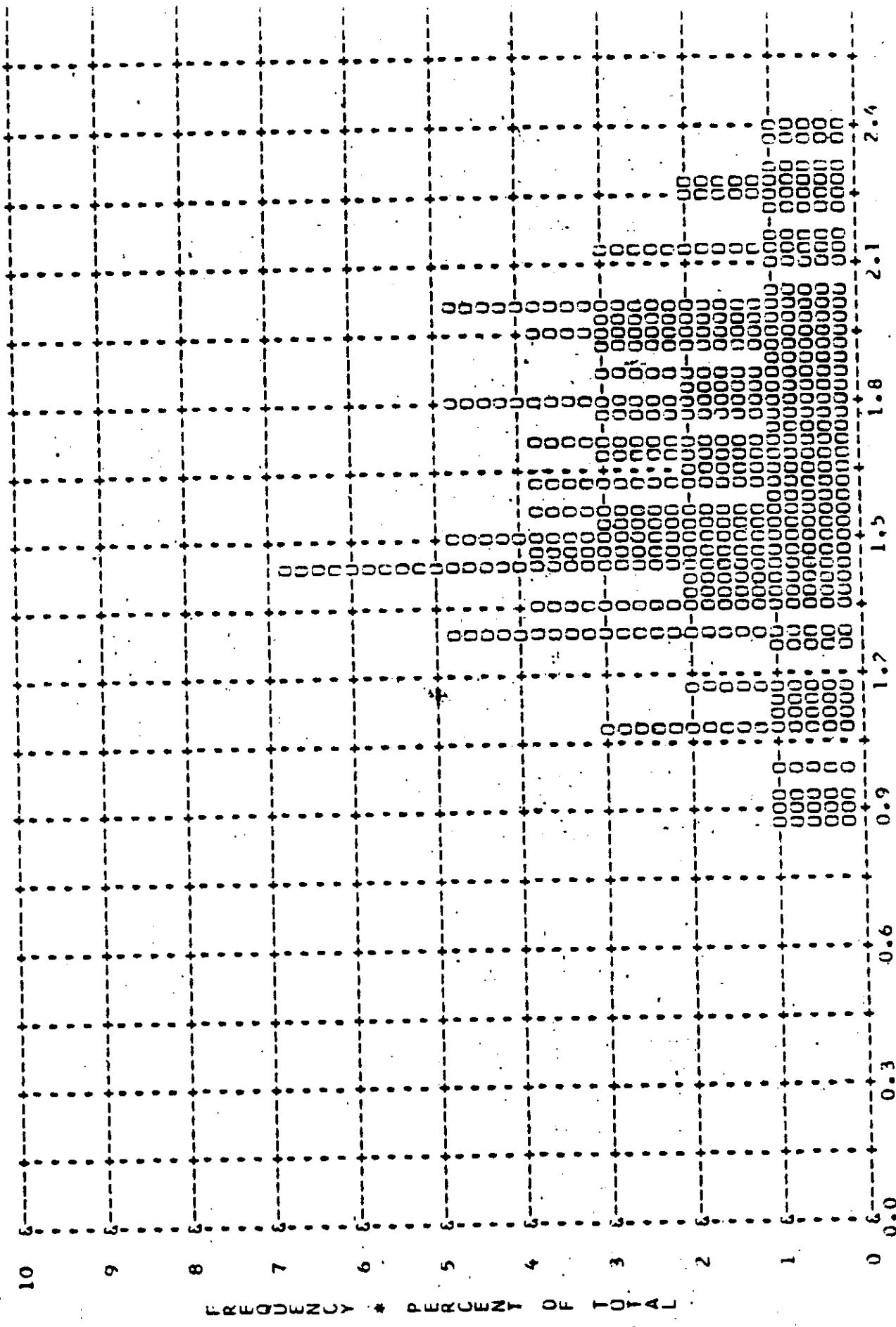
FIGURE A-10

TOP SECRET C

TOP SECRET C

HQ-SECRET C

MISSION * 1040-1 * INSTR * AFT * 5/23/7 PLOT OF D MAX * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 1.65 * MEDIAN * 1.63 * STD. DEV * 0.35 * RANGE * 0.85 TO 2.38 WITH 106 SAMPLES



* DENSITY *

PINNACLE A-10

HQ-SECRET C

TOP SECRET C

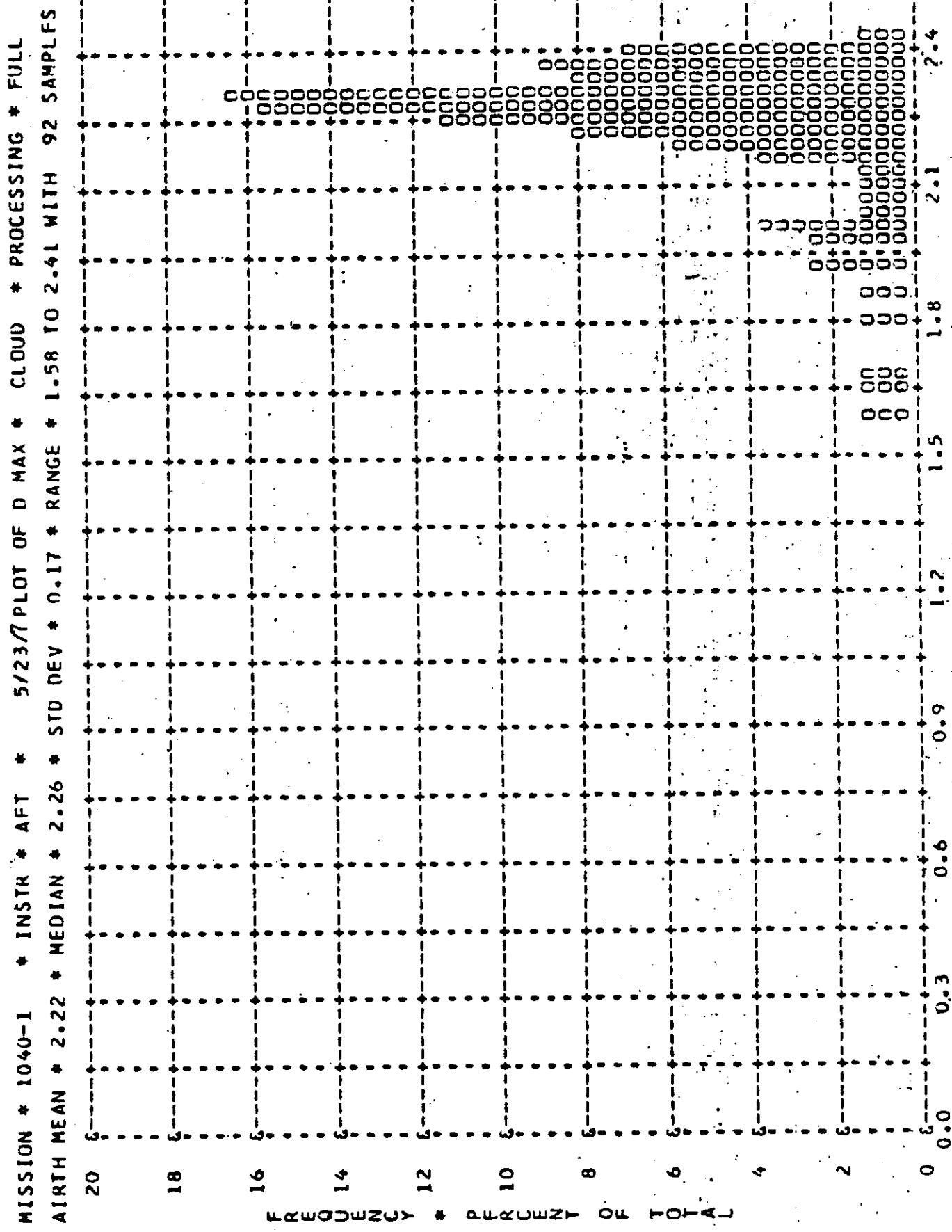


FIGURE A-21

TOP SECRET C

HOP-SEGMENT C

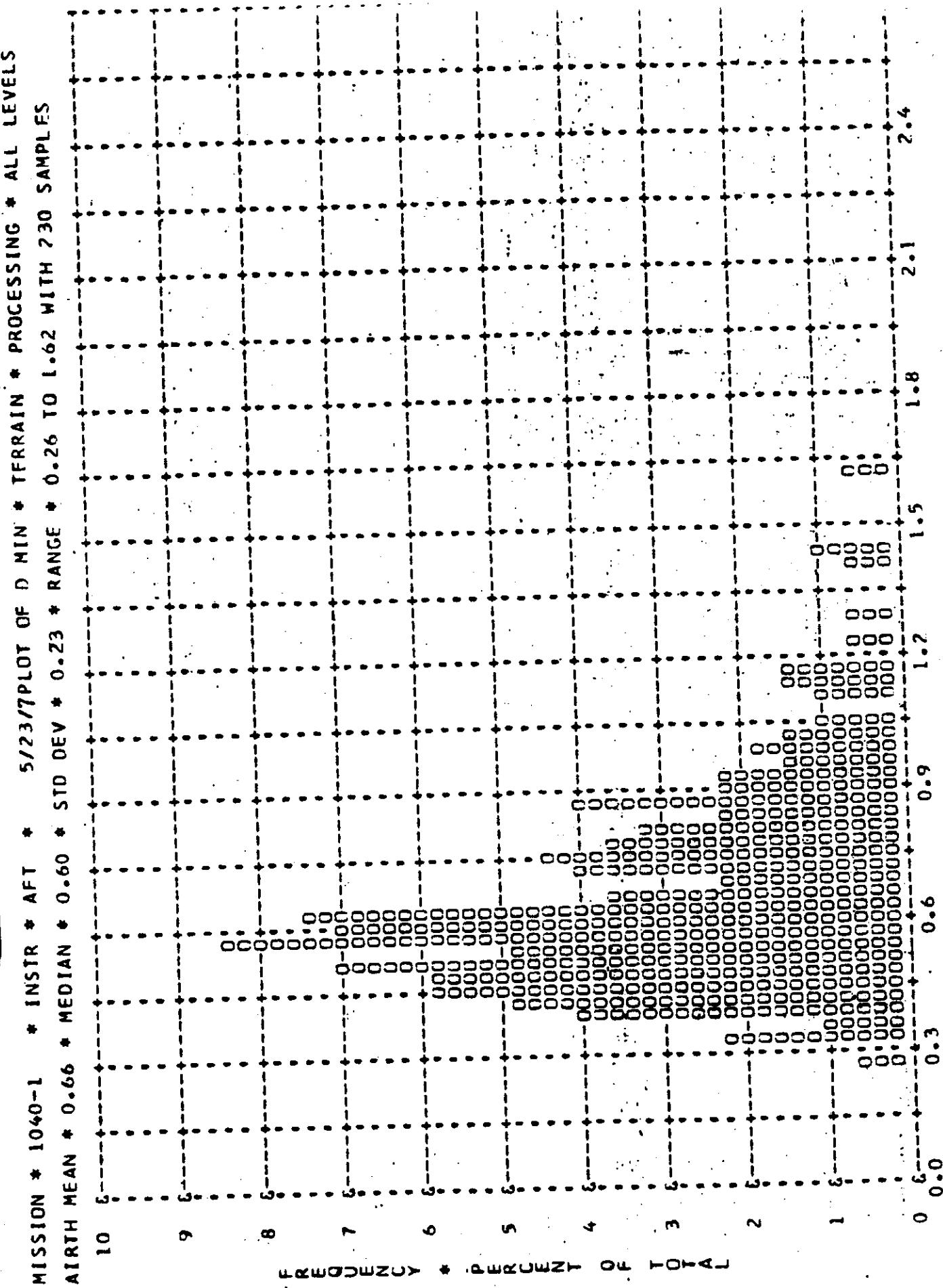


FIGURE A-7

TOP SECRET C

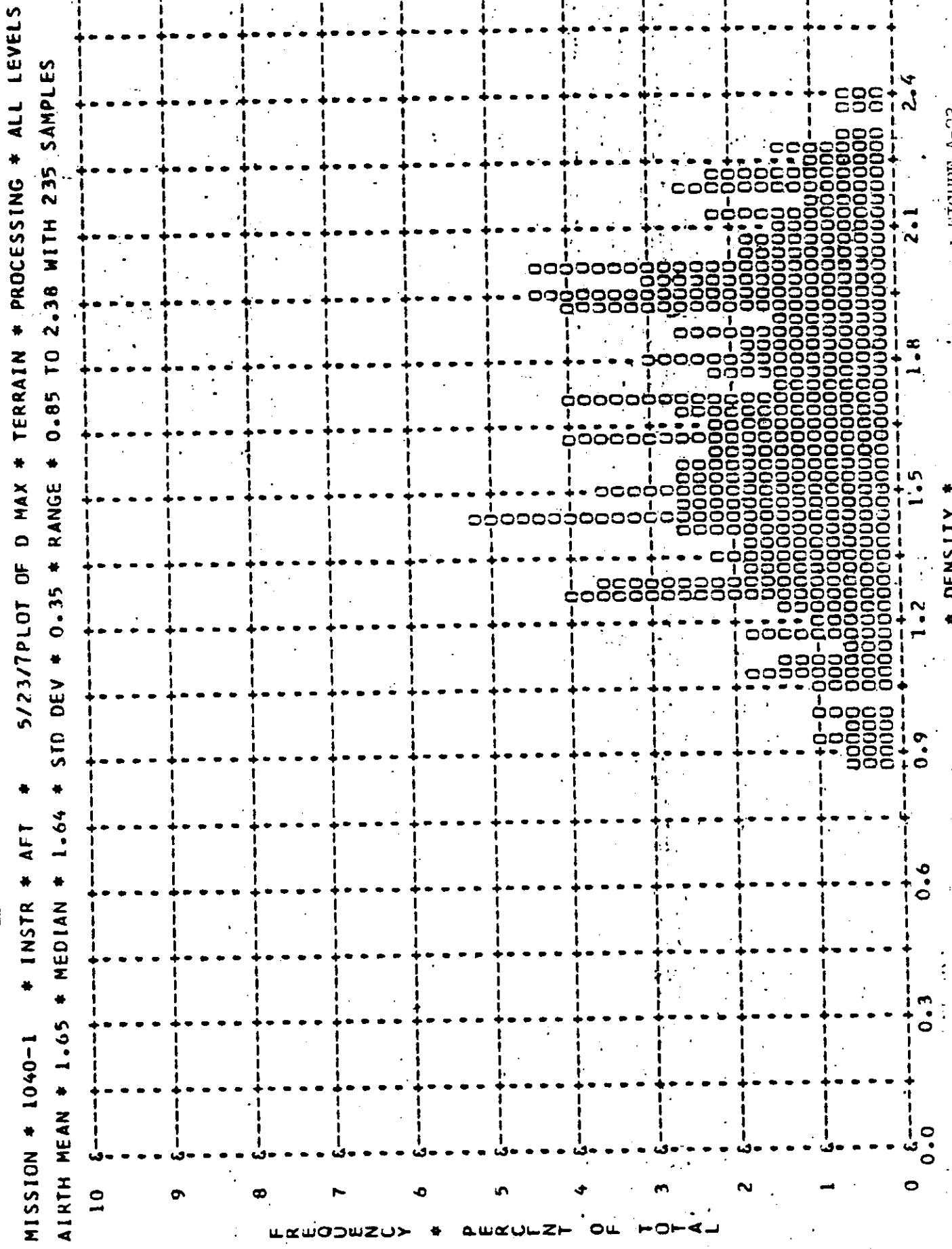
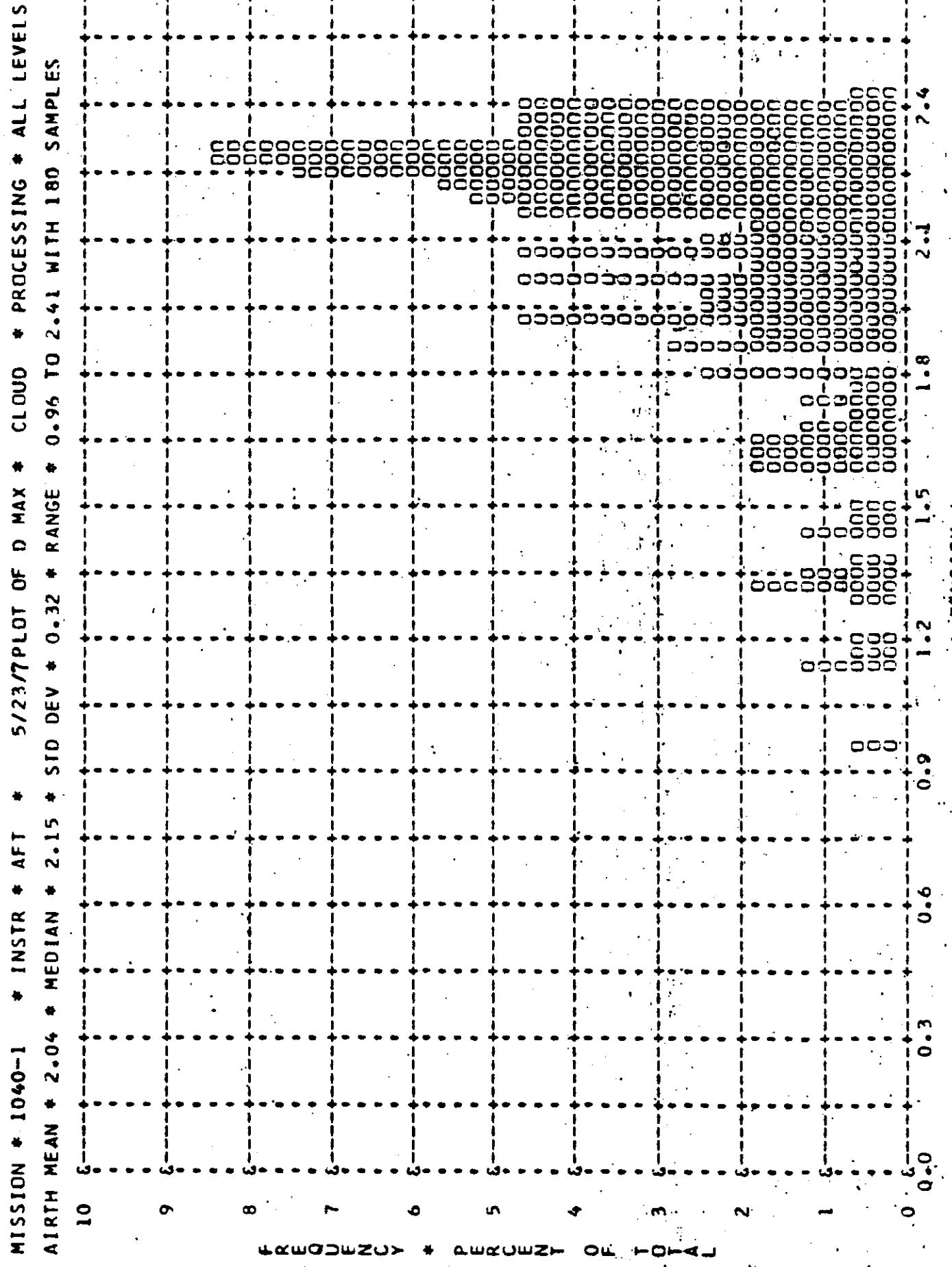


FIGURE A-23

TOP SECRET C

TOP SECRET C



TOP SECRET C

FIGURE A-7h

* DENSITY *

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * FWD * 5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
0.01	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0
SUBTOTAL	3	0	0	0	0	0	0	0

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.51	0 0	0	1	0 0
0.52	0 0	0	1	2 2
0.53	0 0	0	3	4 1
0.54	0 0	0	1	6
0.55	0 0	0	4	0 5
0.56	0 0	0	5	5 5
0.57	0 0	0	5	6 6
0.58	0 0	0	4	5 5
0.59	0 0	0	3	6 6
0.60	0 0	0	4	5 5
0.61	0 0	0	3	4 4
0.62	0 0	0	3	3 3
0.63	0 0	0	4	6 6
0.64	0 0	0	3	5 5
0.65	0 0	0	3	6 6
0.66	0 0	0	4	5 5
0.67	0 0	0	3	4 4
0.68	0 0	0	4	4 4
0.69	0 0	0	4	1 2
0.70	0 0	0	2	6 6
0.71	0 0	0	4	4 4
0.72	0 0	0	3	1 2
0.73	0 0	0	3	3 3
0.74	0 0	0	1	2 2
0.75	0 0	0	0	3 3
0.76	0 0	0	0	1 1
0.77	0 0	0	0	0 0
0.78	0 0	0	0	0 0
0.79	0 0	0	0	0 0
0.80	0 0	0	0	0 0
0.81	0 0	0	0	0 0
0.82	0 0	0	0	0 0
0.83	0 0	0	0	0 0
0.84	0 0	0	0	0 0
0.85	0 0	0	0	0 0
0.86	0 0	0	0	0 0
0.87	0 0	0	0	0 0
0.88	0 0	0	0	0 0
0.89	0 0	0	0	0 0
0.90	0 0	0	0	0 0
0.91	0 0	0	0	0 0
0.92	0 0	0	0	0 0
0.93	0 0	0	0	0 0
0.94	0 0	0	0	0 0
0.95	0 0	0	0	0 0
0.96	0 0	0	0	0 0
0.97	0 0	0	0	0 0
0.98	0 0	0	0	0 0
0.99	0 0	0	0	0 0
1.00	0 0	0	0	0 0
SUBTOTAL	3	57	124	184

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * FWD 5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01	0	0	2	2
1.02	0	0	1	1
1.03	0	0	1	1
1.04	0	0	1	1
1.05	0	0	1	1
1.06	0	0	2	2
1.07	0	0	1	1
1.08	0	0	1	1
1.09	0	0	1	1
1.10	0	0	1	1
1.11	0	0	1	1
1.12	0	0	1	1
1.13	0	0	1	1
1.14	0	0	1	1
1.15	0	0	1	1
1.16	0	0	1	1
1.17	0	0	1	1
1.18	0	0	1	1
1.19	0	0	1	1
1.20	0	0	1	1
1.21	0	0	1	1
1.22	0	0	1	1
1.23	0	0	1	1
1.24	0	0	1	1
1.25	0	0	1	1
1.26	0	0	1	1
1.27	0	0	1	1
1.28	0	0	1	1
1.29	0	0	1	1
1.30	0	0	1	1
1.31	0	0	1	1
1.32	0	0	1	1
1.33	0	0	1	1
1.34	0	0	1	1
1.35	0	0	1	1
1.36	0	0	1	1
1.37	0	0	1	1
1.38	0	0	1	1
1.39	0	0	1	1
1.40	0	0	1	1
1.41	0	0	1	1
1.42	0	0	1	1
1.43	0	0	1	1
1.44	0	0	1	1
1.45	0	0	1	1
1.46	0	0	1	1
1.47	0	0	1	1
1.48	0	0	1	1
1.49	0	0	1	1
1.50	0	0	1	1
SUBTOTAL	0	5	11	37
			30	47
			3	3
			41	89

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION # 1040-2 * INSTRUMENT # FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM		INTERMEDIATE MIN MAX LIM		FULL MIN MAX LIM		ALL LEVELS MIN MAX LIM	
1.51	0	0	0	0	0	0	0	2
1.52	0	0	0	0	0	0	0	3
1.53	0	0	0	0	0	0	0	3
1.54	0	0	0	0	0	0	0	1
1.55	0	0	0	0	0	0	0	5
1.56	0	0	0	0	0	0	0	3
1.57	0	0	0	0	0	0	0	2
1.58	0	0	0	0	0	0	0	5
1.59	0	0	0	0	0	0	0	7
1.60	0	0	0	0	0	0	0	3
1.61	0	0	0	0	0	0	0	2
1.62	0	0	0	0	0	0	0	7
1.63	0	0	0	0	0	0	0	5
1.64	0	0	0	0	0	0	0	2
1.65	0	0	0	0	0	0	0	2
1.66	0	0	0	0	0	0	0	1
1.67	0	0	0	0	0	0	0	1
1.68	0	0	0	0	0	0	0	1
1.69	0	0	0	0	0	0	0	1
1.70	0	0	0	0	0	0	0	1
1.71	0	0	0	0	0	0	0	1
1.72	0	0	0	0	0	0	0	1
1.73	0	0	0	0	0	0	0	1
1.74	0	0	0	0	0	0	0	1
1.75	0	0	0	0	0	0	0	1
1.76	0	0	0	0	0	0	0	1
1.77	0	0	0	0	0	0	0	1
1.78	0	0	0	0	0	0	0	1
1.79	0	0	0	0	0	0	0	1
1.80	0	0	0	0	0	0	0	1
1.81	0	0	0	0	0	0	0	1
1.82	0	0	0	0	0	0	0	1
1.83	0	0	0	0	0	0	0	1
1.84	0	0	0	0	0	0	0	1
1.85	0	0	0	0	0	0	0	1
1.86	0	0	0	0	0	0	0	1
1.87	0	0	0	0	0	0	0	1
1.88	0	0	0	0	0	0	0	1
1.89	0	0	0	0	0	0	0	1
1.90	0	0	0	0	0	0	0	1
1.91	0	0	0	0	0	0	0	1
1.92	0	0	0	0	0	0	0	1
1.93	0	0	0	0	0	0	0	1
1.94	0	0	0	0	0	0	0	1
1.95	0	0	0	0	0	0	0	1
1.96	0	0	0	0	0	0	0	1
1.97	0	0	0	0	0	0	0	1
1.98	0	0	0	0	0	0	0	1
1.99	0	0	0	0	0	0	0	1
2.00	0	0	0	0	0	0	0	1
SUBTOTAL	0	0	1	5	0	32	3	97
							3	132
								75

~~TOP SECRET C~~

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0 0	0 0	0 0	0 0
2.02	0 0	0 0	0 0	0 0
2.03	0 0	0 0	0 0	0 0
2.04	0 0	0 0	0 0	0 0
2.05	0 0	0 0	0 0	0 0
2.06	0 0	0 0	0 0	0 0
2.07	0 0	0 0	0 0	0 0
2.08	0 0	0 0	0 0	0 0
2.09	0 0	0 0	0 0	0 0
2.10	0 0	0 0	0 0	0 0
2.11	0 0	0 0	0 0	0 0
2.12	0 0	0 0	0 0	0 0
2.13	0 0	0 0	0 0	0 0
2.14	0 0	0 0	0 0	0 0
2.15	0 0	0 0	0 0	0 0
2.16	0 0	0 0	0 0	0 0
2.17	0 0	0 0	0 0	0 0
2.18	0 0	0 0	0 0	0 0
2.19	0 0	0 0	0 0	0 0
2.20	0 0	0 0	0 0	0 0
2.21	0 0	0 0	0 0	0 0
2.22	0 0	0 0	0 0	0 0
2.23	0 0	0 0	0 0	0 0
2.24	0 0	0 0	0 0	0 0
2.25	0 0	0 0	0 0	0 0
2.26	0 0	0 0	0 0	0 0
2.27	0 0	0 0	0 0	0 0
2.28	0 0	0 0	0 0	0 0
2.29	0 0	0 0	0 0	0 0
2.30	0 0	0 0	0 0	0 0
2.31	0 0	0 0	0 0	0 0
2.32	0 0	0 0	0 0	0 0
2.33	0 0	0 0	0 0	0 0
2.34	0 0	0 0	0 0	0 0
2.35	0 0	0 0	0 0	0 0
2.36	0 0	0 0	0 0	0 0
2.37	0 0	0 0	0 0	0 0
2.38	0 0	0 0	0 0	0 0
2.39	0 0	0 0	0 0	0 0
2.40	0 0	0 0	0 0	0 0
2.41	0 0	0 0	0 0	0 0
2.42	0 0	0 0	0 0	0 0
2.43	0 0	0 0	0 0	0 0
2.44	0 0	0 0	0 0	0 0
2.45	0 0	0 0	0 0	0 0
2.46	0 0	0 0	0 0	0 0
2.47	0 0	0 0	0 0	0 0
2.48	0 0	0 0	0 0	0 0
2.49	0 0	0 0	0 0	0 0
2.50	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	5 21	26 98
				31 119

~~TOP SECRET C~~

~~TOP SECRET C~~

MISSION # 1040-2 * INSTRUMENT # FWD

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL' LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	1	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	1	0	0	1	0
SUBTOTAL	0	0	0	0	0	0	0	1	0	0	1	0
TOTAL	6	6	6	76	76	57	176	176	139	258	258	202

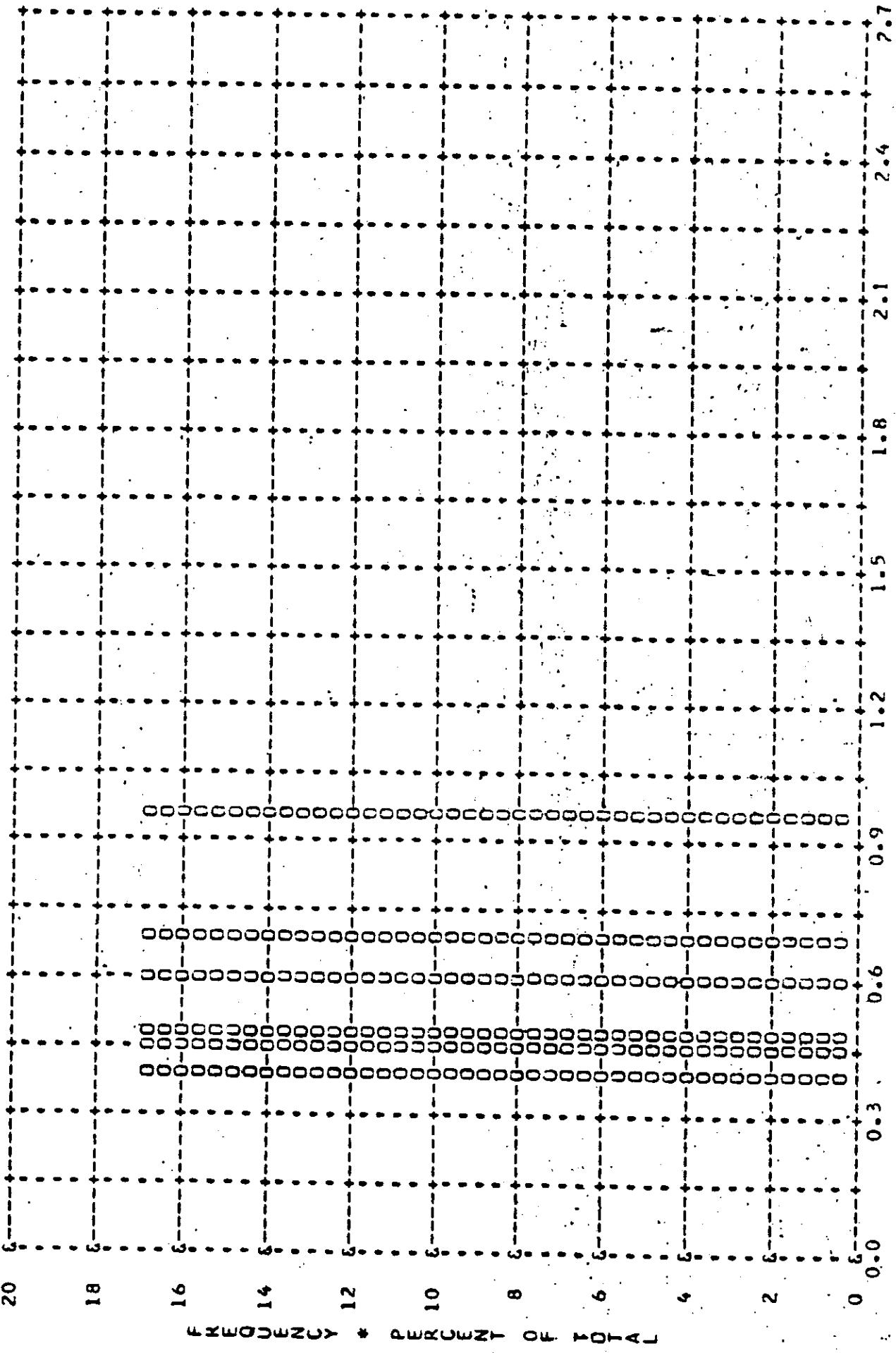
MISSION 1040-2		INSTR - FWD		5/23/		PROCESSING AND EXPOSURE ANALYSI					
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED
PRIMARY	6	0 PC	17 PC	67 PC	0 PC	17 PC					
INTERMEDIATE	76	0 PC	1 PC	71 PC	25 PC	3 PC					
FULL	176	2 PC	0 PC	73 PC	26 PC	0 PC					
ALL LEVELS	258	1 PC	1 PC	72 PC	25 PC	1 PC					
PROCESS LEVEL	BASE & FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----	0.91 AND UP				
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP					
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP					

~~TOP SECRET C~~

TABLE A-3

MISS. N * 1040-2 * INSTR * FWD * 5/23/7 PLNU OF D MIN * TERRAIN * PROCESSING * PRIMARY

AIRTH MEAN * 0.59 * MEDIAN * 0.60 * STD DEV * 0.22 * RANGE * 0.37 TO 0.96 WITH 6 SAMPLES



* DENSITY *

FIGURE A-25

TOP SECRET C

MISSION # 1040-2 * INSTR # FWD * 5/23/77 PLOT OF D MAX * TERRAIN * PROCESSING * PRIMARY

AIRTH MEAN # 1.22 * MEDIAN # 1.19 * STD DEV # 0.22 * RANGE # 1.04 TO 1.62 WITH 6 SAMPLES

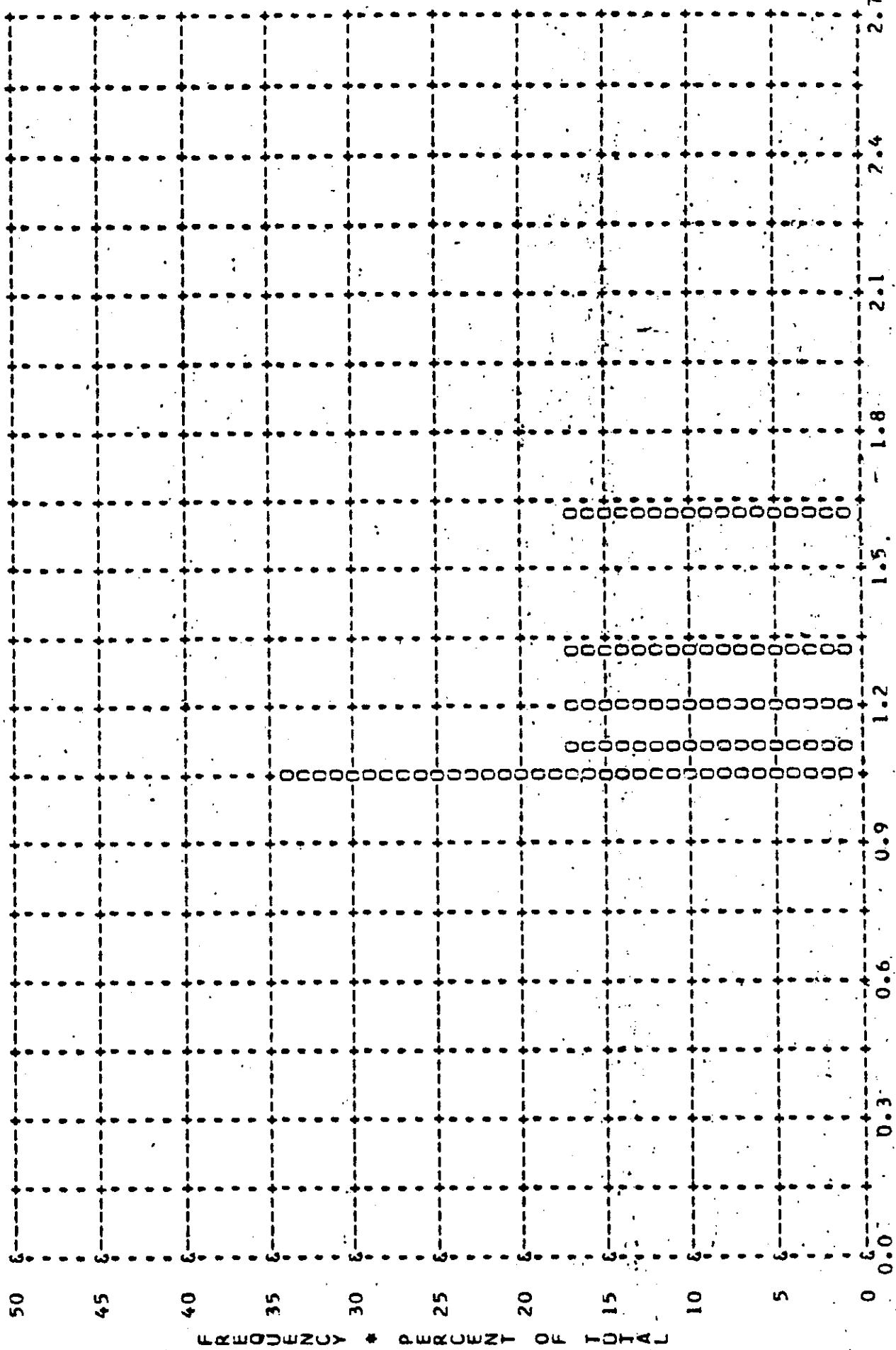


FIGURE A-26

TOP SECRET

TOP SECRET C

MISSION * 1040-2 * INSTR * FWD * 5/23/7 PLOT OF D MAX * CLOUD * PROCESSING * PRIMARY

AIRTH MEAN * 1.69 * MEDIAN * 1.77 * STD DEV * 0.19 * RANGE * 1.35 TO 1.89 WITH 6 SAMPLES

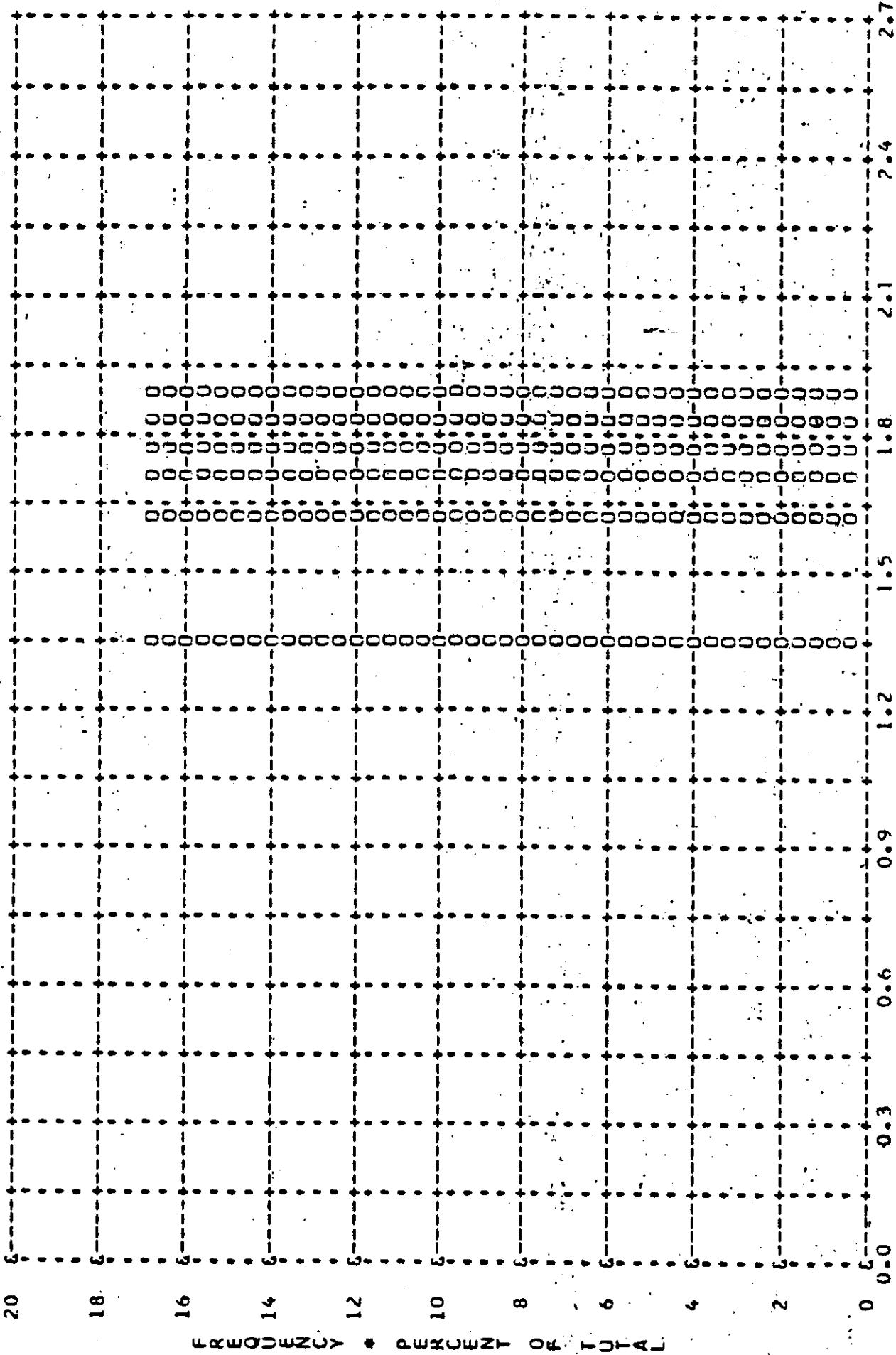


FIGURE A-27

TOP SECRET C

TUP SECRET C

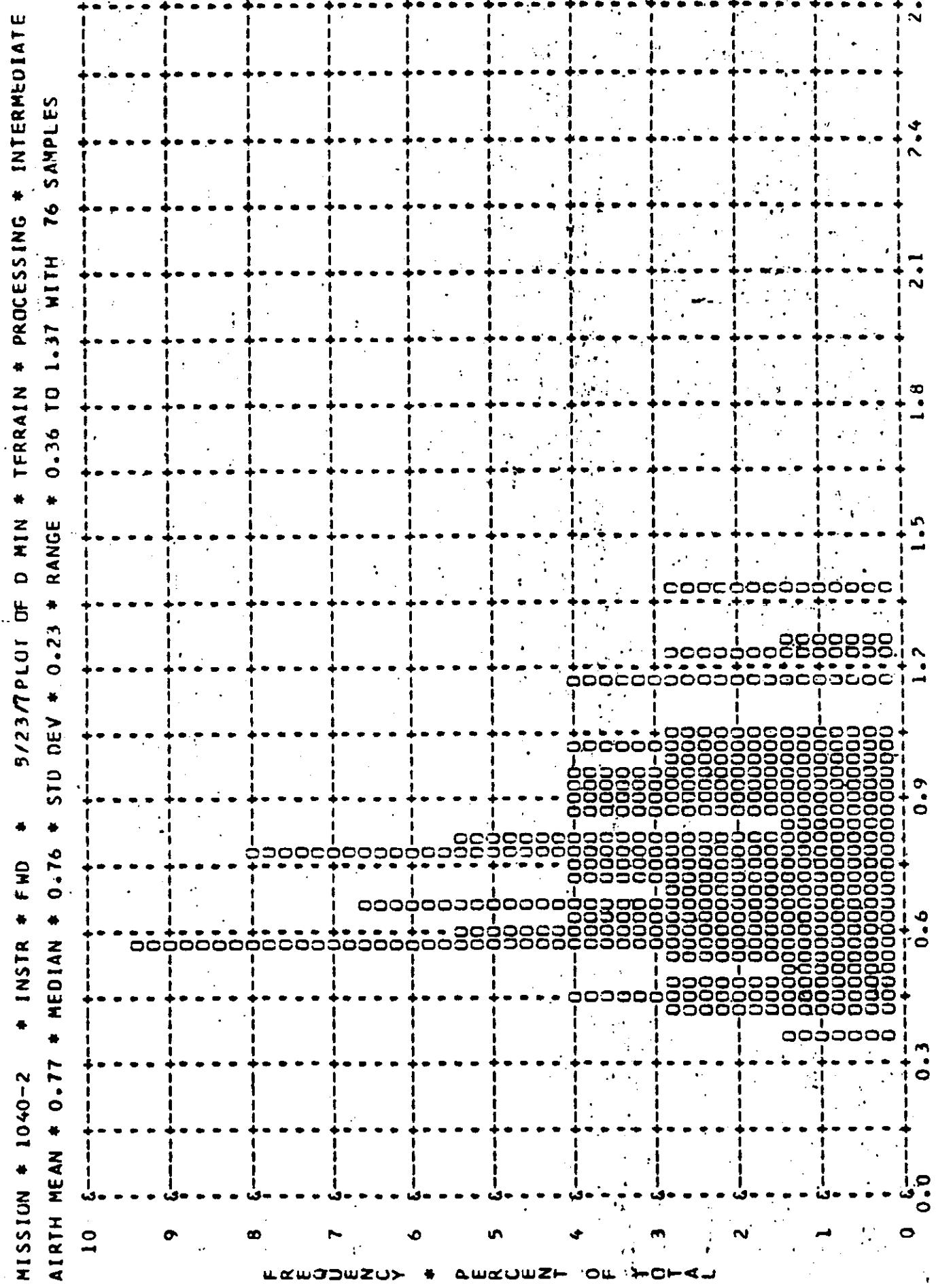


FIGURE A-28

TUP SECRET C

TOP SECRET C

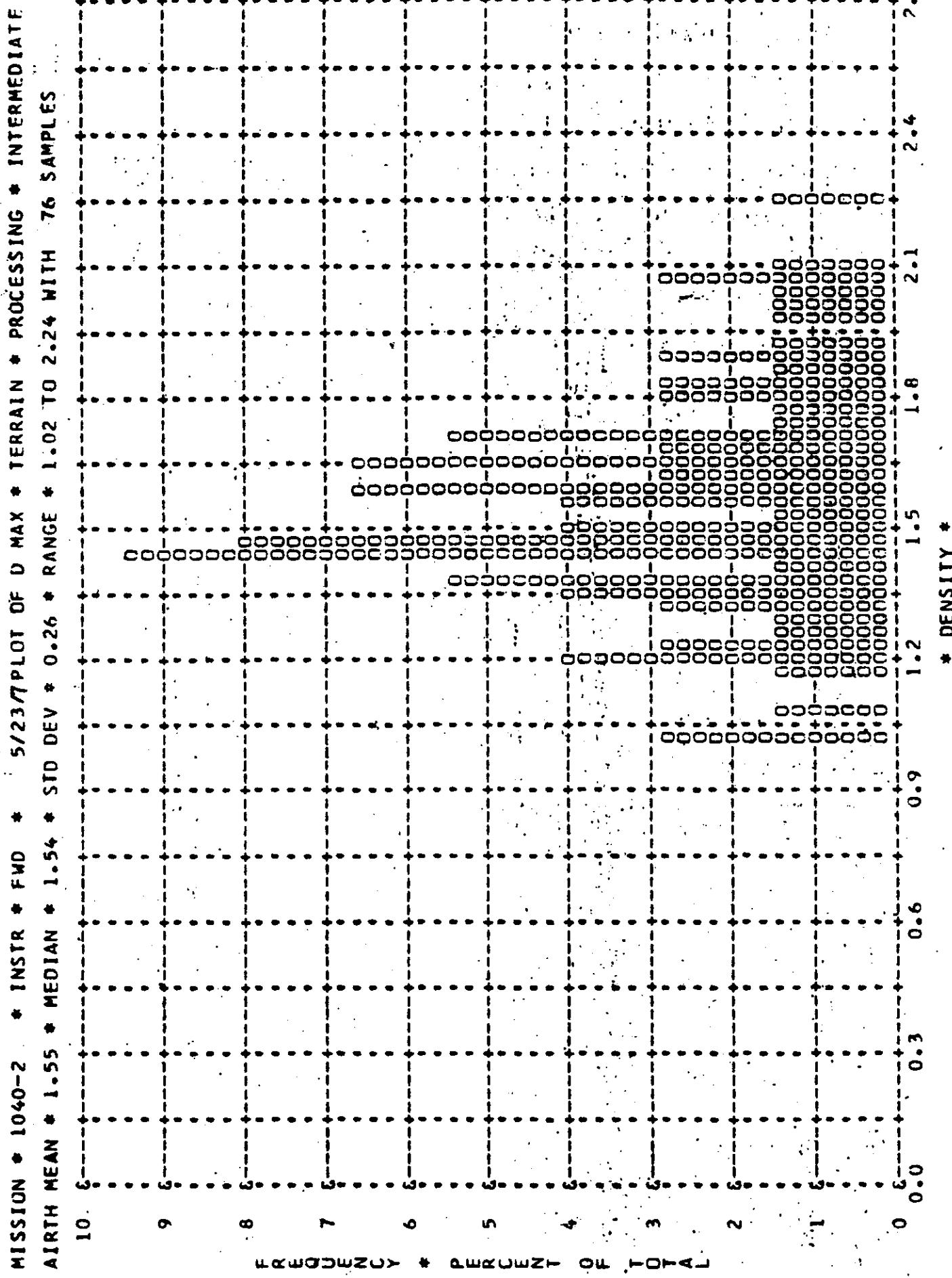


FIGURE A-29

TOP SECRET C

TOP SECRET C

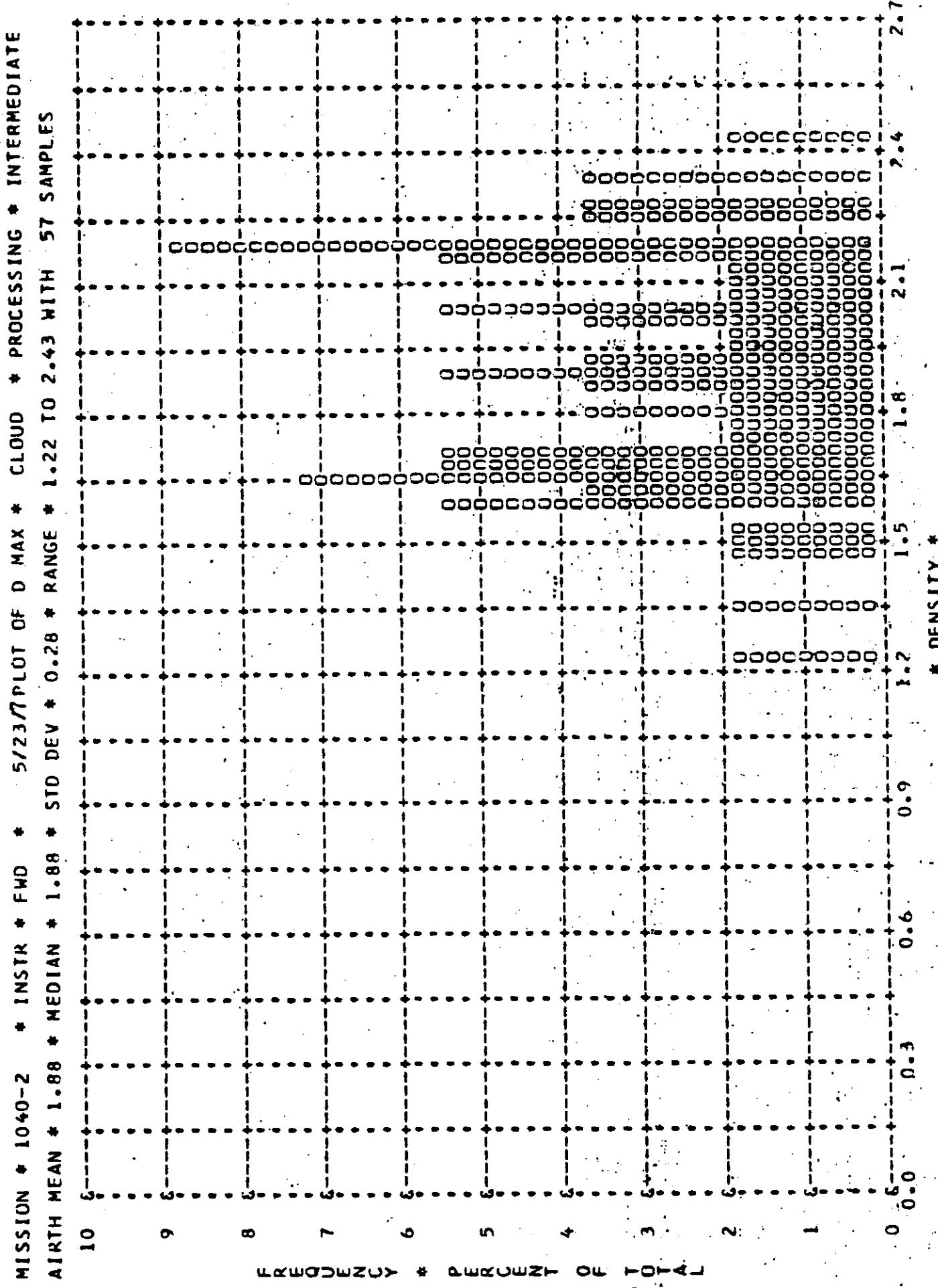
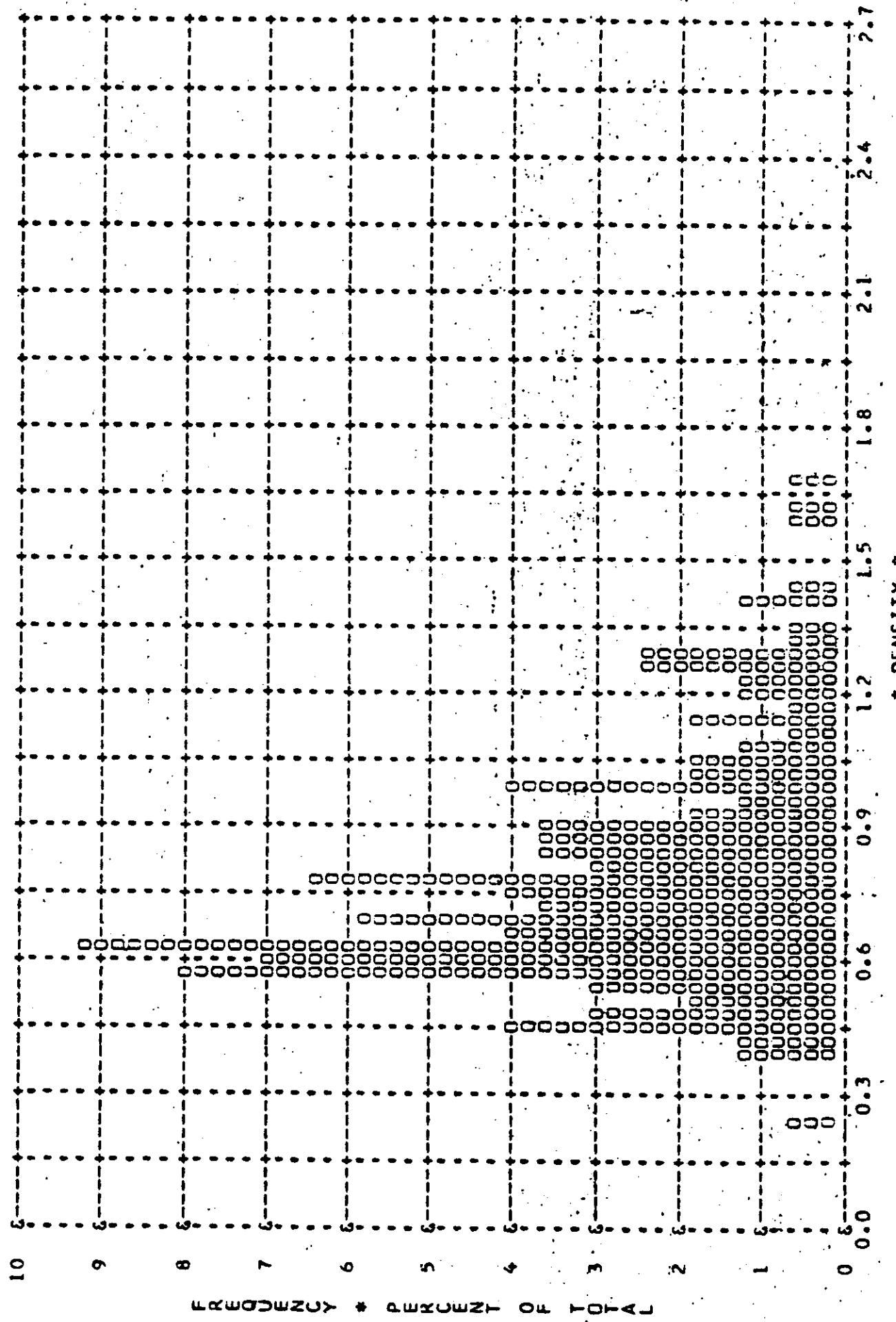


FIGURE A-30

TOP SECRET C

MISSION * 1040-2 * INSTR * FWD * 5/23/7 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.78 * MEDIAN * 0.72 * STD DEV * 0.27 * RANGE * 0.24 TO 1.67 WITH 176 SAMPLES



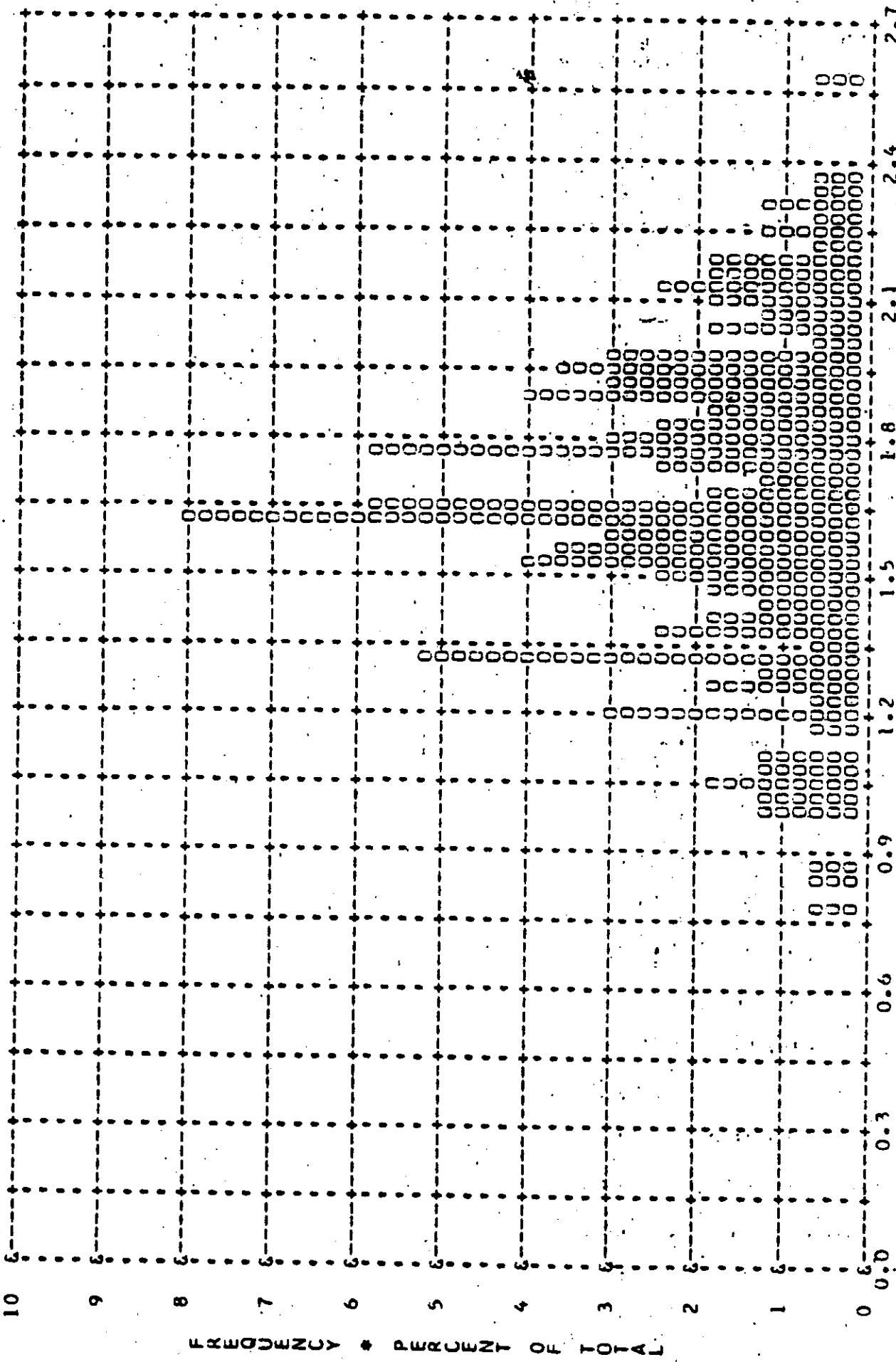
* DENSITY *

FIGURE A-31

TOP SECRET C

~~TOP SECRET C~~

MISSION * 1040-2 * INSTR * FWD * 5/23/7 PLAT OF D MAX * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 1.65 * MEDIAN * 1.63 * STD DEV * 0.34 * RANGE * 0.77 TO 2.58 WITH 176 SAMPLES



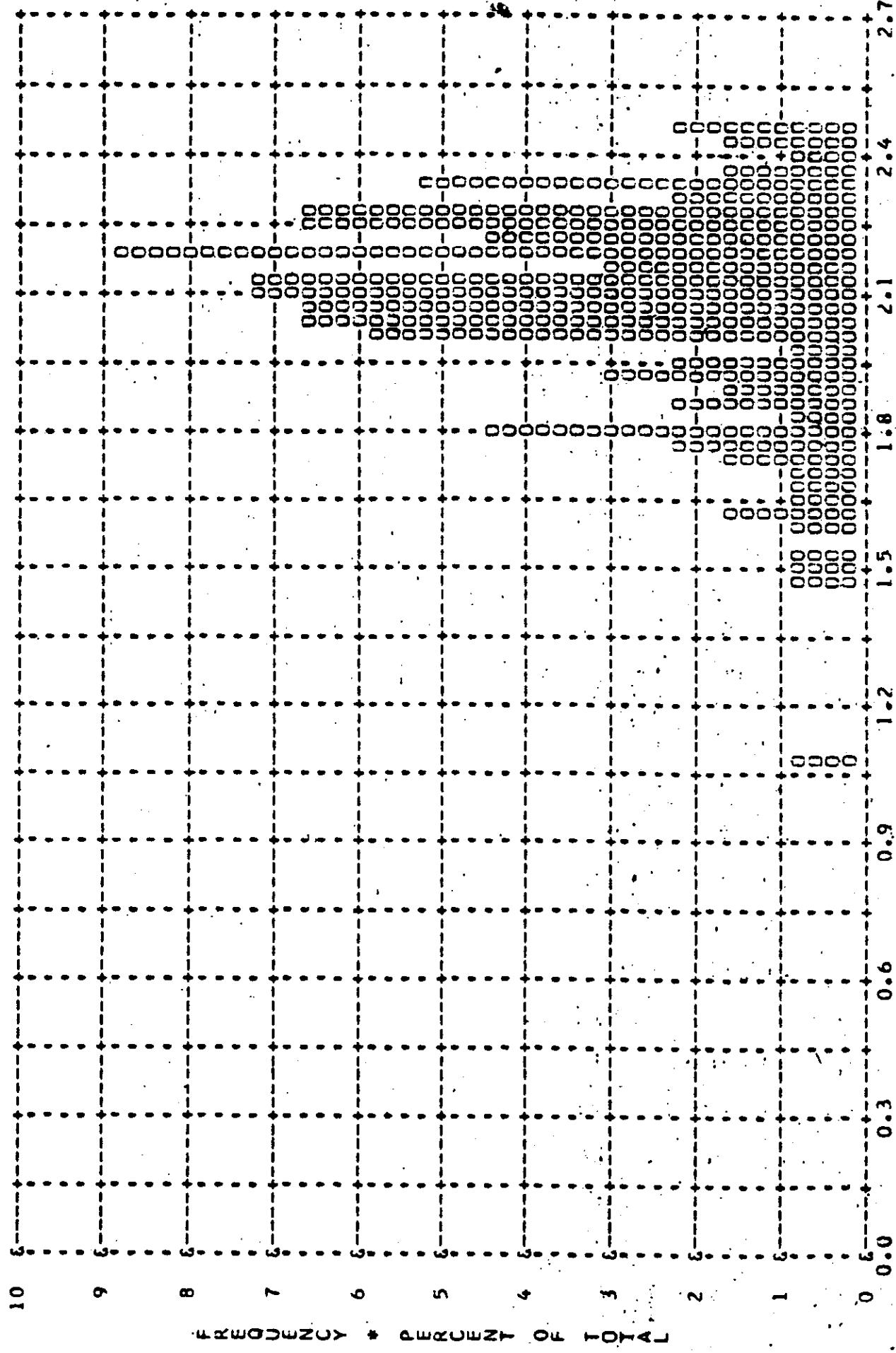
* DENSITY *

~~TOP SECRET C~~

FIGURE A-32

TOP SECRET-C

MISSION * 1040-2 * INSTR * FWD * 5/23/77 PLOT OF D MAX * CLOUD * PROCESSING * FULL
AIRTH MEAN * 2.07 * MEDIAN * 2.10 * STD DEV * 0.23 * RANGE * 1.08 TO 2.45 WITH 139 SAMPLES



TOP SECRET-C

FIGURE A-33

TOP SECRET C

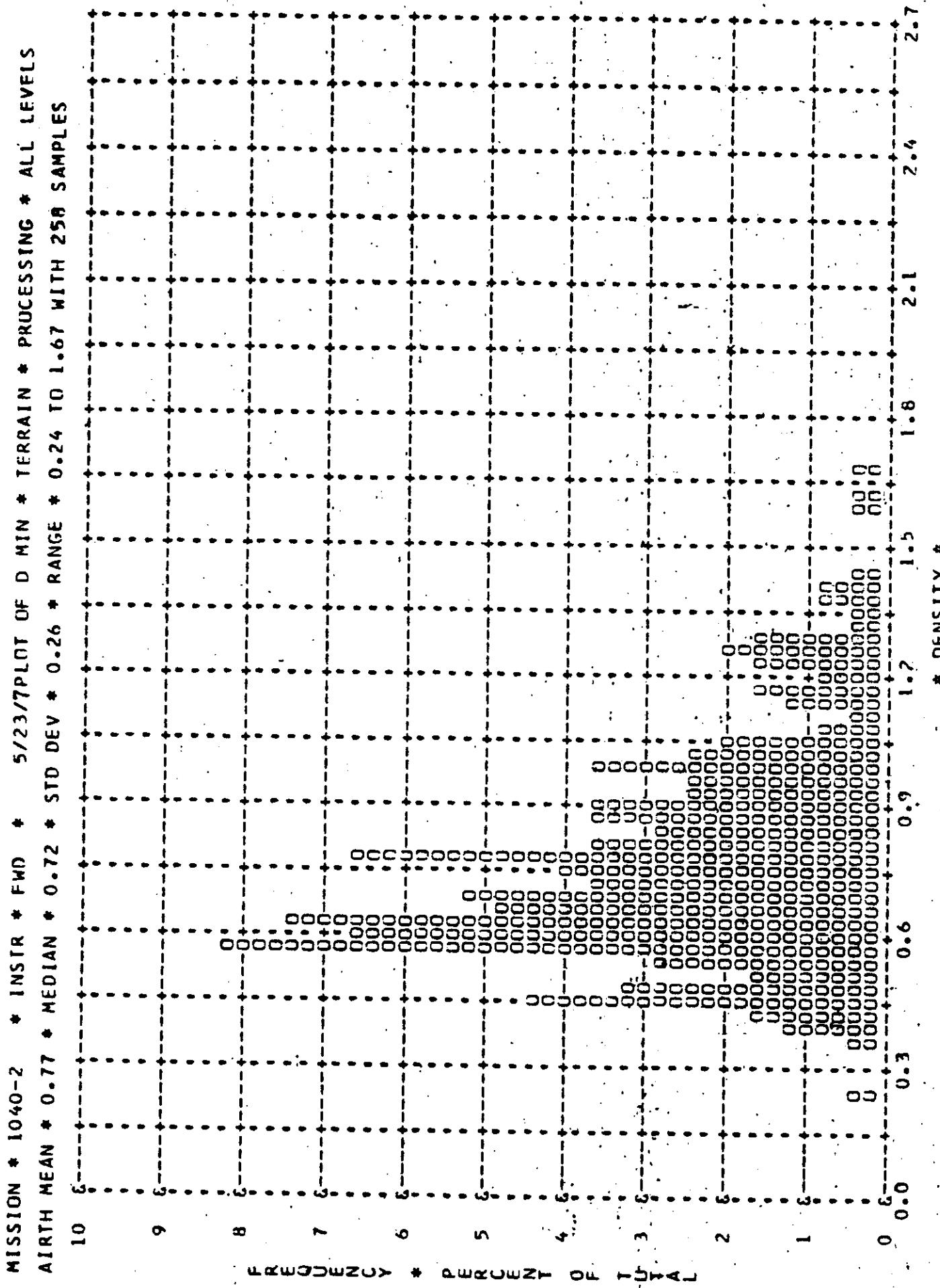
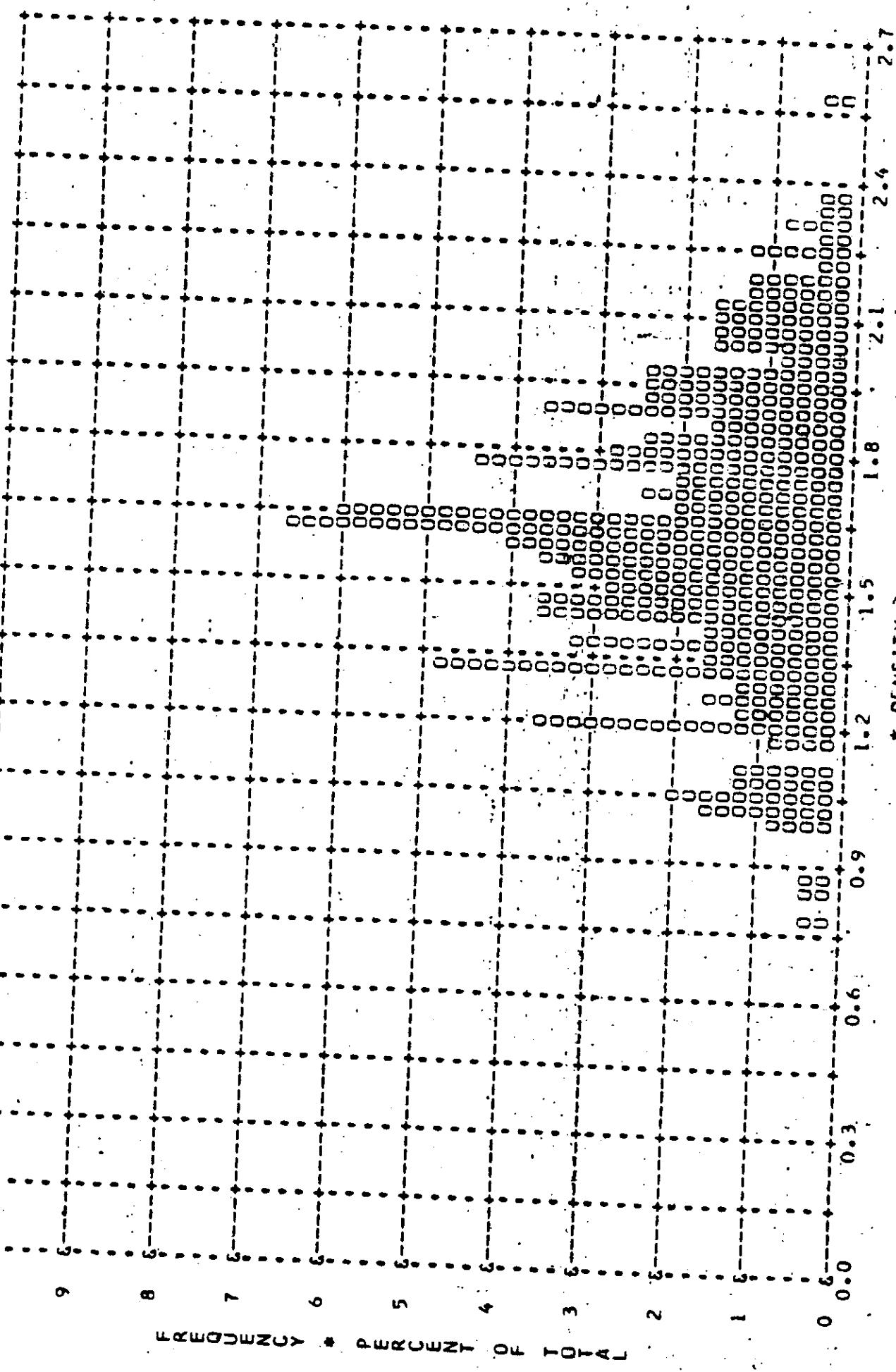


FIGURE A-31

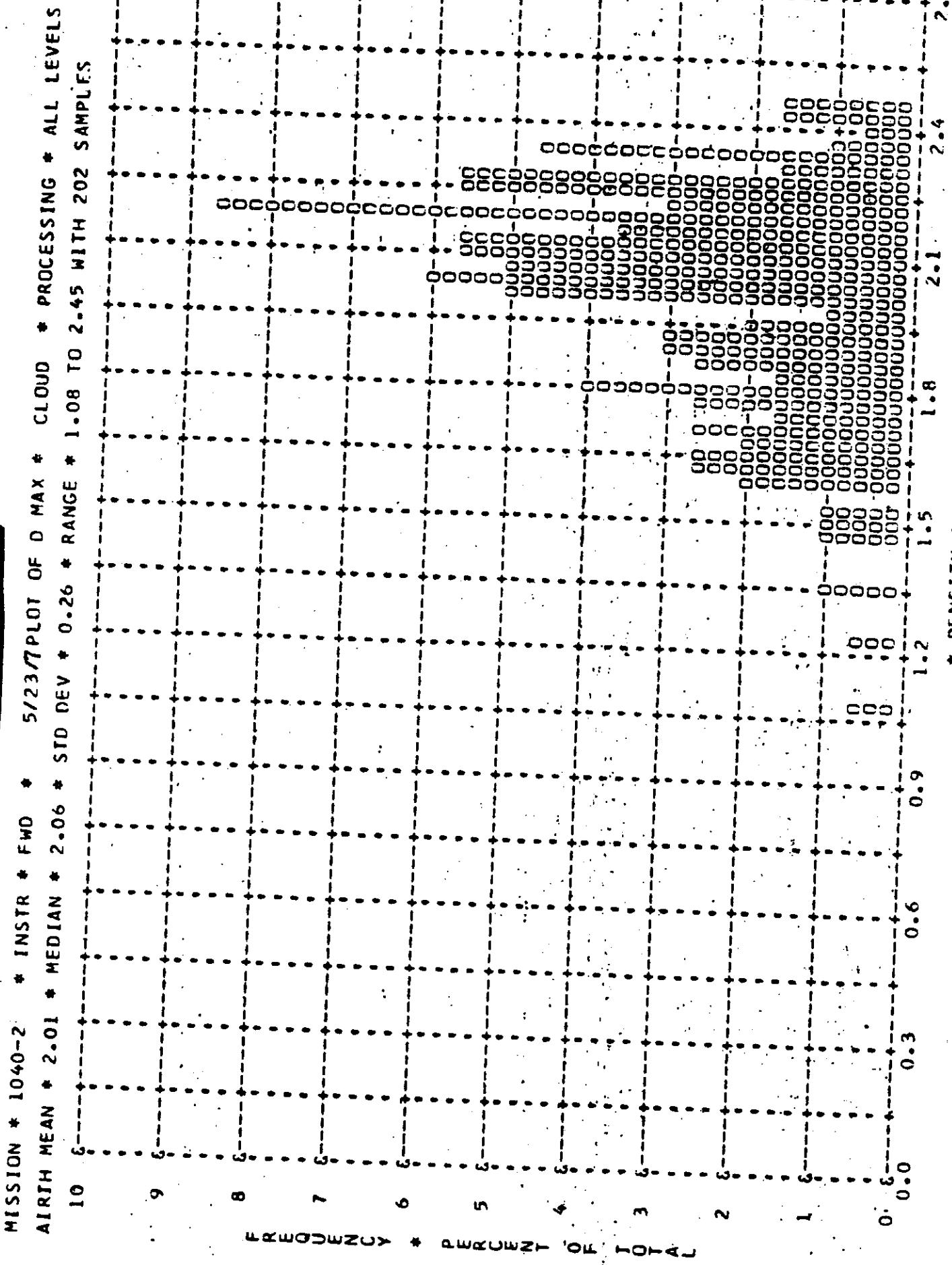
TOP SECRET C

MISSION * 1040-2 * INSTR * FWD * 5/23/79 PLOT OF D MAX * TERRAIN * PROCESSING * ALL LFVFS
AIRTH MEAN * 1.61 * MEDIAN * 1.61 * STD DEV. * 0.33 * RANGE * 0.77 TO 2.58 WITH 258 SAMPLES



TOP SECRET C

FIGURE A-35



TOP SECRET C

* DENSITY *

FIGURE A-30

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * AFT : 5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.01	0 0	0 0	0 0	0 0
0.02	0 0	0 0	0 0	0 0
0.03	0 0	0 0	0 0	0 0
0.04	0 0	0 0	0 0	0 0
0.05	0 0	0 0	0 0	0 0
0.06	0 0	0 0	0 0	0 0
0.07	0 0	0 0	0 0	0 0
0.08	0 0	0 0	0 0	0 0
0.09	0 0	0 0	0 0	0 0
0.10	0 0	0 0	0 0	0 0
0.11	0 0	0 0	0 0	0 0
0.12	0 0	0 0	0 0	0 0
0.13	0 0	0 0	0 0	0 0
0.14	0 0	0 0	0 0	0 0
0.15	0 0	0 0	0 0	0 0
0.16	0 0	0 0	0 0	0 0
0.17	0 0	0 0	0 0	0 0
0.18	0 0	0 0	0 0	0 0
0.19	0 0	0 0	0 0	0 0
0.20	0 0	0 0	0 0	0 0
0.21	0 0	0 0	0 0	0 0
0.22	0 0	0 0	0 0	0 0
0.23	0 0	0 0	0 0	0 0
0.24	0 0	0 0	0 0	0 0
0.25	0 0	0 0	0 0	0 0
0.26	0 0	0 0	0 0	0 0
0.27	0 0	0 0	0 0	0 0
0.28	0 0	0 0	0 0	0 0
0.29	0 0	0 0	0 0	0 0
0.30	0 0	0 0	0 0	0 0
0.31	0 0	0 0	0 0	0 0
0.32	0 0	0 0	0 0	0 0
0.33	0 0	0 0	0 0	0 0
0.34	0 0	0 0	0 0	0 0
0.35	0 0	0 0	0 0	0 0
0.36	0 0	0 0	0 0	0 0
0.37	0 0	0 0	0 0	0 0
0.38	0 0	0 0	0 0	0 0
0.39	0 0	0 0	0 0	0 0
0.40	0 0	0 0	0 0	0 0
0.41	0 0	0 0	0 0	0 0
0.42	0 0	0 0	0 0	0 0
0.43	0 0	0 0	0 0	0 0
0.44	0 0	0 0	0 0	0 0
0.45	0 0	0 0	0 0	0 0
0.46	0 0	0 0	0 0	0 0
0.47	0 0	0 0	0 0	0 0
0.48	0 0	0 0	0 0	0 0
0.49	0 0	0 0	0 0	0 0
0.50	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	0 0	0 0

TABLE A-4

~~TOP SECRET C~~

MISSION # 1040-2 * INSTRUMENT # AET

5/23/67 DENSITY FREQ DISTR

~~TOP SECRET~~ C

TABLE A-4

~~TOP SECRET C~~

MISSION # 1040-2 * INSTRUMENT # AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01	0 0	0 0	0 0	0 0
1.02	0 0	0 0	2 0	2 0
1.03	0 0	0 0	0 0	0 0
1.04	0 0	0 0	0 0	0 0
1.05	0 0	0 0	0 0	0 0
1.06	0 0	0 0	0 0	0 0
1.07	0 0	0 0	0 0	0 0
1.08	0 0	0 0	0 0	0 0
1.09	0 0	0 0	0 0	0 0
1.10	0 0	0 0	0 0	0 0
1.11	0 0	0 0	0 0	0 0
1.12	0 0	0 0	0 0	0 0
1.13	0 0	0 0	0 0	0 0
1.14	0 0	0 0	0 0	0 0
1.15	0 0	0 0	0 0	0 0
1.16	0 0	0 0	0 0	0 0
1.17	0 0	0 0	0 0	0 0
1.18	0 0	0 0	0 0	0 0
1.19	0 0	0 0	0 0	0 0
1.20	0 0	0 0	0 0	0 0
1.21	0 0	0 0	0 0	0 0
1.22	0 0	0 0	0 0	0 0
1.23	0 0	0 0	0 0	0 0
1.24	0 0	0 0	0 0	0 0
1.25	0 0	0 0	0 0	0 0
1.26	0 0	0 0	0 0	0 0
1.27	0 0	0 0	0 0	0 0
1.28	0 0	0 0	0 0	0 0
1.29	0 0	0 0	0 0	0 0
1.30	0 0	0 0	0 0	0 0
1.31	0 0	0 0	0 0	0 0
1.32	0 0	0 0	0 0	0 0
1.33	0 0	0 0	0 0	0 0
1.34	0 0	0 0	0 0	0 0
1.35	0 0	0 0	0 0	0 0
1.36	0 0	0 0	0 0	0 0
1.37	0 0	0 0	0 0	0 0
1.38	0 0	0 0	0 0	0 0
1.39	0 0	0 0	0 0	0 0
1.40	0 0	0 0	0 0	0 0
1.41	0 0	0 0	0 0	0 0
1.42	0 0	0 0	0 0	0 0
1.43	0 0	0 0	0 0	0 0
1.44	0 0	0 0	0 0	0 0
1.45	0 0	0 0	0 0	0 0
1.46	0 0	0 0	0 0	0 0
1.47	0 0	0 0	0 0	0 0
1.48	0 0	0 0	0 0	0 0
1.49	0 0	0 0	0 0	0 0
1.50	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	7 15	21 46

~~TOP SECRET C~~

TABLE A-4

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * AET

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51	0	0	0	0	0	0	0	0	0	0	0	0
1.52	0	0	0	0	0	0	0	0	0	0	0	0
1.53	0	0	0	0	0	0	0	0	0	0	0	0
1.54	0	0	0	0	0	0	0	0	0	0	0	0
1.55	0	0	0	0	0	0	0	0	0	0	0	0
1.56	0	0	0	0	0	0	0	0	0	0	0	0
1.57	0	0	0	0	0	0	0	0	0	0	0	0
1.58	0	0	0	0	0	0	0	0	0	0	0	0
1.59	0	0	0	0	0	0	0	0	0	0	0	0
1.60	0	0	0	0	0	0	0	0	0	0	0	0
1.61	0	0	0	0	0	0	0	0	0	0	0	0
1.62	0	0	0	0	0	0	0	0	0	0	0	0
1.63	0	0	0	0	0	0	0	0	0	0	0	0
1.64	0	0	0	0	0	0	0	0	0	0	0	0
1.65	0	0	0	0	0	0	0	0	0	0	0	0
1.66	0	0	0	0	0	0	0	0	0	0	0	0
1.67	0	0	0	0	0	0	0	0	0	0	0	0
1.68	0	0	0	0	0	0	0	0	0	0	0	0
1.69	0	0	0	0	0	0	0	0	0	0	0	0
1.70	0	0	0	0	0	0	0	0	0	0	0	0
1.71	0	0	0	0	0	0	0	0	0	0	0	0
1.72	0	0	0	0	0	0	0	0	0	0	0	0
1.73	0	0	0	0	0	0	0	0	0	0	0	0
1.74	0	0	0	0	0	0	0	0	0	0	0	0
1.75	0	0	0	0	0	0	0	0	0	0	0	0
1.76	0	0	0	0	0	0	0	0	0	0	0	0
1.77	0	0	0	0	0	0	0	0	0	0	0	0
1.78	0	0	0	0	0	0	0	0	0	0	0	0
1.79	0	0	0	0	0	0	0	0	0	0	0	0
1.80	0	0	0	0	0	0	0	0	0	0	0	0
1.81	0	0	0	0	0	0	0	0	0	0	0	0
1.82	0	0	0	0	0	0	0	0	0	0	0	0
1.83	0	0	0	0	0	0	0	0	0	0	0	0
1.84	0	0	0	0	0	0	0	0	0	0	0	0
1.85	0	0	0	0	0	0	0	0	0	0	0	0
1.86	0	0	0	0	0	0	0	0	0	0	0	0
1.87	0	0	0	0	0	0	0	0	0	0	0	0
1.88	0	0	0	0	0	0	0	0	0	0	0	0
1.89	0	0	0	0	0	0	0	0	0	0	0	0
1.90	0	0	0	0	0	0	0	0	0	0	0	0
1.91	0	0	0	0	0	0	0	0	0	0	0	0
1.92	0	0	0	0	0	0	0	0	0	0	0	0
1.93	0	0	0	0	0	0	0	0	0	0	0	0
1.94	0	0	0	0	0	0	0	0	0	0	0	0
1.95	0	0	0	0	0	0	0	0	0	0	0	0
1.96	0	0	0	0	0	0	0	0	0	0	0	0
1.97	0	0	0	0	0	0	0	0	0	0	0	0
1.98	0	0	0	0	0	0	0	0	0	0	0	0
1.99	0	0	0	0	0	0	0	0	0	0	0	0
2.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL				54		29		96		24		150

~~TOP SECRET~~ C

TABLE A-4

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01	0	0	0	0	0	1	0	2	2	0	2	3
2.02	0	0	0	0	0	0	0	3	3	0	3	3
2.03	0	0	0	0	0	0	0	3	3	0	4	4
2.04	0	0	0	0	0	0	0	4	4	1	4	4
2.05	0	0	0	0	0	0	0	1	1	1	6	6
2.06	0	0	0	0	0	0	0	1	1	1	4	4
2.07	0	0	0	0	0	0	0	2	2	1	3	3
2.08	0	0	0	0	0	0	0	3	3	0	3	3
2.09	0	0	0	0	0	0	0	4	4	1	4	4
2.10	0	0	0	0	0	0	0	1	1	1	1	1
2.11	0	0	0	0	0	0	0	1	1	1	1	1
2.12	0	0	0	0	0	0	0	1	1	1	1	1
2.13	0	0	0	0	0	0	0	1	1	1	1	1
2.14	0	0	0	0	0	0	0	1	1	1	1	1
2.15	0	0	0	0	0	0	0	1	1	1	1	1
2.16	0	0	0	0	0	0	0	1	1	1	1	1
2.17	0	0	0	0	0	0	0	1	1	1	1	1
2.18	0	0	0	0	0	0	0	1	1	1	1	1
2.19	0	0	0	0	0	0	0	1	1	1	1	1
2.20	0	0	0	0	0	0	0	1	1	1	1	1
2.21	0	0	0	0	0	0	0	1	1	1	1	1
2.22	0	0	0	0	0	0	0	1	1	1	1	1
2.23	0	0	0	0	0	0	0	1	1	1	1	1
2.24	0	0	0	0	0	0	0	1	1	1	1	1
2.25	0	0	0	0	0	0	0	1	1	1	1	1
2.26	0	0	0	0	0	0	0	1	1	1	1	1
2.27	0	0	0	0	0	0	0	1	1	1	1	1
2.28	0	0	0	0	0	0	0	1	1	1	1	1
2.29	0	0	0	0	0	0	0	1	1	1	1	1
2.30	0	0	0	0	0	0	0	1	1	1	1	1
2.31	0	0	0	0	0	0	0	1	1	1	1	1
2.32	0	0	0	0	0	0	0	1	1	1	1	1
2.33	0	0	0	0	0	0	0	1	1	1	1	1
2.34	0	0	0	0	0	0	0	1	1	1	1	1
2.35	0	0	0	0	0	0	0	1	1	1	1	1
2.36	0	0	0	0	0	0	0	1	1	1	1	1
2.37	0	0	0	0	0	0	0	1	1	1	1	1
2.38	0	0	0	0	0	0	0	1	1	1	1	1
2.39	0	0	0	0	0	0	0	1	1	1	1	1
2.40	0	0	0	0	0	0	0	1	1	1	1	1
2.41	0	0	0	0	0	0	0	1	1	1	1	1
2.42	0	0	0	0	0	0	0	1	1	1	1	1
2.43	0	0	0	0	0	0	0	1	1	1	1	1
2.44	0	0	0	0	0	0	0	1	1	1	1	1
2.45	0	0	0	0	0	0	0	1	1	1	1	1
2.46	0	0	0	0	0	0	0	1	1	1	1	1
2.47	0	0	0	0	0	0	0	1	1	1	1	1
2.48	0	0	0	0	0	0	0	1	1	1	1	1
2.49	0	0	0	0	0	0	0	1	1	1	1	1
2.50	0	0	0	0	0	0	0	1	1	1	1	1
SUBTOTAL	0	0	0	0	0	0	7	26	0	34	114	41

~~TOP SECRET C~~

TABLE A-4

~~TOP SECRET C~~

MISSION * 1040-2 * INSTRUMENT * AFT

5/23/67 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN	PRIMARY MAX	PRIMARY LIM	INTERMEDIATE MIN	INTERMEDIATE MAX	INTERMEDIATE LIM	FULL MIN	FULL MAX	FULL LIM	ALL LEVELS MIN	ALL LEVELS MAX	ALL LEVELS LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	5	76	77	58	163	165	138	239	242	201

MISSION 1040-2

INSTR - AFT

5/23/67 PROCESSING AND EXPOSURE ANALYS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	3 PC	41 PC	39 PC
INTERMEDIATE	76	0 PC	7 PC	75 PC	17 PC	1 PC
FULL	163	5 PC	0 PC	79 PC	16 PC	0 PC
ALL LEVELS	239	3 PC	2 PC	78 PC	16 PC	0 PC
PROCESS LEVEL	BASE & FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP&PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	0.91 AND U
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.35 AND U 1.70 AND U

~~TOP SECRET C~~

TABLE A-4

TOP SECRET C

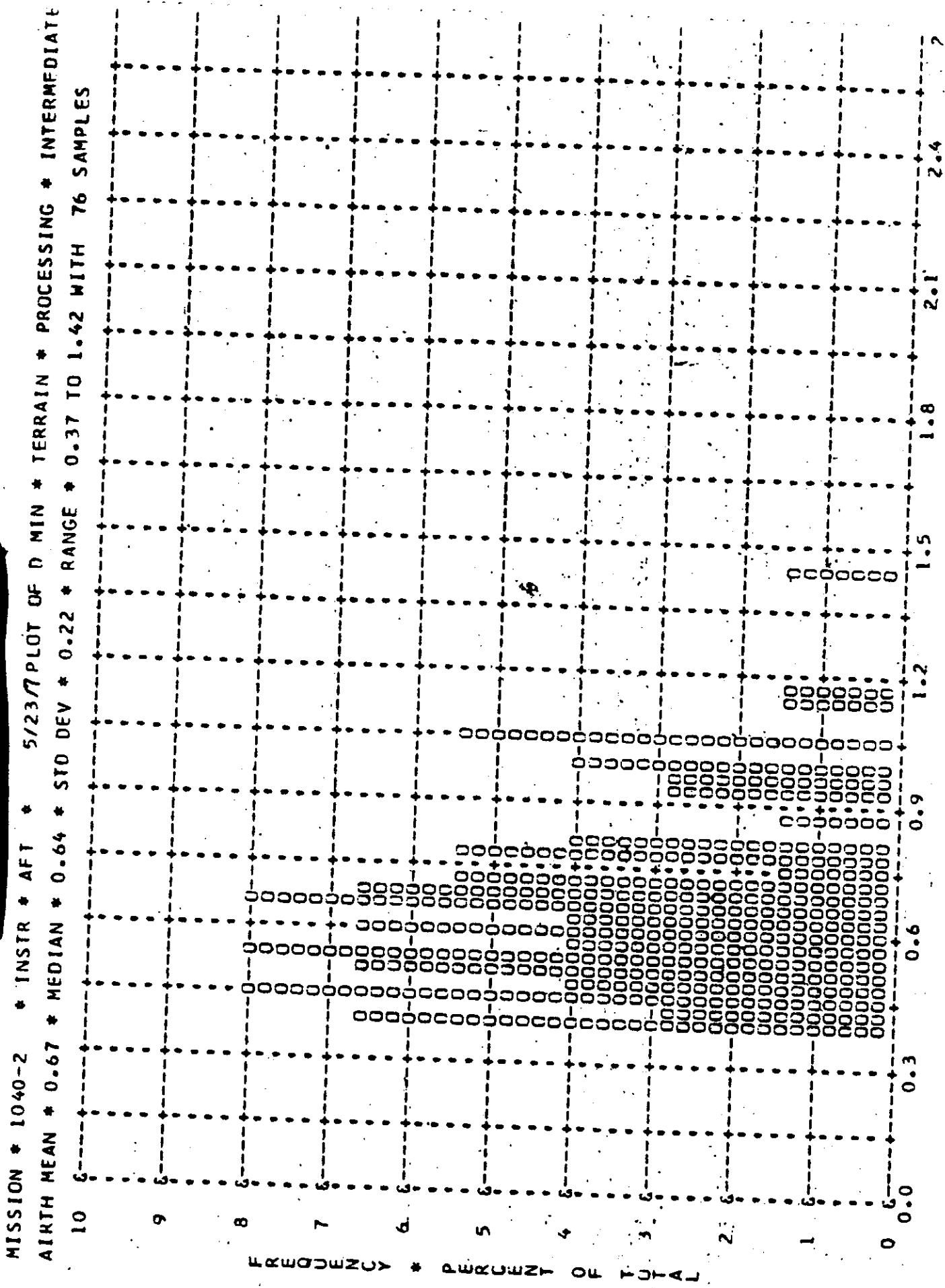


FIGURE A-27

TOP SECRET C

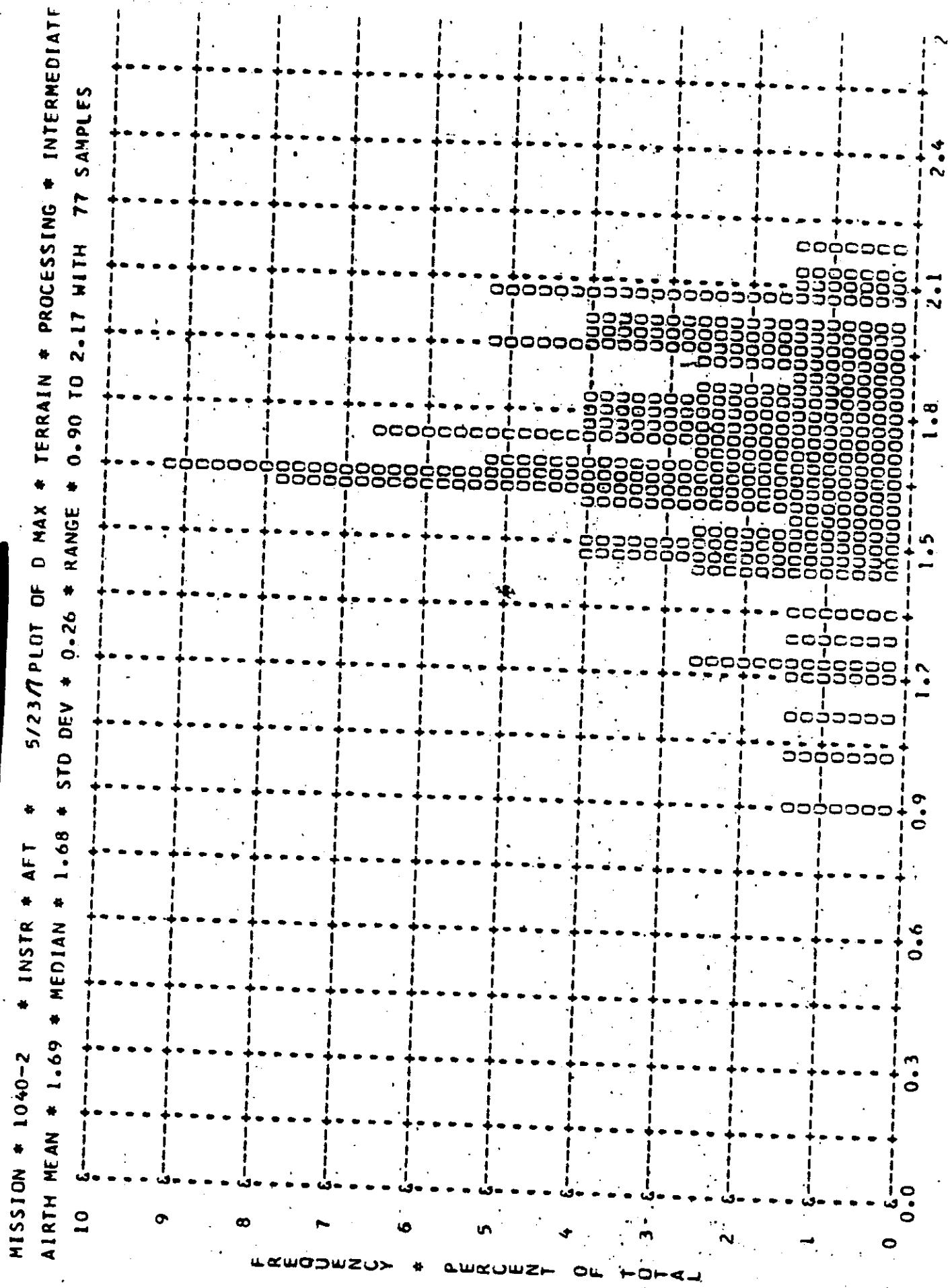
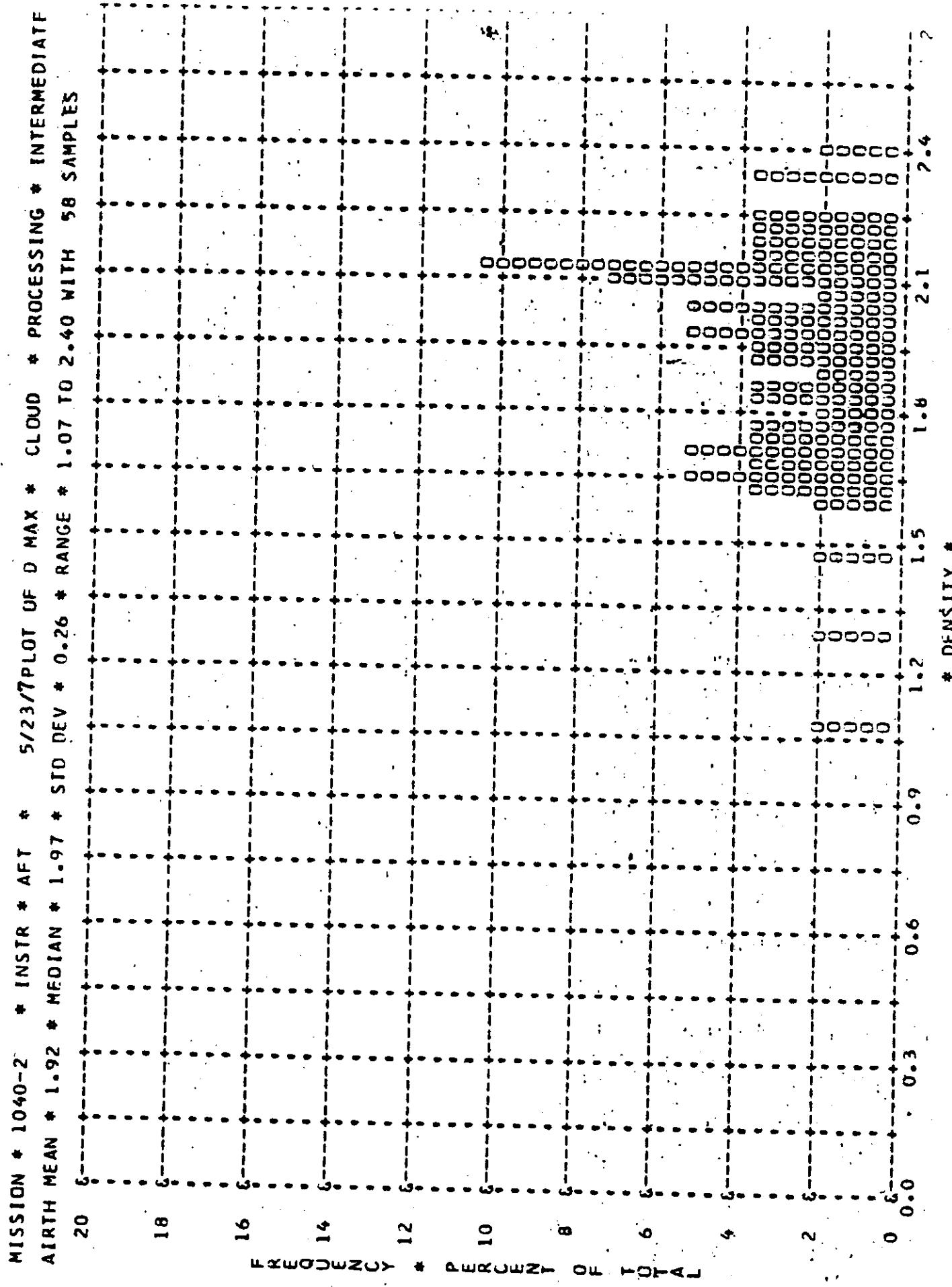


FIGURE A-38

TOP SECRET C



MISSION * 1040-2 * INSTR * AFT * 5/23/77 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.68 * MEDIAN * 0.63 * STD DEV * 0.22 * RANGE * 0.11 TO 1.43 WITH 163 SAMPLES

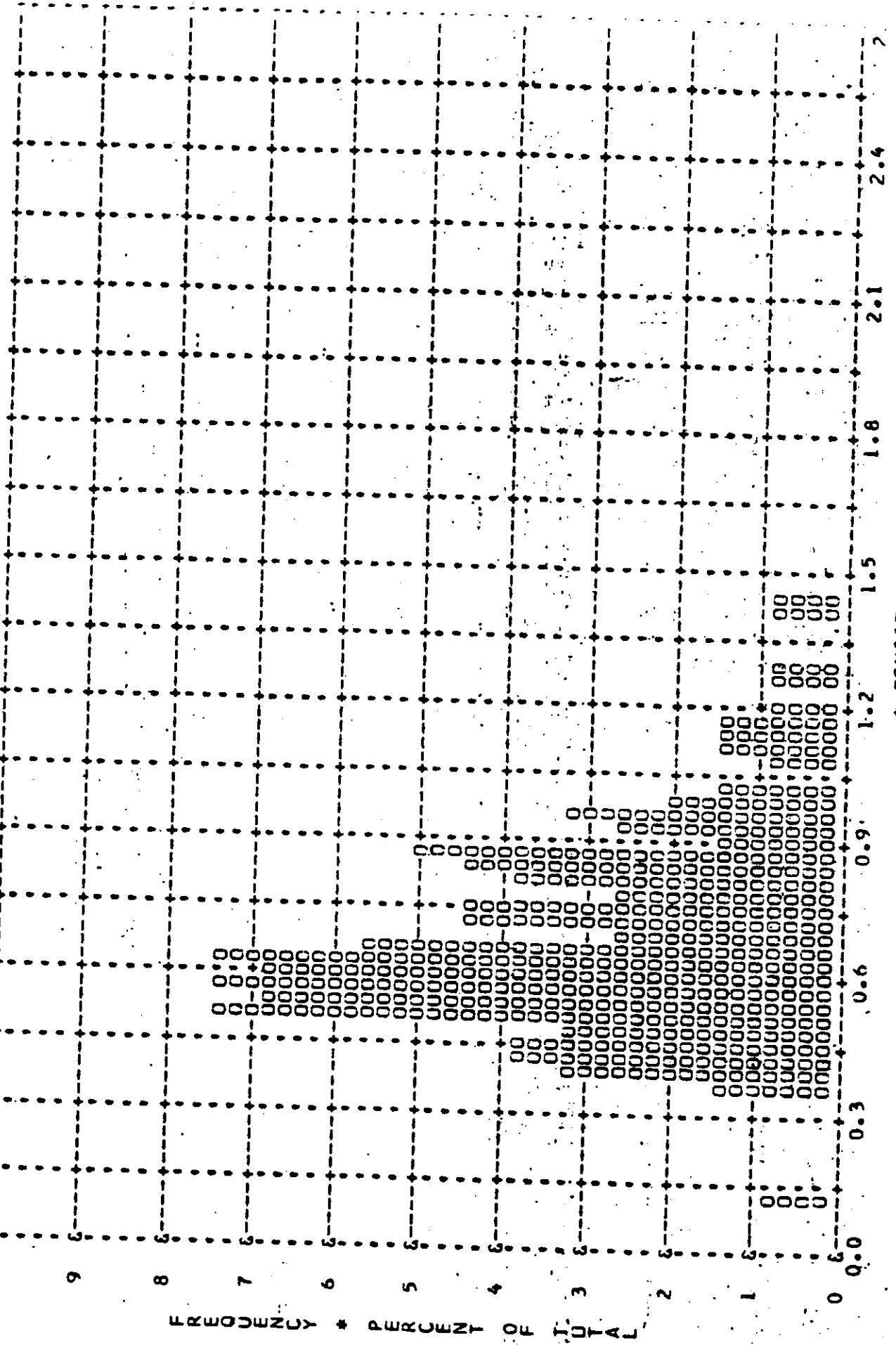
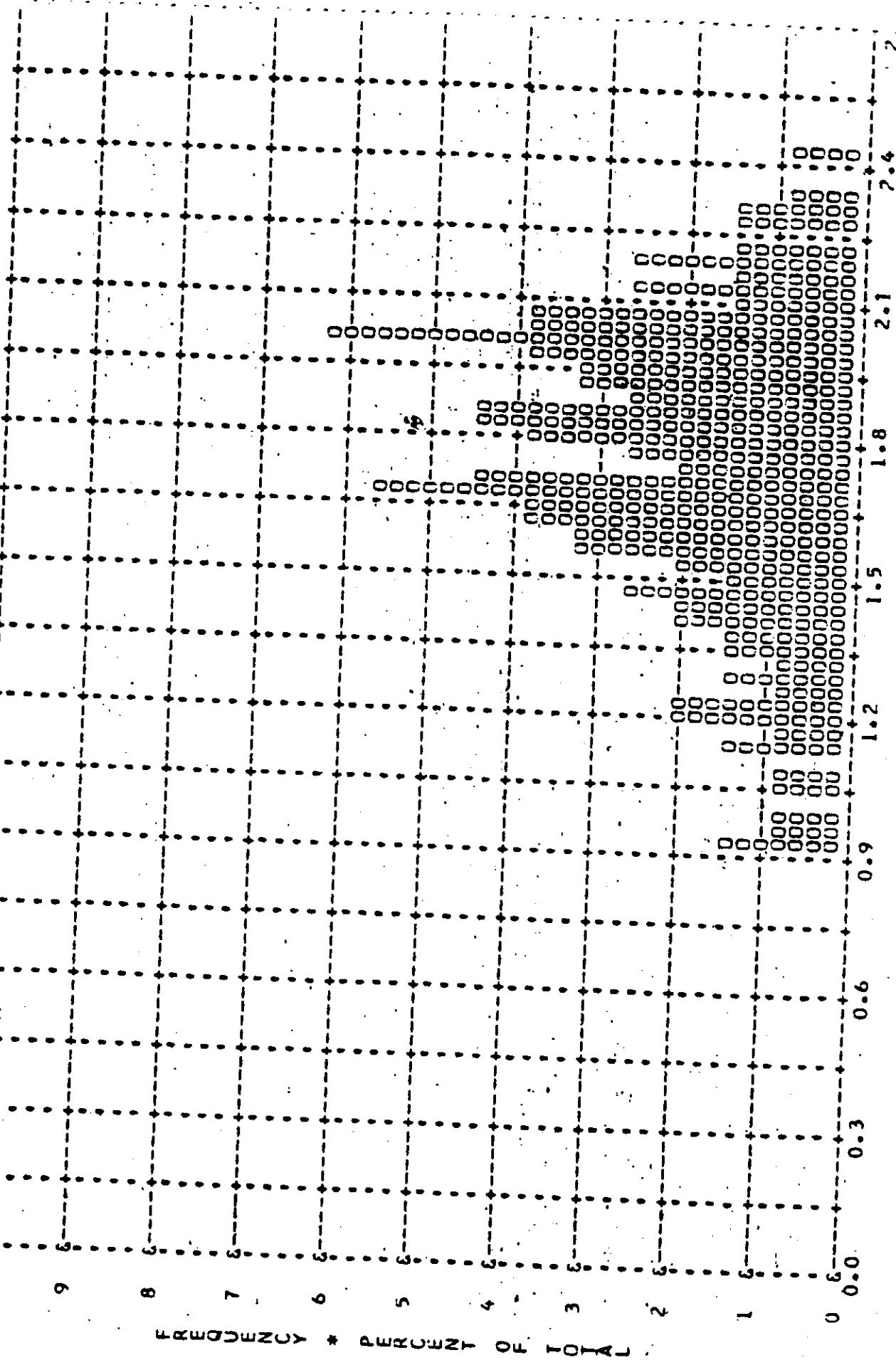


FIGURE A-10

* DENSITY *

TERRAIN

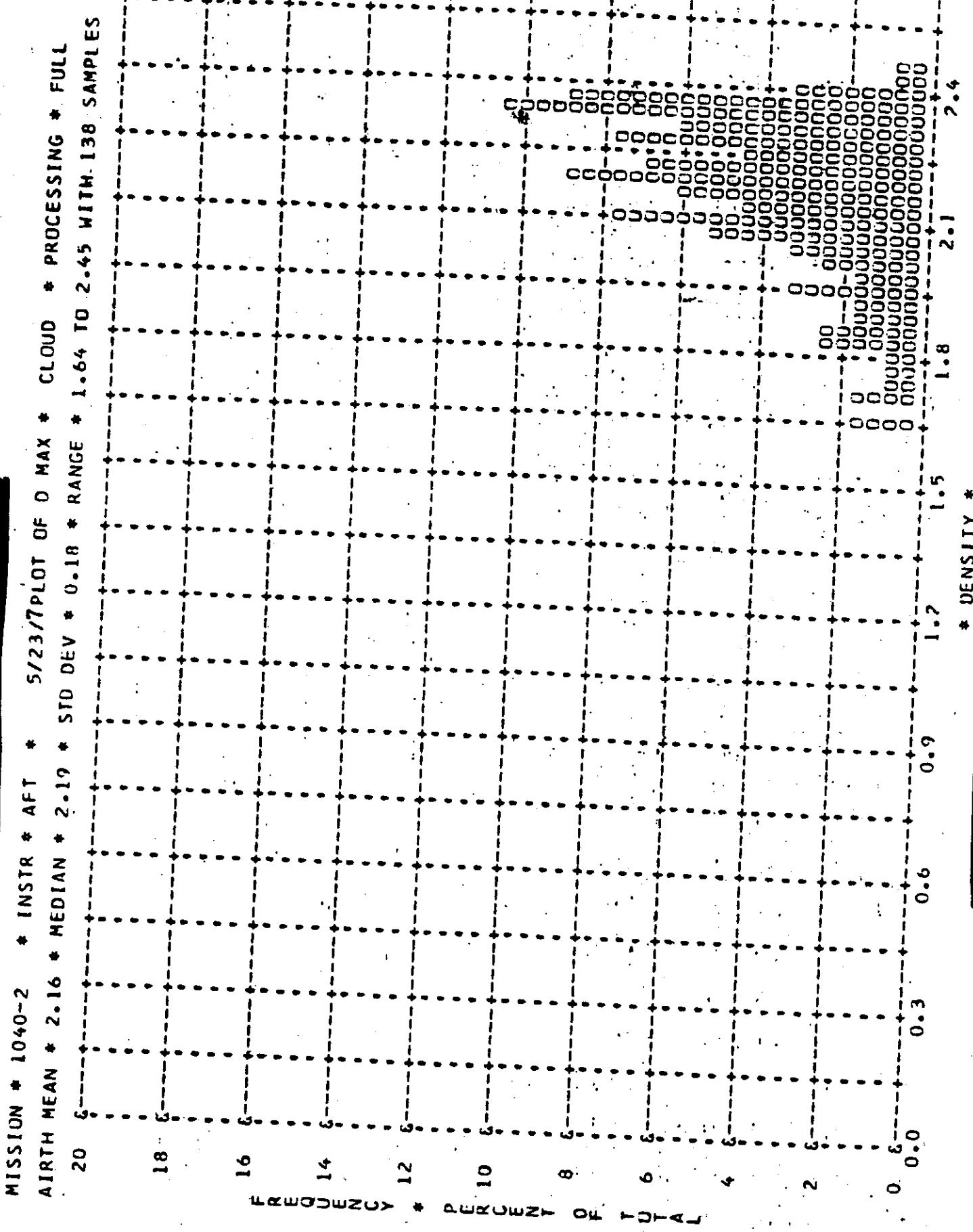
MISSION * 1040-2 * INSTR * AFT * 5/23/7 PLOT OF D MAX * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 1.74 * MEDIAN * 1.77 * STU DEV * 0.32 * RANGE * 0.91 TO 2.43 WITH 165 SAMPLES



* DENSITY *

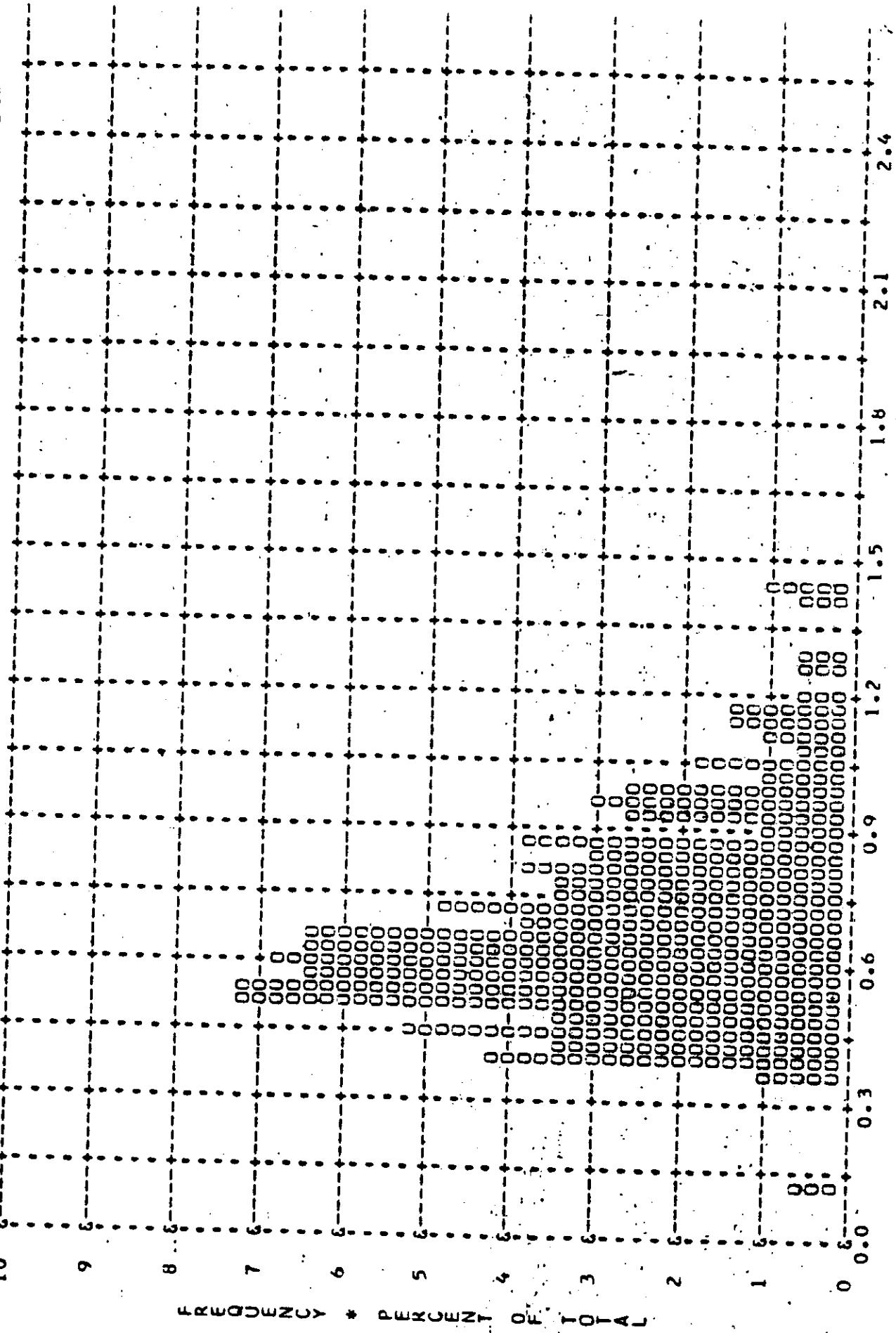
TOP SECRET

480-Secret C

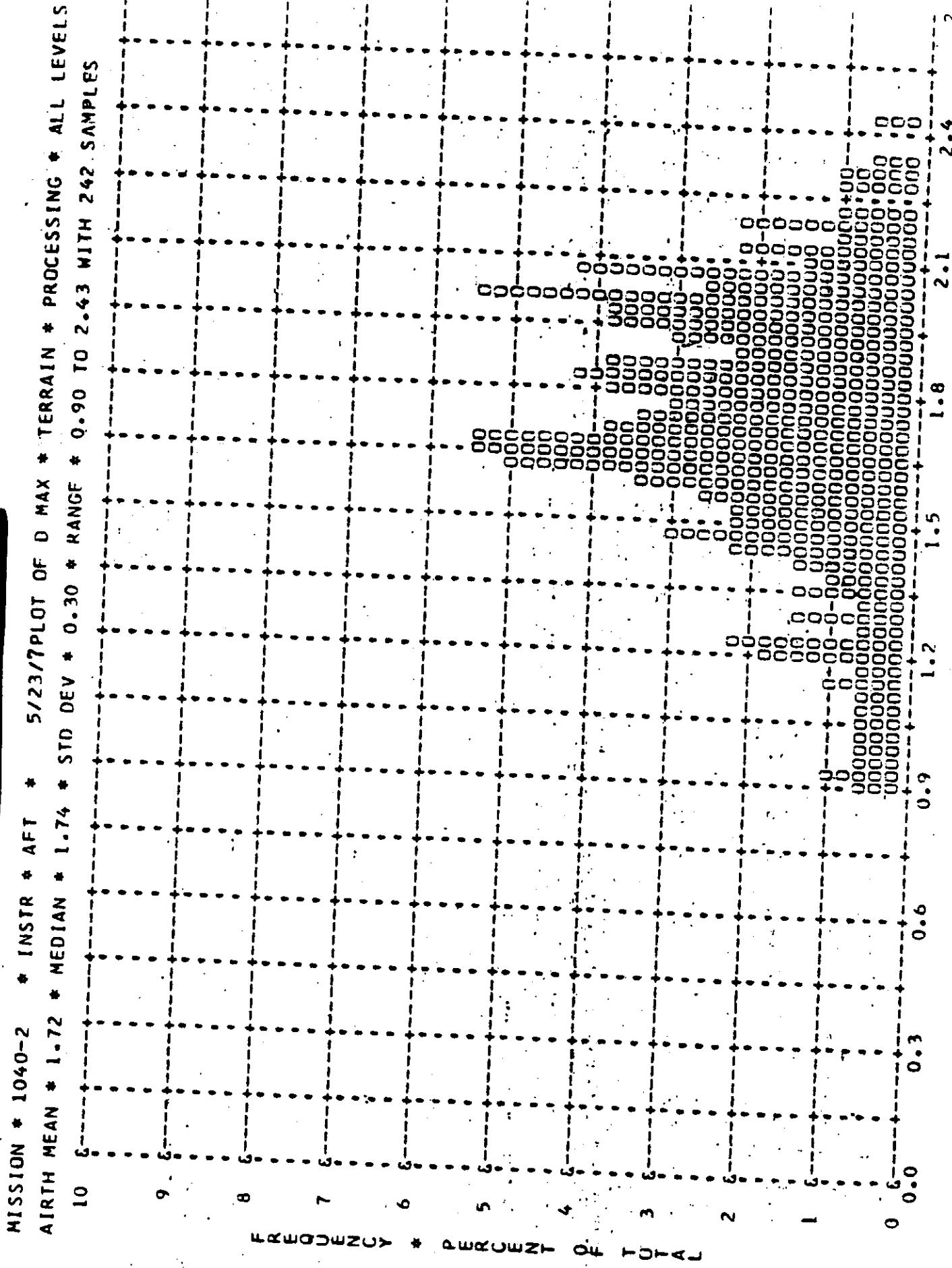


~~TOP SECRET C~~

MISSION * 1040-2 * INSTR * AFT * 5/23/7 PLOT OF D MIN * TERRAIN * PROCESSING * ALL LEVELS
AIRTH MEAN * 0.68 * MEDIAN * 0.63 * STD DEV * 0.22 * RANGE * 0.11 TO 1.43 WITH 239 SAMPLES



TOP SECRET C

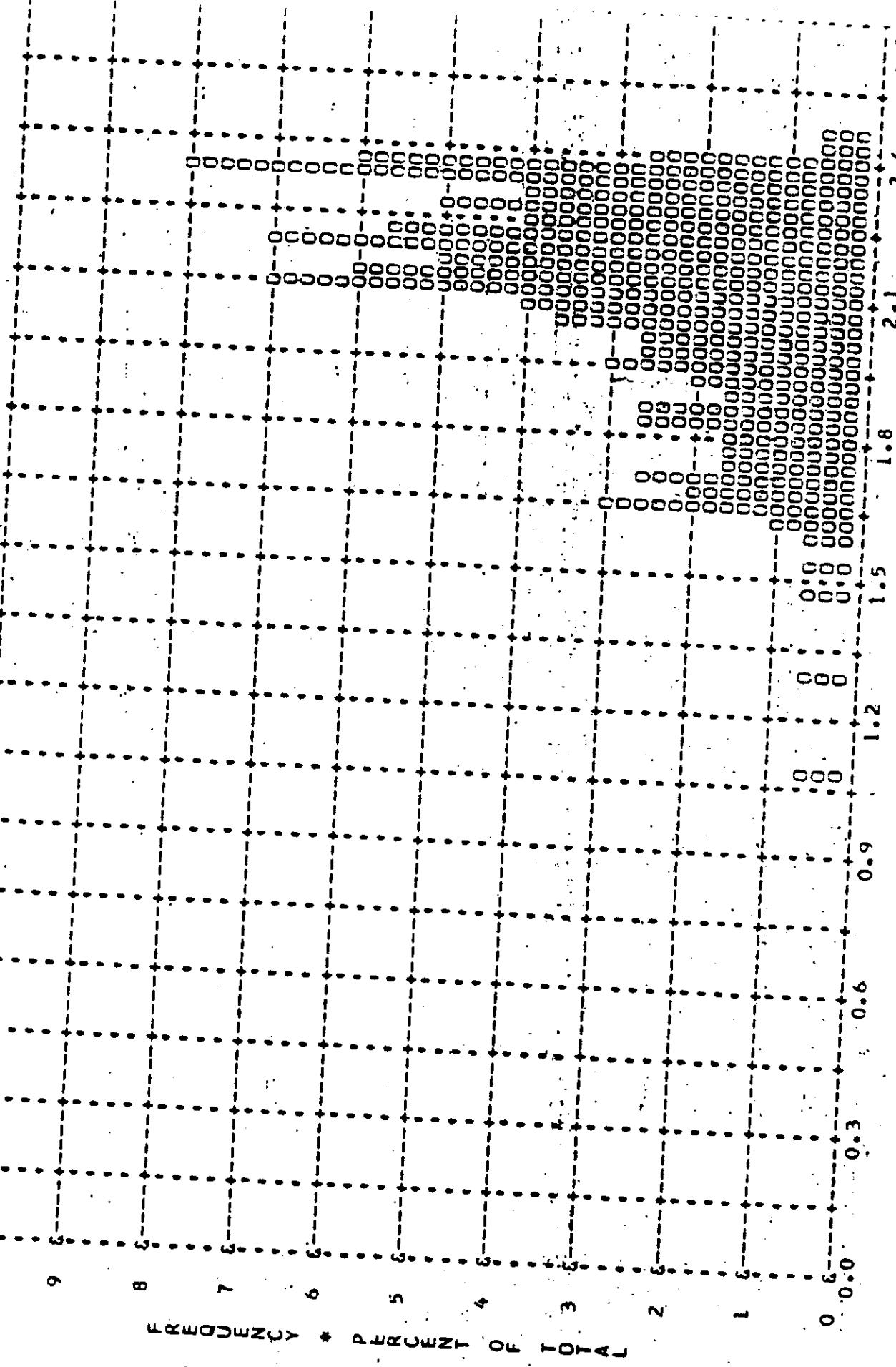


TOP SECRET C

TOP SECRET C

-TOP SECRET C

MISSION * 1040-2 * INSTR * AFT * 5/23/7 PLOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS
AIRT MEAN * 2.08 * MEDIAN * 2.12 * STD DEV * 0.24 * RANGE * 1.07 TO 2.45 WITH 201 SAMPLES



* DENSITY *

-TOP SECRET C

~~TOP SECRET C~~

Distribution:

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To



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